



Burn-in & Test Socket Workshop

March 6-9, 2005
Hilton Phoenix East / Mesa Hotel
Mesa, Arizona

ARCHIVE

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**Burn-in & Test
Socket Workshop**

Technical Program

Session 1

Monday 3/07/05 8:30AM

MAKING BETTER CONTACT

“Enhanced High Strength/High Conductivity Copper-Beryllium Strip For Demanding BiTS Applications”

John C. Harkness - Brush Wellman Inc.

“Challenges Of Contacting Lead-Free Devices”

Brian William Sheposh – Johnstech International

“Application Of Socket Cleaning And Contact Restoration To Reduce Burn-In, Test & Device Programming Cost”

Erik Orwoll – Nu Signal LLC Jason Hughes – IBM Microelectronics

Enhanced High Strength/ High Conductivity Copper-Beryllium Strip for Demanding BiTS Applications

**John C. Harkness FASM
Brush Wellman Inc.**



**2005 Burn-in and Test
Socket Workshop
March 6 - 9, 2005**

Outline

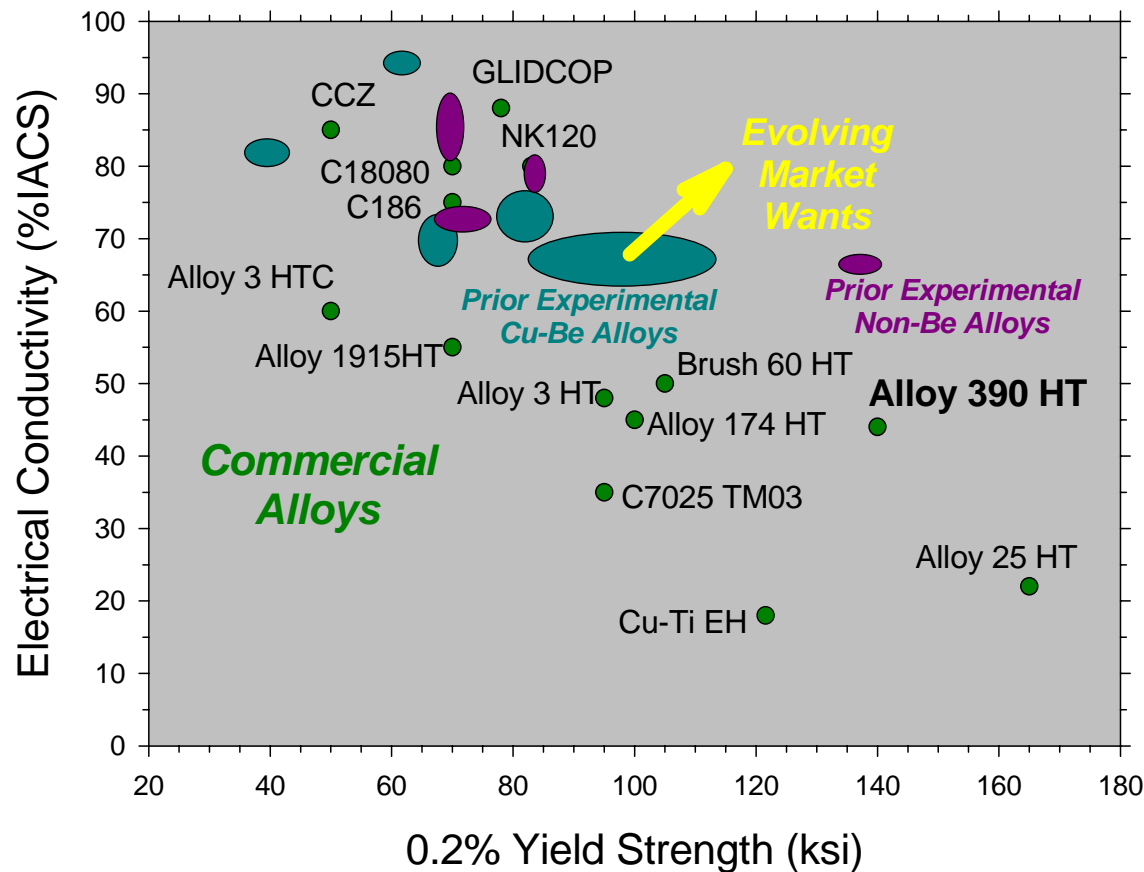
- BiTS -- materials challenges
- %IACS vs. YS in Cu alloys ... then & now
- Brushform 65TM & Alloy 390TM
 - Product development methodology
 - Chemistry, mechanical/physical props
 - Conductivity vs. T
 - Stress relaxation
- Alloy comparisons
- BiTS applications feedback
- Summary

BiTS Materials Challenges

- Driving Forces
 - Larger wafers, smaller pitch, higher pin count, shorter contacts create new problems in ...
 - Fabrication
 - Co-planarity
 - Compliance
 - Thermal management
 - Higher power/lower voltage
 - Long socket life (cycles)
 - Performance stability
- Base Metal Requirements
 - High yield strength
 - Moderate elastic modulus
 - Good formability
 - High electrical & thermal conductivity
 - Good stress relaxation resistance
 - Good fatigue strength
 - Low/uniform residual stress

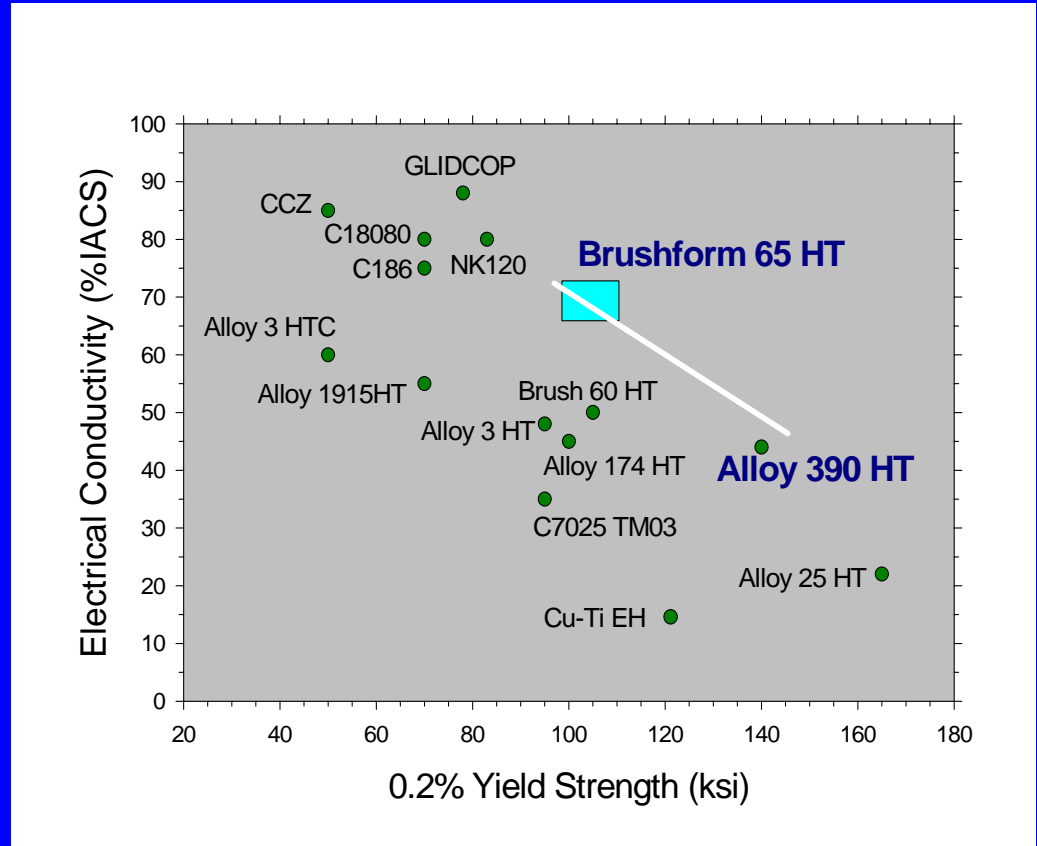
Historical Conductivity vs. Strength Relationships in Cu Alloys

