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New universal multi-beam Kelvin contactor concept for turret applications

**Mathias Westenhuber
Johann Pötzing
COHU ITS**



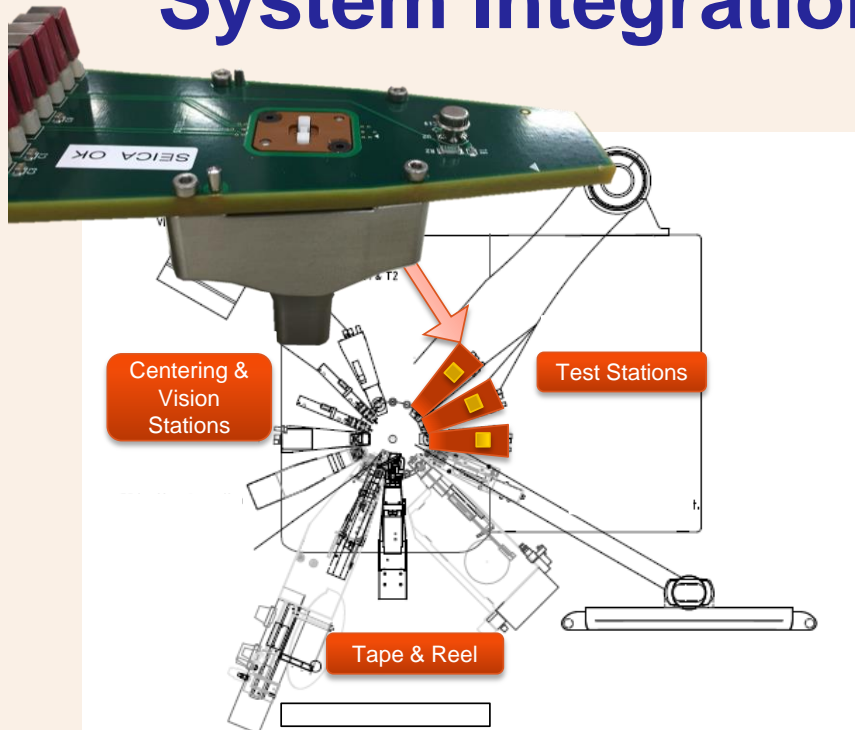
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Agenda

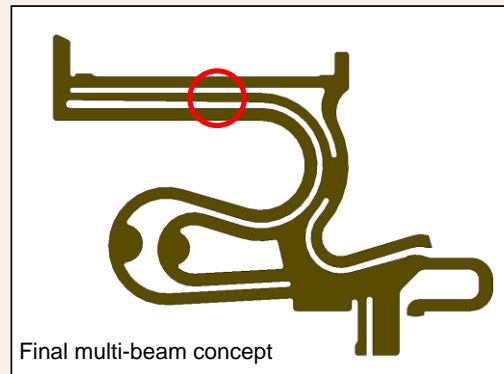
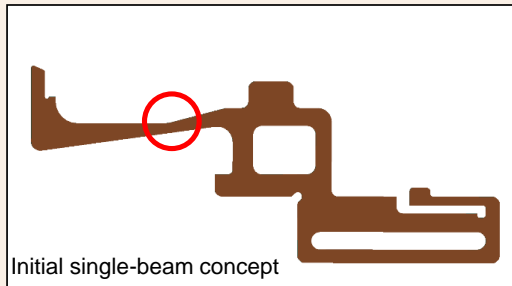
- System Integration Overview
- Why multi-beam Kelvin Contactor?
- Validation
- Why side-by-side Kelvin?
- Upside-down load board configuration
- Conclusion

System Integration Overview

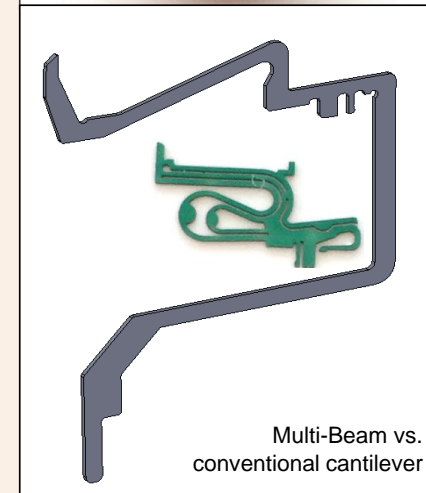
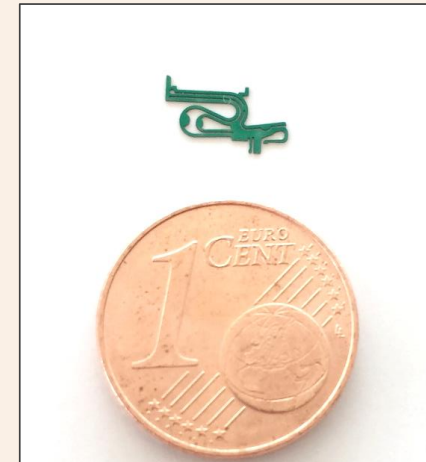


