NINETEENTH ANNUAL Burn-in & Test Strategies Workshop

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Heating Up - Burn-in and Thermal

Contactor Thermal Control Features

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Heating Up - Burn-in and Thermal

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Introduction

Industry trend

- Today's semiconductor applications do have the need for tighter temperature control
- Temperature ranges expanding to meet more stringent end use condition and there is a need for better control of the temperature range and temperature accuracy
- High test side parallelisms \rightarrow Test in Strip handling
- Small contact length for high frequency ranges......







Introduction

Thermal and power management

- Increasing total power across a smaller form factors \rightarrow Power density increase
- Handling the heat, produced by the DUT itself drive the need of active thermal management.
- Temperature range -40° C 160° C
- Demand for reducing calibration time when setting up a system or change to a different package
- Pre heat or soak time management →utilization of system

Design concept for thermal performance

- Dealing with material / Thermal coefficient / High current demands
- DUT to chuck thermal interface
- Preheating and controlling during test.



Project definition

- SOW:
 - Contact site parallelism:
 - Calibration-less contactor:
 - Package size:
 - Handling system:
- Challenges:
 - +/- 2° C accuracy
 - High parallelism x 27
 - Small contact element length \rightarrow
 - HF pins \rightarrow 3.2 mm contact compressed length
 - Mechanical robustness \rightarrow
 - contactor array
 - Accurate sensor reading \rightarrow
 - correlation to DUT



x 27 -40° C to 160° C

- DFN 2.5 x 2.5, 10 Pin + Ground
- COHU Jaguar Test in Strip Handler



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Concept phase

- Advantage Daughter Board:
 - Improved thermal insulation (insulation thickness)
 - Decoupling load board from temperature
 - Improved temperature stability at the device
 - Easier to integrate the thermal connection between seal plate and socket.
 - Possible to use universal load board for different configurations
- Advantage Non Pogo Tower:
 - Shorter signal length to board signal integrity
 - Direct connection to main board
 - No additional board (reduced interfaces)



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Concept V1_a Geometry and Simulation



Concept V1_a Simulation



- Spring pin Temperatures:
 - Max: 155.7° C
 - Min: 144.2° C
 - Delta: 11.5° C
- Temperature difference between contact sites on the air entrance and outlet!

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Concept V1_b Geometry and Simulation



- Change the Air channel geometry:
 - Increase the cross section at the last contact site to avoid the stall effect and reach a more homogeneous temperature

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Concept V1_b Simulation



- Spring pin Temperatures:
 - Max: 155.3° C
 - Min: 143.3° C
 - Delta: 12° C
- Temperature difference between contact sites on the air entrance and outlet!
- No improvement!



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Opening

Chamber

T = +160[°C]

side:

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1111 1111

11.0

1111

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Concept V2_a Geometry and Boundary

 $T = +151[^{\circ}C]$

T = +157[°C] ·

T = +158[°C]-

T = +157[°C]~

T = +155[°C]. T = +151[°C]

T = +155[°C] -

111

1111



• Change the airflow concept:

- Purpose: get the same airflow on all contact sites by designing a conical cavity and stream thru each Contact site using a throttle



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Concept V2_a Simulation



- Spring pin Temperatures: ٠
 - Max: 148.4° C
 - Min: 128.8° C
 - Delta: 19.6° C
- We made it worse! ...?
- Temperature difference • between the Pin within one contact site!
- Outer contact sites colder than • inner contact sites

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Concept V2_b Geometry

		<u> </u>	0	• Cha Us isc	ange the airflow sing the exhaust plate the outer co	direction: air to ontact sites
	Air inlet Air inlet		Airou	Air in Air in Air in		Air outlet Air outlet Air outlet
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Concept V2_b Simulation



- Spring pin Temperatures:
 - Max: 151.8° C
 - Min: 141.9° C
 - Delta: 9.9° C
 - Improved temperature spread over all contact sites



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Concept V2_b Results

• Contact site mapping:

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- Spring pin temperatures:
 - Max: 149.0° C
 - Min: 146.1° C
 - Delta: 2.9° C

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• Average contact site temperature



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Conclusion - Simulation

- Simulation results show homogenous temperature over all contact sites:
 - Does it correlate with the reality?
 - Simulation is within +/-2° C average per contact site
 - What is the DUT reading?
 - Is it possible to calibrate the System to the simulated values? (Power system)
 - One channel to control the contactor air system... is it enough?
 - Where is the right position of the sensor for controlling (→DUT reading?
 - The sensor need to be part of the handler temperature control loop
 - Do we need additional sensors for monitoring?

No choice, we have to try it!



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Measurements DUT 24.5° C



For all temperature test the same condition:

- Docking installed
- Purge air cover installed to simulate tester purge air (40l/min)

• 10s test time

Contactor center sensor
(2) for feedback-control

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Measurements DUT 125° C

- Soak-time 60 s (Strip Chamber)
- 125° C set point base calibrated, contactor w/o calibration
- Within +/-2° C

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Measurements - 40°C

- Soak-time 120 s (Strip Chamber)
- -40° C set point base calibrated, contactor w/o calibration
- Within +/-2° C

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Measurements +160° C

- Soak-time 120s (Strip Chamber)
- 160° C set point base calibrated, contactor w/o calibration
- Within +/-2.5° C (including drift)

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Conclusion and next steps

Accomplishment:

- No settling or change during 24h temperature run
- Calibration-less contactor for -40 to 160° C (constant offset for contactor temperature required to achieve best results in drift = depending on internal contactor sensor location)
- High parallelism (x 27) RF-contactor running within +/-2.5° C from -40 to 160° C over complete strip with 2500 devices

Next steps:

- · Setup a project to bring calibration-less concept into serial status
 - Integrate the sensor routing into the socket interface definition
 - Prove of concept for different applications (packages and contact site parallelism)
 - Concept integration in other high parallel handlings concepts → P&P.....