Inescapable Rule: %IACS varies *INVERSELY* with strength
[but, the "frontier" has advanced with each new generation of materials]



A New Shift in the %IACS vs. YS Frontier

- **Brushform 65TM HT Strip**
 - Strength & formability of prior high performance Cu-Be alloys (Alloy 3, Brush 60TM, Alloy 174TM)
 - **Net 15-20 %IACS greater electrical conductivity**
- **Alloy 390 HTTM Strip**
 - Conductivity of prior high performance Cu-Be alloys
 - **Nominal 40 ksi higher YS**
- **Existing UNS Cu-Be chemistry & proprietary mill hardening processes**
 - *Consistent* properties & residual stress



Outputs of Brush Wellman's "Stage Gate" New Product Development Process

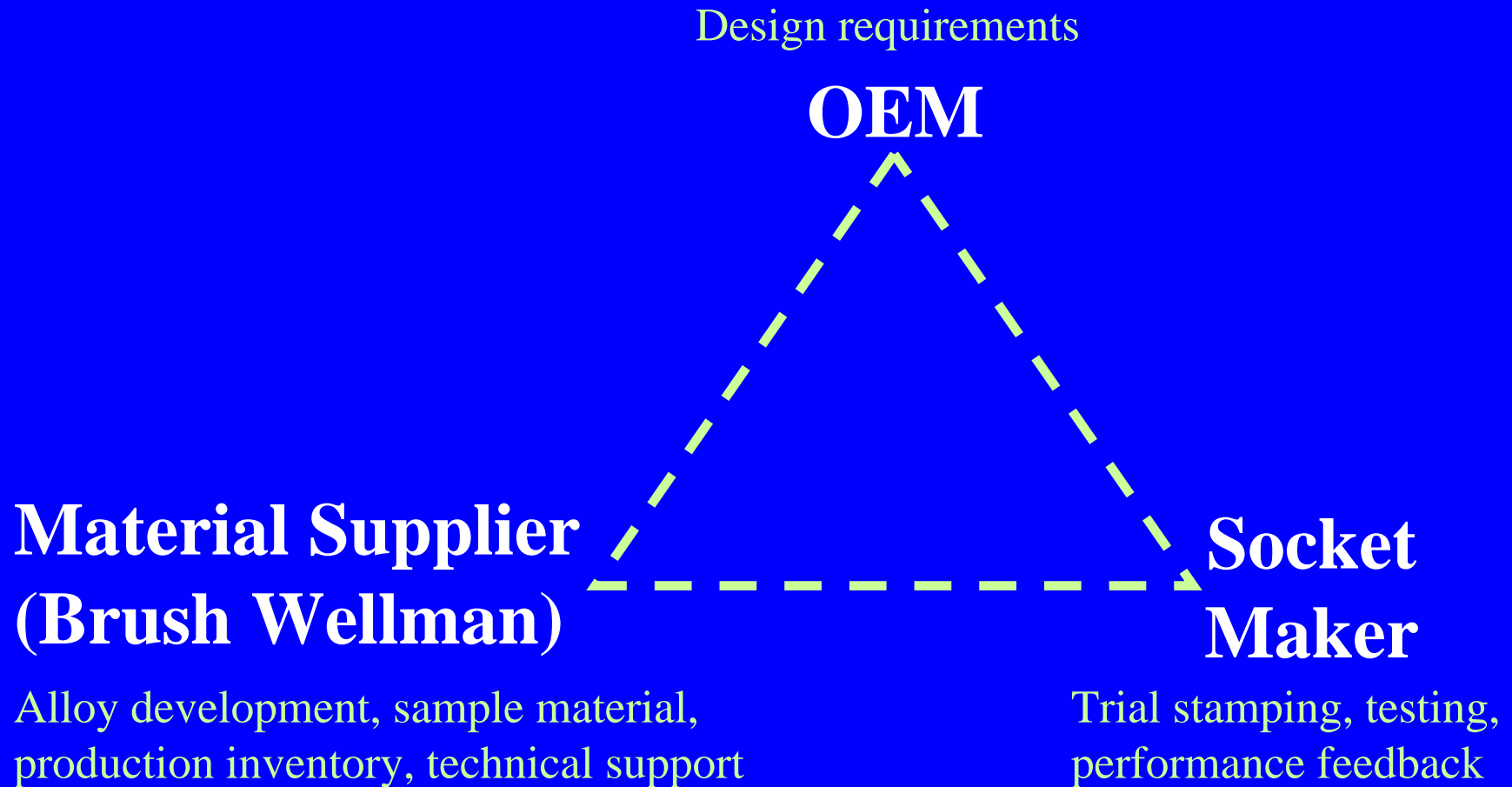
“Stage Gate” New Product Development Process (I)

- Identify a new competitive product with a good value proposition for the customer
- Market/customer focus
- Benchmark vs. competing & historical products
- Front-end planning
- Early & clearly defined product attributes
- Cross-functional team & champion

“Stage Gate” New Product Development Process (II)

- Work to company strengths
- Tough new product launch criteria
- Rigorous/disciplined process -- tough “go/no go” criteria
- Speed -- but not at expense of execution quality
- Detailed/high quality execution of each project phase

Partnering for Success in Next Generation BiTS (Harsh Environments)



Alloy 390™ HT

Data Sheet (I)