- To integrate test stations into a Turret Handler space is very limited
Only compact cantilever Test Sockets can be integrated
- Turret Handler are typically running at high speed

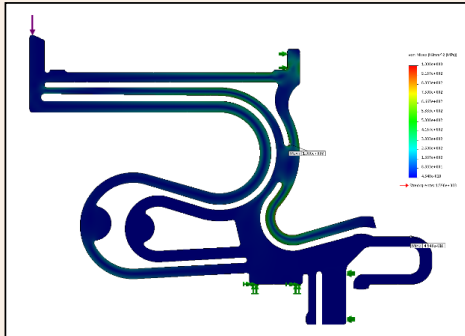
Why Multi-Beam Kelvin Contactor?



- Significant pin size reduction by maintaining high current carrying capability and good signal integrity
- The multi-beam concept allows to increase the current carrying capacity CCC from 2 A to 3 A
- The cross section was increased from 0.22 mm to 0.55 mm → x2.5!
- Low contact force of 0.20 N (0.20 mm deflection) by maintaining a big cross section

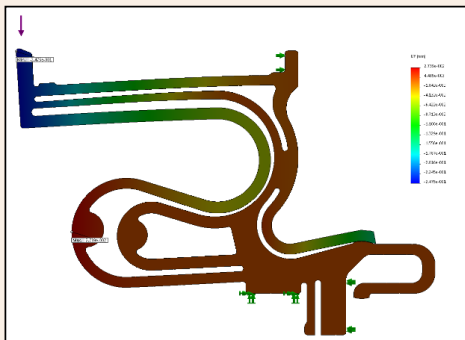


Lifetime, Stress & Compression Simulation



- Stress simulation

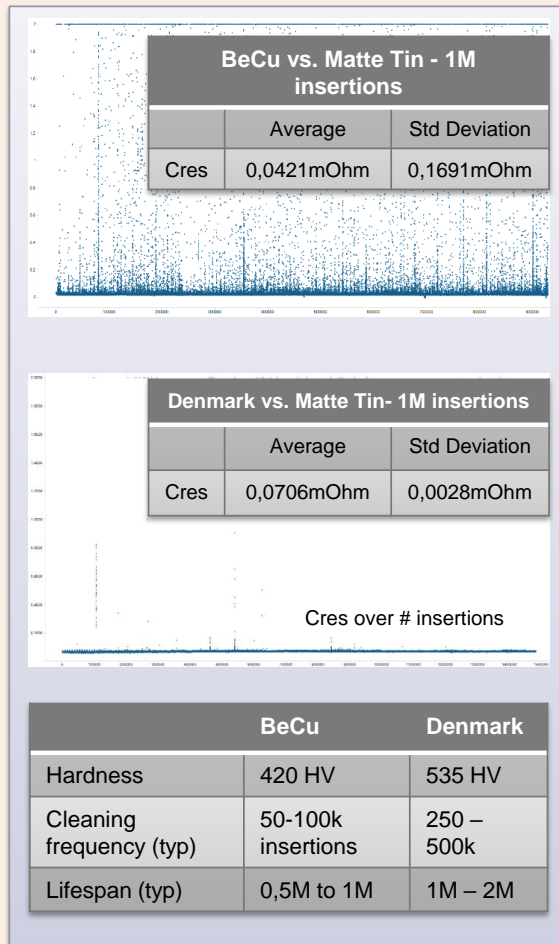
- The multi-beam concept allows to distribute the stress over the three beams and assures a low mechanical stress in the pin structure
- Mechanical validations did confirm no broken pins up to 10 million cycles



- Compression simulation

- The multi-beam concept allows a high compression while maintain a low contact force (0.20mm – 0.2N)

CRES Validation



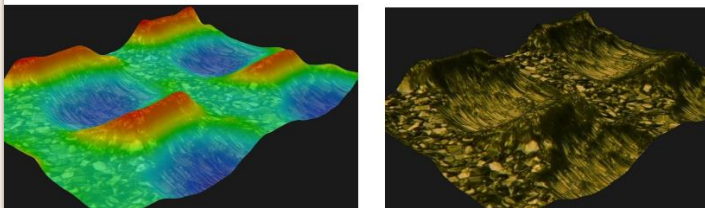
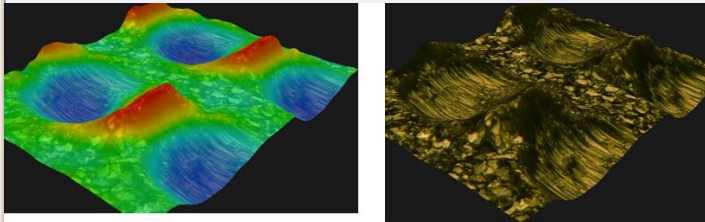
- Actual lead frame material was used to simulate “Test Floor environment”
- Denmark has significant higher hardness HV vs CuBe and shows a very tight CRES standard deviation
- Pin material prevents solder transfer and migration which results in longer cleaning intervals and improved pin lifetime



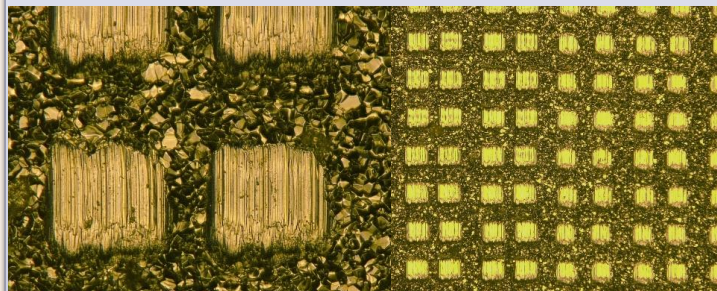
Leadframe material with Matte Tin plating

Validation

Scrub mark depth 7 μ m after 10 insertions



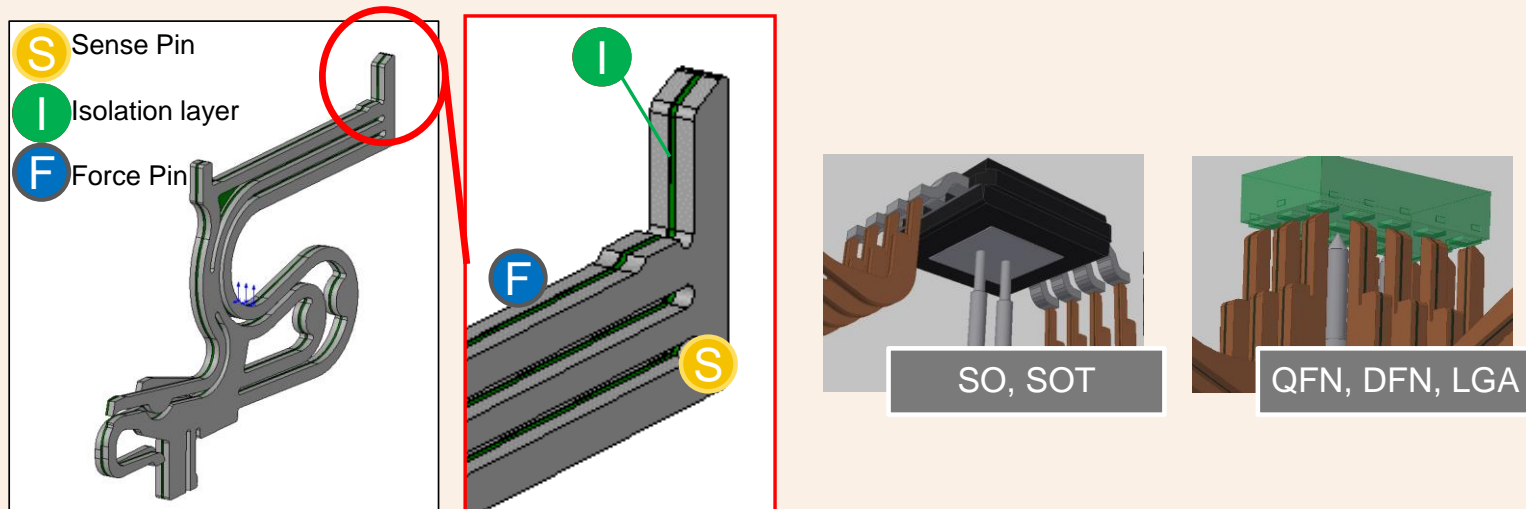
Scrub mark length validation 60 μ m



wear & tear rate validation

| insertions | wear rate (NIAuPD) | Top view | Oblique view |
|------------|--------------------|----------|--------------|
| 100k | 3 μ m | | |
| 500k | 6 μ m | | |
| 1M | 10 μ m | | |
| 2M | 12 μ m | | |
| 3M | 14 μ m | | |