C17460 = (0.15-0.5)Be-(1.00-1.40)Ni-0.5maxZr-Cu

| <u>Physical Property</u> | <u>English Units</u> | <u>Metric Units</u> |
|------------------------------|--------------------------------------|------------------------|
| Density | 0.318 lb/in ³ | 8.81 g/cm ³ |
| Melting Range | 1975F–1880F | 1080C-1030C |
| Electrical Cond. (Room T) | 44 %IACS min. | 0.38 Megmho-cm |
| Thermal Cond. | 135 BTU/hr ft F (@ 200 F) | 235 W/mK (@ 100 C) |

Alloy 390™ HT

Data Sheet (II)

| <u>Mech. Property</u> | <u>English Units</u> | <u>Metric Units</u> |
|-----------------------|----------------------|---------------------|
| 0.2% YS | 135-153 ksi | 930-1055 MPa |
| UTS | 138-158 ksi | 950-1090 MPa |
| Elongation | 1% min | 1% min |
| Elastic Modulus | 20 msi | 138 GPa |
| Hardness (DPH) | 275-340 | 275-340 |
| 90 deg Bend* | 2 R/t GW & BW | 2 R/t GW & BW |

*** Up to 0.004 in. (0.10 mm) thick**

Brushform 65™

PRELIMINARY Data Sheet (I)

C17460 = (0.15-0.5)Be-(1.00-1.40)Ni-0.5maxZr-Cu

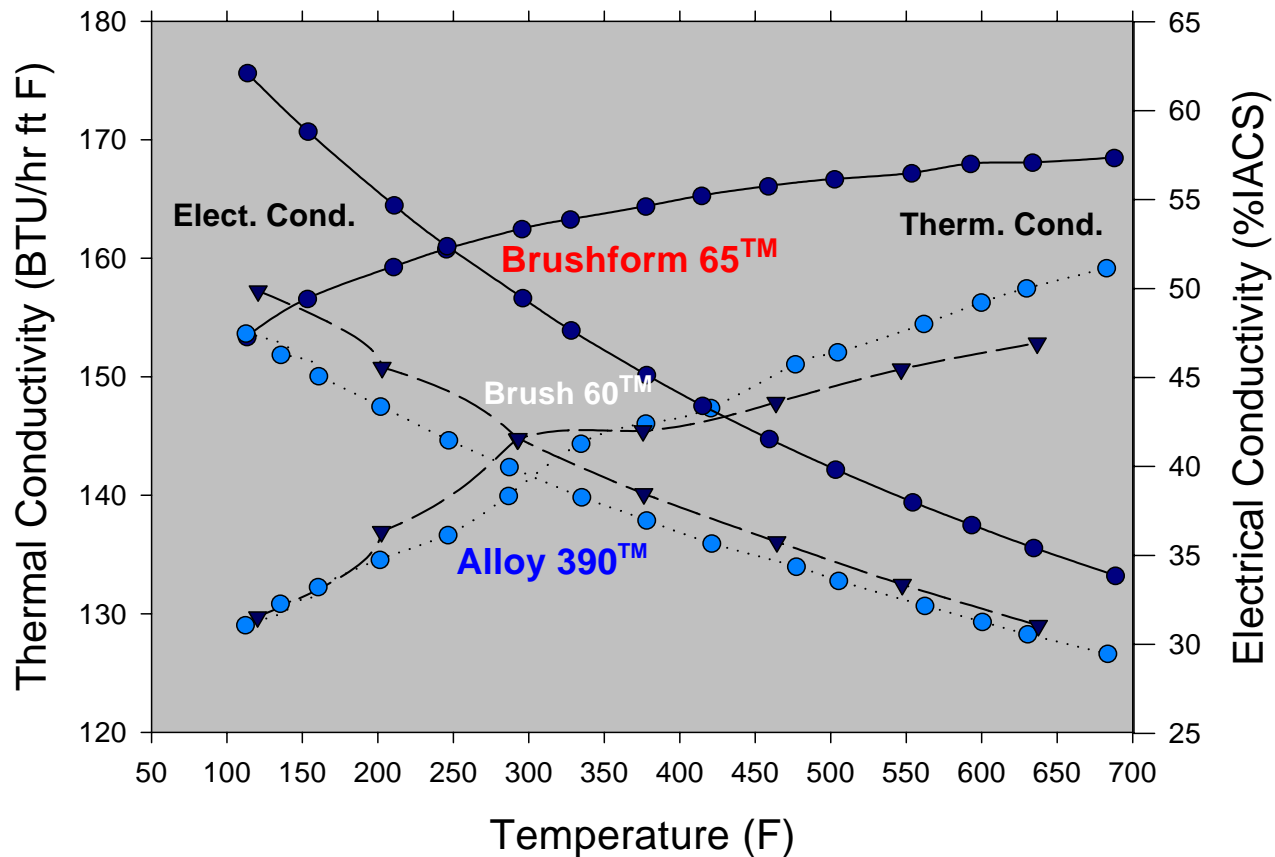
| <u>Physical Property</u> | <u>English Units</u> | <u>Metric Units</u> |
|------------------------------|--------------------------------------|------------------------|
| Density | 0.318 lb/in ³ | 8.81 g/cm ³ |
| Melting Range | 1975F–1880F | 1080C-1030C |
| Electrical Cond. (Room T) | 65 %IACS min. | 0.56 Megmho-cm |
| Thermal Cond. | 160 BTU/hr ft F (@ 200 F) | 275 W/mK (@ 100 C) |

Brushform 65™

PRELIMINARY Data Sheet (II)