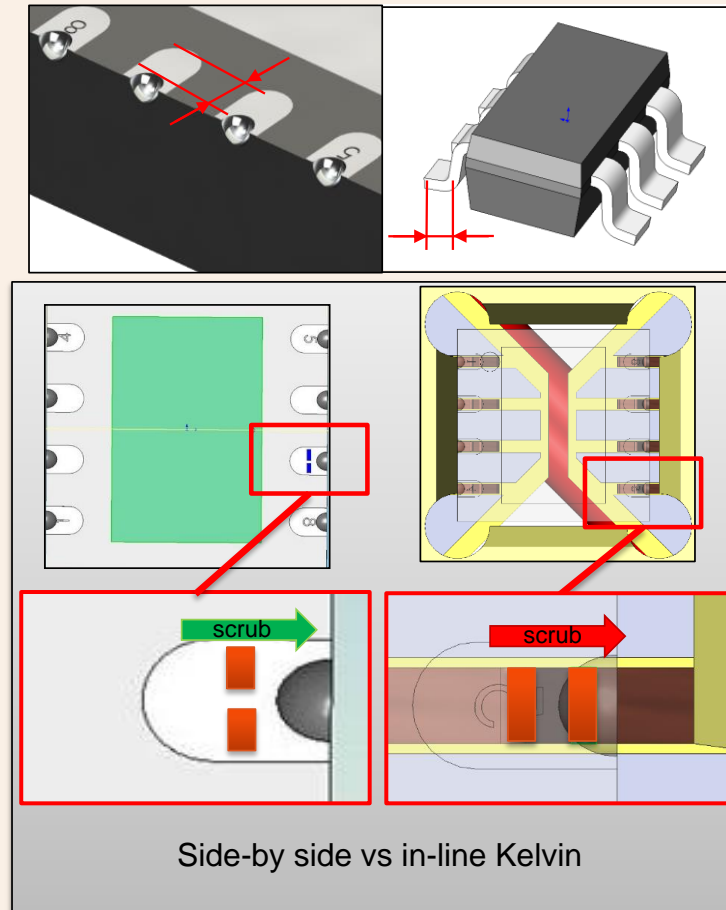
Side-by-side Architecture



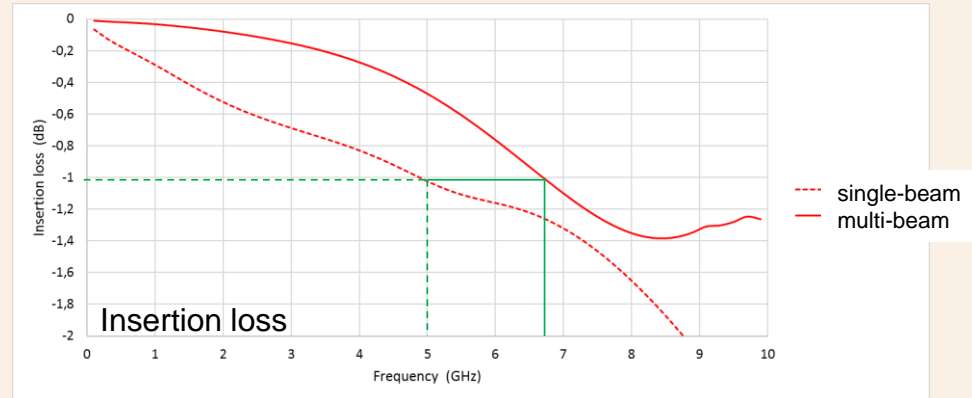
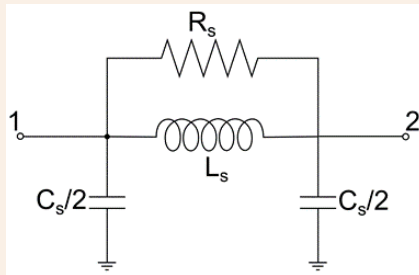
- Force & Sense pin are able to move independently
- High performance insulation layer extremely durable and flexible
- Isolation layer is attached to the force pin
- Total pin thickness ~0.25 mm
- Pin compression creates a 60 μm scrub on the device pad / lead
- Multi-beam structure allows passive cooling for power applications

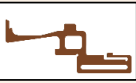
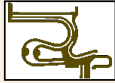
Why Side-by-side Kelvin Contactor?

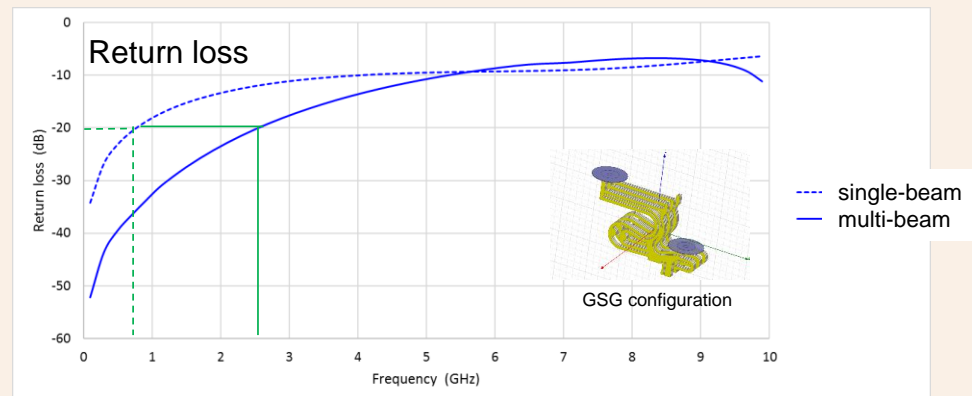
- QFN Devices show a trend towards shorter pad lengths
- Solderability Inspection features reducing the available contact area further
- The lead length of small SOT Devices provide insufficient contact area
- Typical contact surface areas are $< 0.25\text{mm} \times 0.2\text{mm}$
- Low CRES requirements demand a homogenous pin with a defined scrub of $60\mu\text{m}$



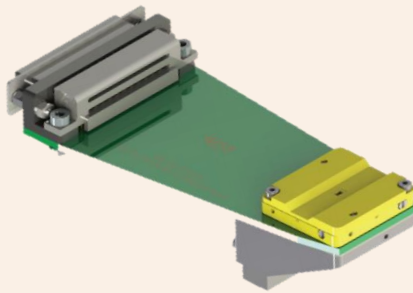
Comparison: Single- vs Multi-beam



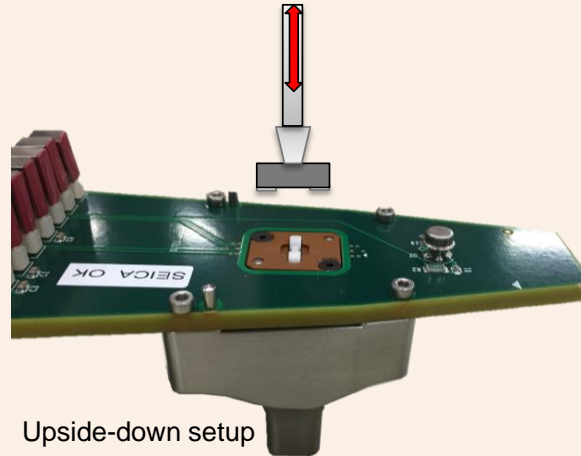
| |  |  |
|-------------------------|---|---|
| Insertion loss @ -1 dB | 4.88 | 6.70 |
| Return loss @ -20 dB | 0.78 | 2.54 |
| Self inductance (nH) | 4.21 | 2.70 |
| Ground capacitance (pF) | 0.78 | 0.92 |



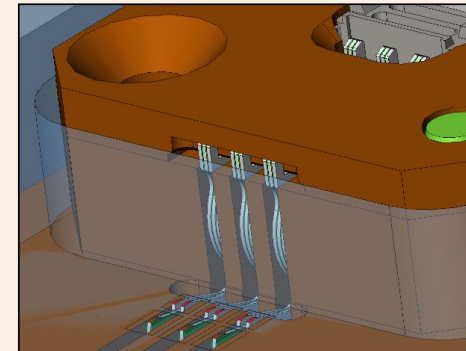
Upside-down Load Board Configuration



Conventional setup



Upside-down setup



- Turret Handlers are optimized to run at very high UPH
 - mounting the PCB on top of the socket creates a z-plunge reduction which assures a short index time < 50ms
- Upside-down load board configuration helps to exchange the PCB within minutes and eliminates time consuming contactor fine tuning

Conclusion

- New multi-beam released to the market and confirmed favorable performance multiple customers
- Outstanding lifetime and ease of use have significantly reduced cost of test and increased the efficiency of the test cell
- Multi-beam concept does have the potential to be applied for RF and Power final test and wafer level applications