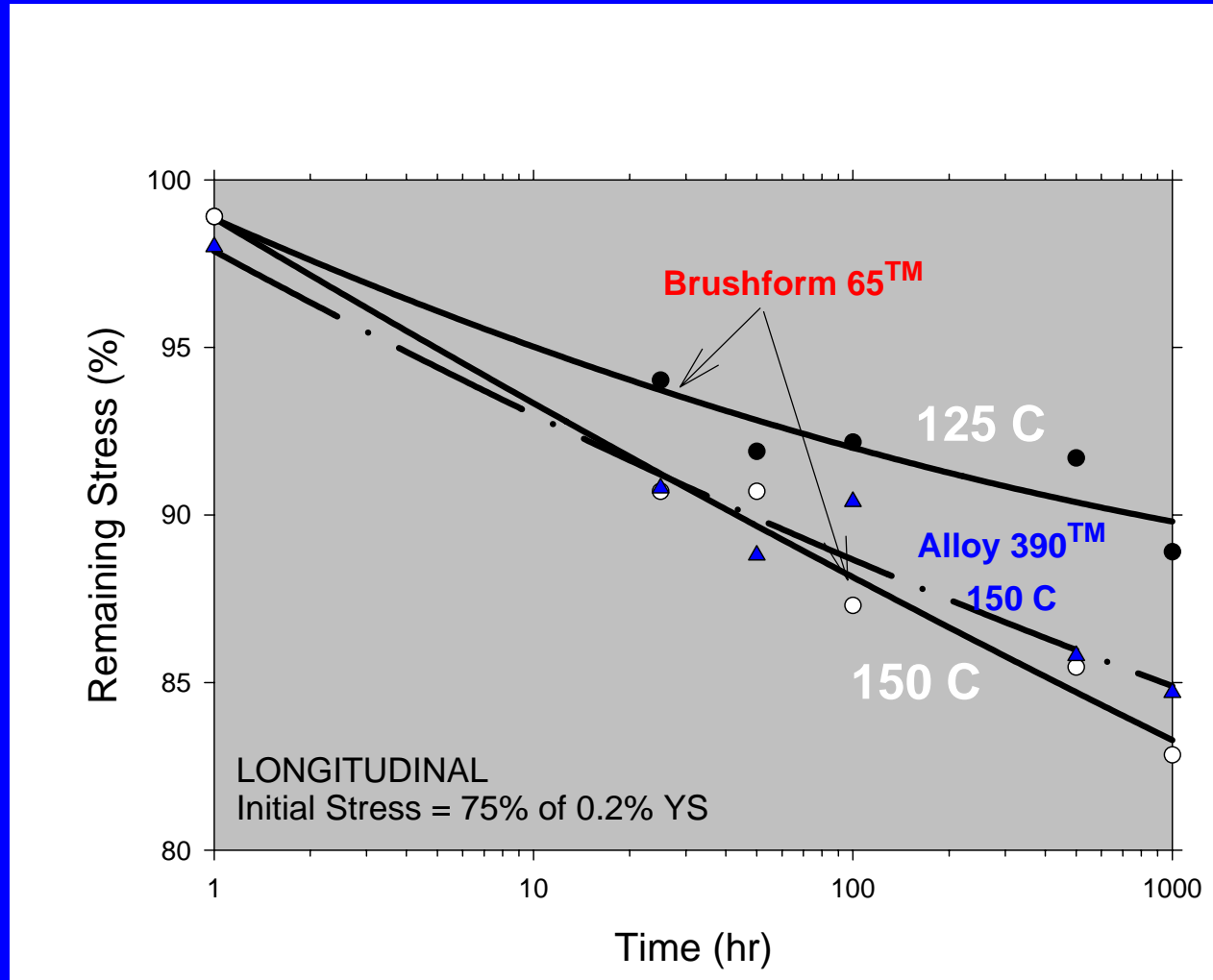
| <u>Mech. Property</u> | <u>English Units</u> | <u>Metric Units</u> |
|---------------------------------|----------------------|---------------------|
| 0.2% YS | 100 ksi min. | 689 Mpa min. |
| UTS | 110 ksi min. | 758 MPa min. |
| Elongation | 5% min. | 5% min. |
| Elastic Modulus | 20 msi | 138 GPa |
| Hardness | 225 DPH min. | 225 DPH min. |
| 90 deg Bend (Nom. 0.006 in.) | 1.3 R/t GW & BW | 1.3 R/t GW & BW |

Enhanced Electrical & Thermal Conductivity Brushform 65™ HT Strip



Good Stress Relaxation Resistance

Alloy 390™ & Brushform 65™



Alloys for Comparison

| <u>Alloy</u> | <u>0.2%YS (ksi)</u> | <u>El. Cond. (%IACS)</u> | <u>T Cond. W/mK</u> | <u>90 deg R/t (GW/BW)</u> | <u>150 C/1k hr (%RS)</u> |
|----------------------------------|-------------------------|------------------------------|-------------------------|-------------------------------|------------------------------|
| 190 HM | 110 | 17 | 105 | 2/2 | 74 |
| 3 HT | 95 | 48 | 238 | 2/2 | 85 |
| Brush 60 TM HT | 105 | 50 | 220 | 1.5/1.5 | 89 |
| Alloy 390 TM HT | 140 | 45 | 220 | 2/2 | 85 |
| Brushform TM 65 HT | 100 | 65 | 275 | 1.3/1.3 | 83 |
| C7025 TM02 | 85 | 35 | 170 | 2.5/2.5 | 88 |
| C199 EH | 114 | 12 | 55 | 2/6 | 98 |
| C18080 | 72 | 82 | 320 | 2/1 | >88 |

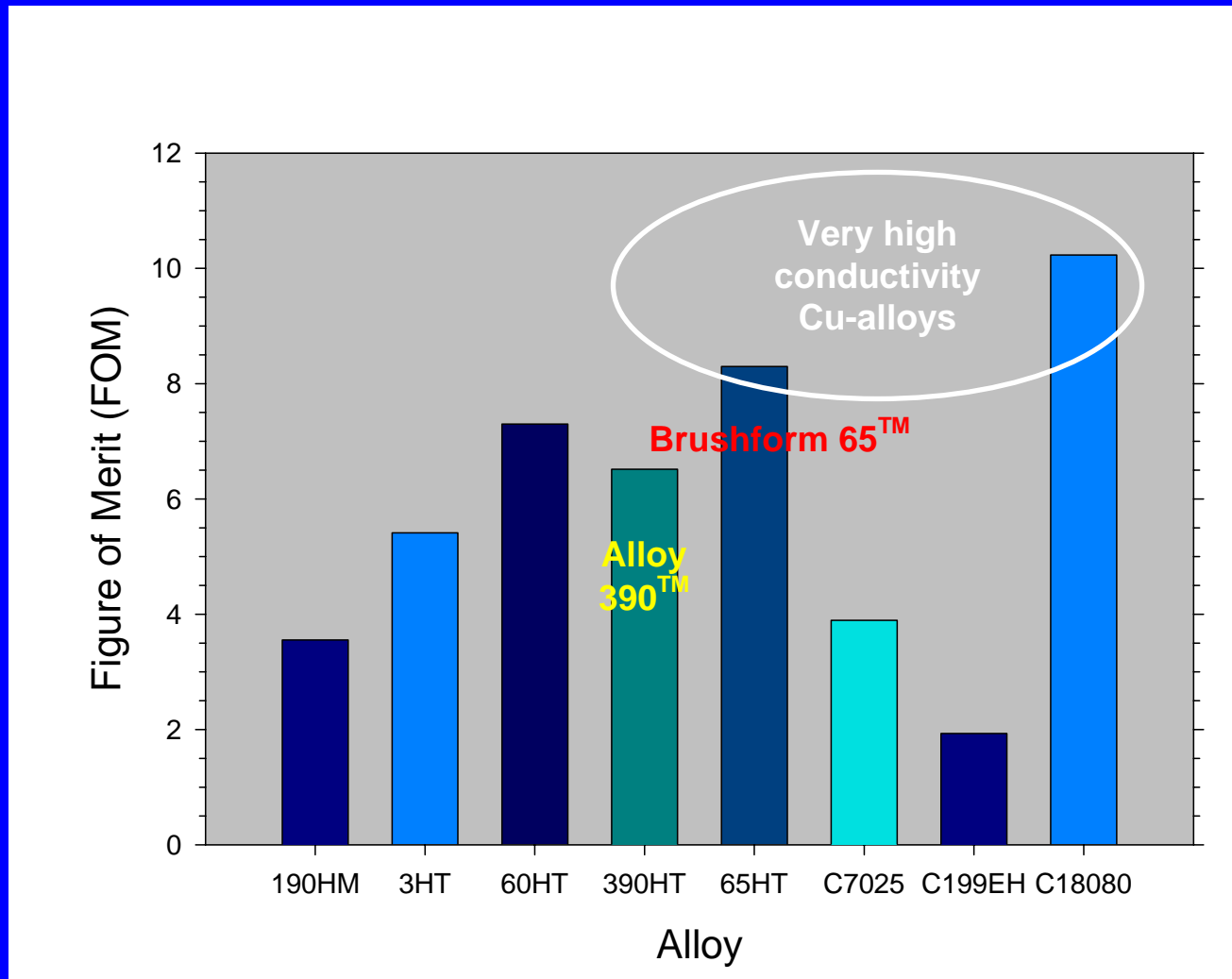
Non-Be alloy data from manufacturer's data sheet and/or sample exam

Connector Alloy Performance “Figure of Merit”

$$\text{FOM} = \frac{(\text{YS} + 2 \times \% \text{IACS}) \times \% \text{RS}}{(1 + \text{BWR}/t) \times 1000}$$

- **Numerator:** Increasing property value -- improves performance
- **Denominator:** Decreasing property value -- improves performance
 - “(1 + BWR/t)” enables 0 R/t value entry
 - “1000” = normalizing factor to keep FOM << 100

Alloy Comparison: “Figure of Merit”



Temperature Rise

- Function of the bulk resistivity of the material
- More important as contacts become smaller, with increased current carrying requirements

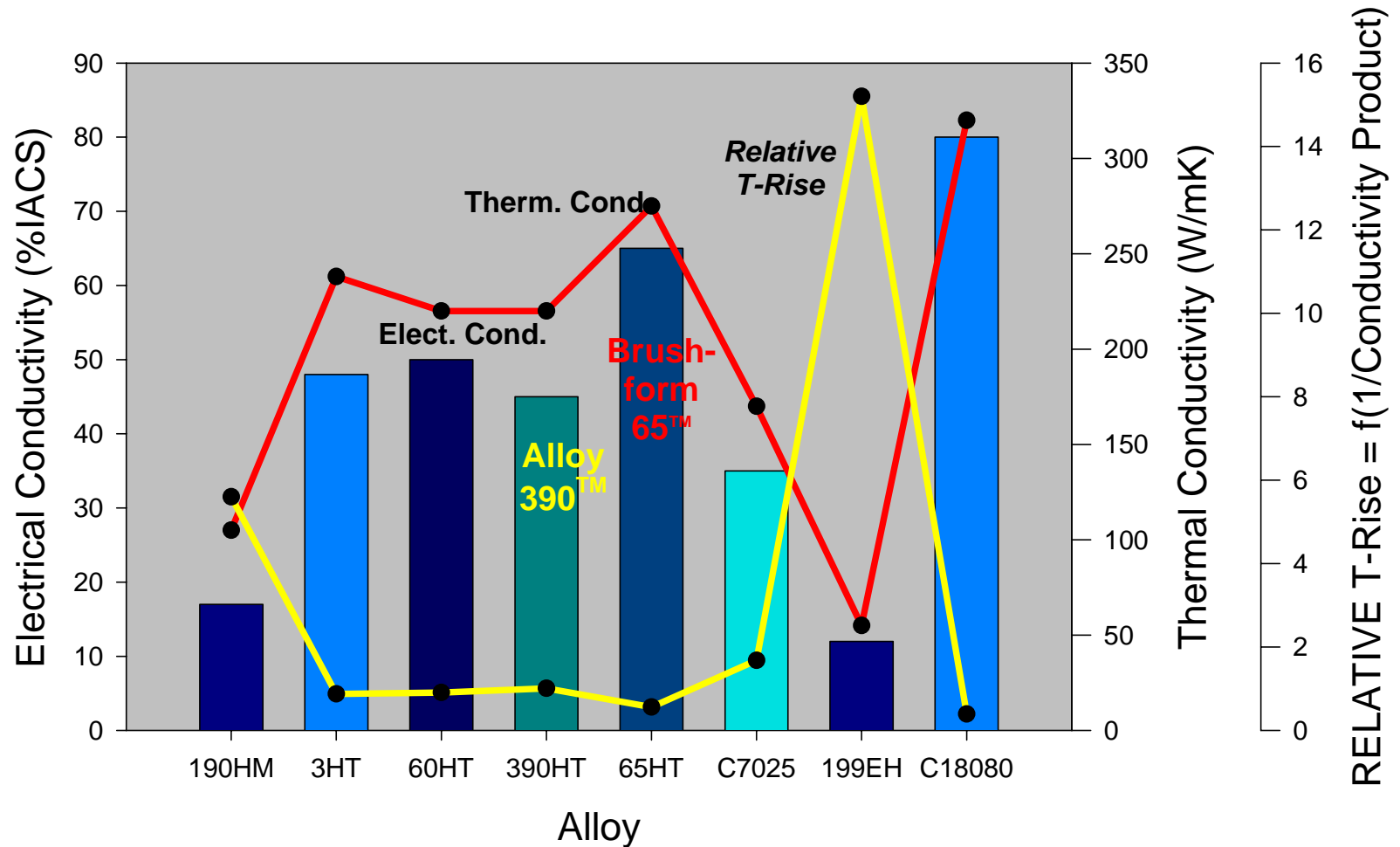
change in temperature

$$\Delta T = \frac{J^2 l^2}{2\gamma k A^2}$$

current
beam length
area
electrical conductivity
thermal conductivity
[Conductivity Product]

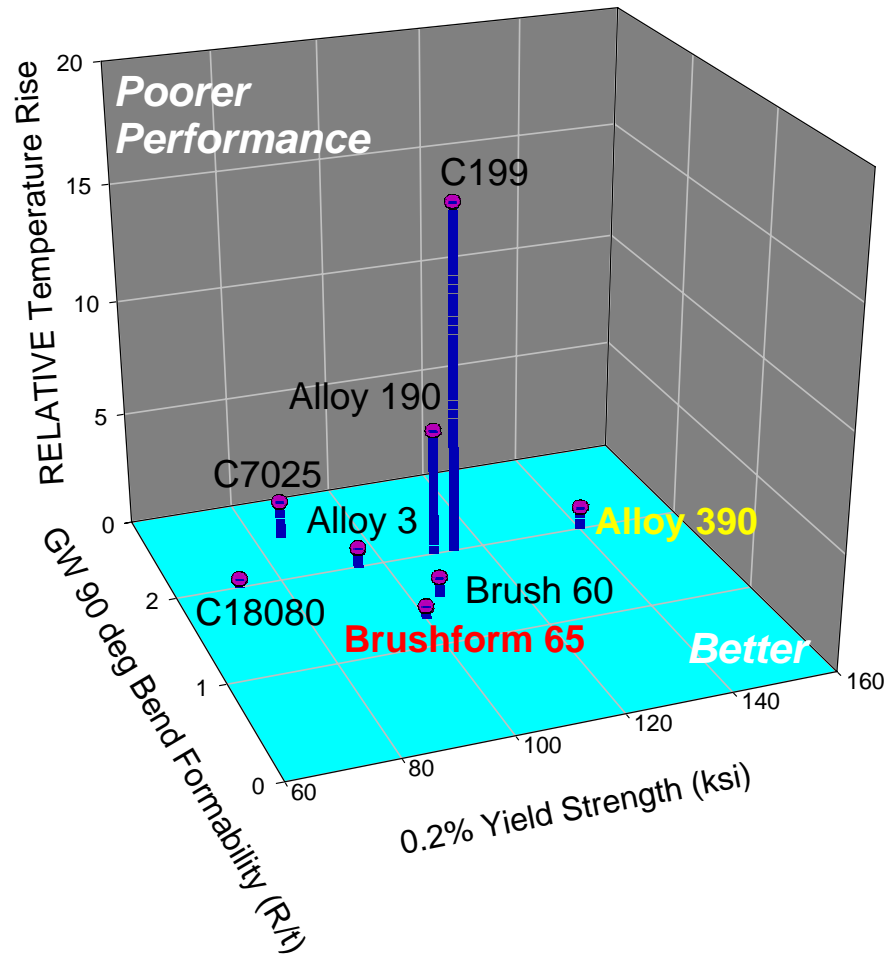
Does not take heat transfer via CONVECTION or RADIATION into account

Alloy Comparison: Relative T-Rise

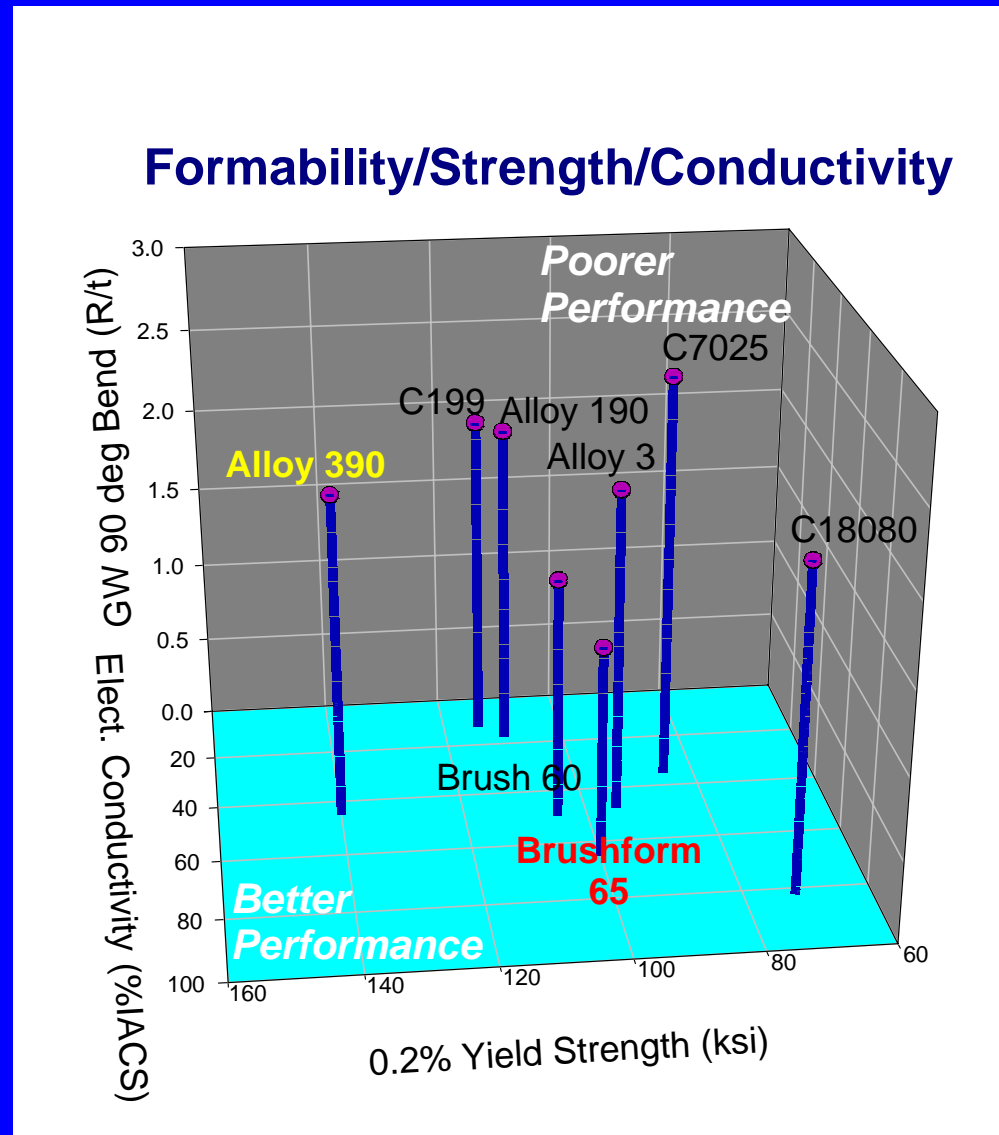


3-Attribute Comparison (I)

Relative T-Rise/Strength/Formability



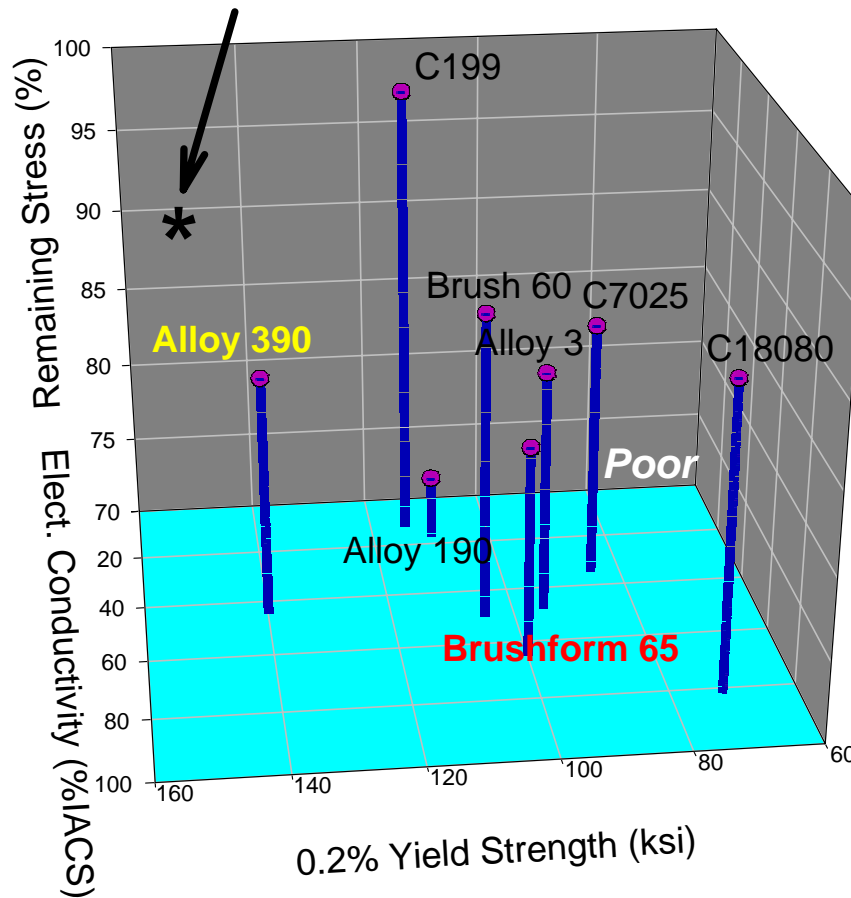
3-Attribute Alloy Comparisons (II)



3-Attribute Alloy Comparisons (III)

Stress Relaxation/Conductivity/Strength

Top Left Front Corner = Better



Alloy 390™ HT in BiTS

- “Proven technology” in on-going BiTS applications
 - LGA (strength)
 - **Low power** (44 %IACS)
 - But less T-rise than lower %IACS Cu-alloys
 - Meets demanding performance requirements
 - Mill hardened
 - No heat treat distortion issues
 - Uniform residual stress -- high stamping yield
 - Consistent strength/hardness
 - Meets higher spring force requirements
 - Passes increased cycle life test standards

Brushform 65™ in BiTS

- “Alpha customer” trials feedback (**POWER** apps.)
 - Stampability similar to other 100 ksi Cu-alloys
 - > 25% improvement in specific resistance vs. Alloy 390 (65 %IACS vs. 44 %IACS)
 - 14% increase in Amperage carried vs. Alloy 390
 - Improved **current carrying capacity**
 - Trial stamping in tooling for higher YS alloy unintentionally compromised mechanical performance
 - Different elastic springback (dimensional control)
 - Higher initial permanent set (minor design change could overcome -- offset by benefits of greater electrical performance)

Summary (I)

- **Brushform 65™ HT & Alloy 390™ HT** meet BiTS material challenges for demanding applications
 - Results of a rigorous “stage gate” New Product Development Process
 - Examples of OEM/Stamper/Supplier partnership for success in next generation BiTS for harsh applications
- Both alloys exhibit good stress relaxation resistance and provide desirable 3-attribute combinations
 - Relative T-rise/strength/formability
 - Formability/strength/conductivity
 - Stress relaxation/strength/conductivity

Summary (II)

- **Alloy 390™ HT** is a lean Cu-Be strip product with **enhanced strength** relative to traditional “high conductivity” Cu-Be alloys
 - Performance Figure of Merit > competitive non-Be Cu-alloys of similar or lower %IACS
 - Strength within the mill hardened “high strength” Cu-Be alloy range, with 44 %IACS minimum
 - Established in on-going LOW POWER BiTS applications
 - Consistent residual stress & strength, high cycle life

Summary (III)

- **Brushform 65™** is a new lean Cu-Ni-Be strip product with **enhanced conductivity/strength combination** relative to all other Cu-base connector alloys
 - Performance Figure of Merit in the same league as competitive very high conductivity Cu alloys
 - High “conductivity product” = low temperature rise
 - BiTS application trials (HIGH CURRENT/POWER)
 - Good stampability
 - Improved specific resistance & current carrying capacity vs. Alloy 390™
 - NO insurmountable mechanical performance issues

Challenges of Contacting Lead-Free Devices

2005 Burn-in and Test Socket Workshop

March 6 - 9, 2005



Brian William Sheposh
Johnstech International

Discussion Topics

- **Defining Interconnect Success**
- **Lead-free Material Trends and Applications**
- **Specifics of Lead-Free Alloys**
- **The Impact on Interconnect Success**
- **Conclusion: Achieving Interconnect Success**

Interconnect Success

- **Goal: Minimize and sustain the junction resistance between the device lead and contact.**

$$R_{\text{total}} = R_c + R_{\text{film}}$$

Constriction

$$R_c \propto F^{-1/2} \text{ (force)} ; R_c \propto \rho_{\text{tip}} \text{ (plating)}$$

Film

$$R_{\text{film}} \gg R_c \text{ (oxide, debris)}$$

Challenges to Interconnect Success

- Maintaining bias throughout product life. $R_c \propto F^{1/2}$
- R_{film} develops on the surface of the contact over insertion (debris and oxide). $R_{\text{film}} \gg R_c$
- Wear of the contact tip can compromise the interconnect integrity:
 - $R_c \propto \rho_{\text{tip}}$
 - $R_c \propto F^{1/2}$
- Plating (contact under-plate metallic oxidizes)
- Function (wipe, piercing, etc.)

Industry Lead-Free Trends

- **Leaded and Pad Packages**
 - Matte Sn
 - NiPd ; NiPdAu
 - SnBi
 - Au
- **Ball Grid Array Packages (BGA)**
 - $\text{SnAg}_{3.0-4.0}\text{Cu}_{0.5}$

Challenges in the Field

- **Matte Sn**
 - Customers see faster rise in resistance which leads to more frequent cleaning when compared to SnPb.
 - Reduced contact life has been observed vs. SnPb, but not as great as with NiPdAu.
- **NiPdAu**
 - Customers observe good contact resistance until the contact plating wears, which promotes a drastic drop in 1st pass yields.
 - Contact life is much less when testing NiPdAu vs. Sn Pb.

Qualification of Interconnect Success

- Contactors Designs
- **BGA Contactor**
 - $\text{Sn}_{63}\text{Pb}_{37}$ eutectic
 - $\text{Sn}_{95.5}\text{Ag}_{4.0}\text{Cu}_{0.5}$
- **Pad Contactor : ROL200 Design**
 - $\text{Sn}_{90}\text{Pb}_{10}$
 - Matte Sn_{100}
 - NiPdAu

Qualification of Interconnect Success

- **Contacts were populated into a contactor and mounted to a test board.**
- **Force Testing: Contact force was measured in real-time as devices were inserted into the contactor.**
- **Resistance Testing: The test board and devices were designed so that four-point Kelvin resistance measurements were made across pairs of contacts throughout the contactor.**

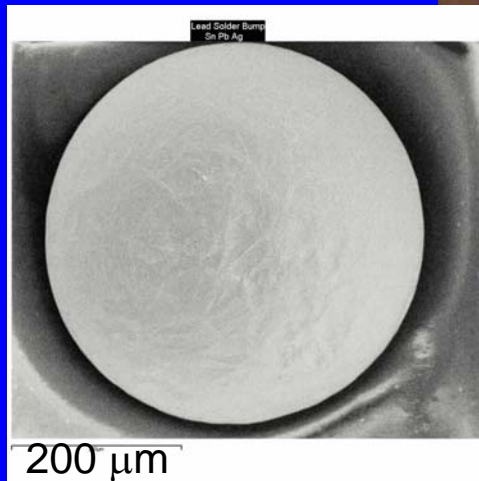
Qualification of Interconnect Success

- **Resistance Testing cont.:** Packaged devices were cycled through the contactor and Kelvin resistance measurements were recorded:
 - BGA Devices: Each device was cycled ten times with resistance readings at the first and sixth insertion (reduce cost)
 - Pad Devices: Each device was cycled only once, insuring virgin plating material on each insertion.

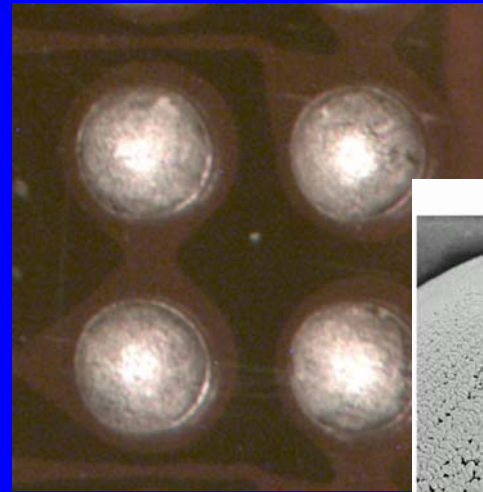
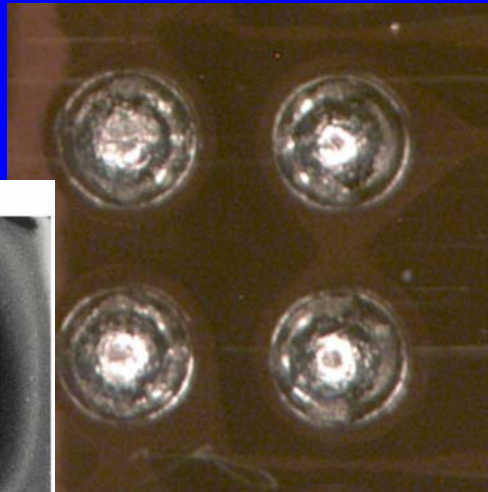
SnAgCu Balls

Physical Appearance

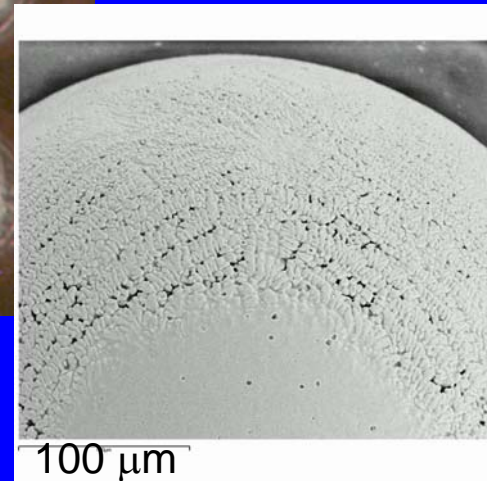
- A dull, grainy, matte finish on the SnAgCu balls due to the formation of pure Sn dendrites on the surface of the ball.



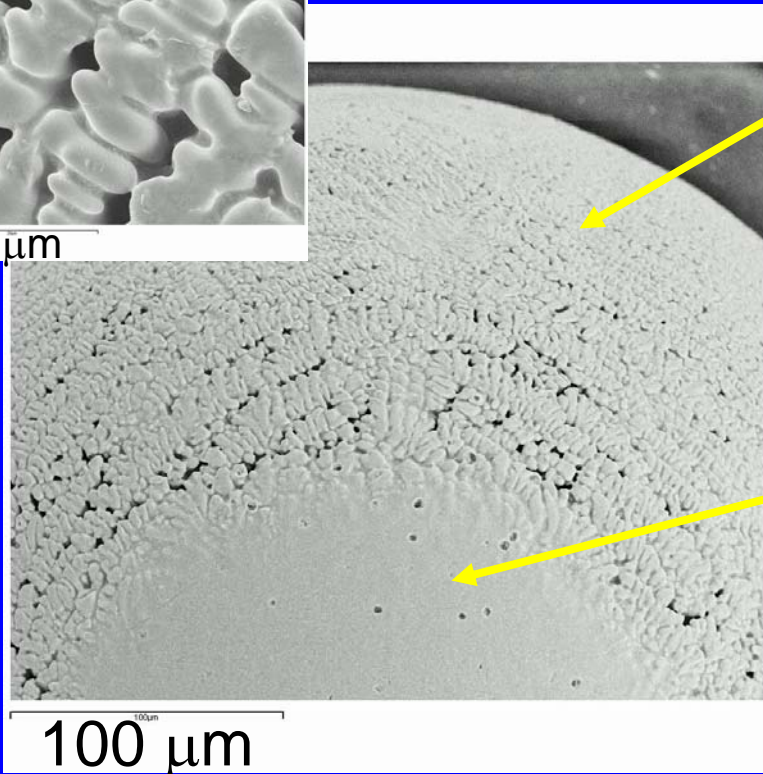
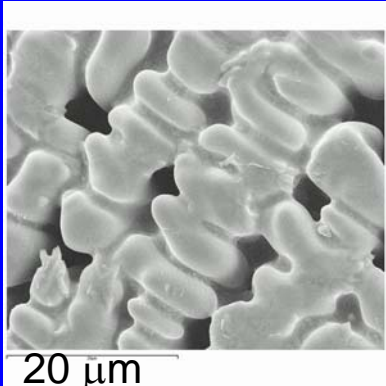
SnPb



SnAgCu



EDS Spectrum of Dendrite Rich Regions - SnAgCu Balls



Average composition
in dendritic rich region

Sn 99.8%

Cu 0.2%

Ag <0.1%

Average composition
in non-dendritic region

Sn 96.1%

Cu 2.3%

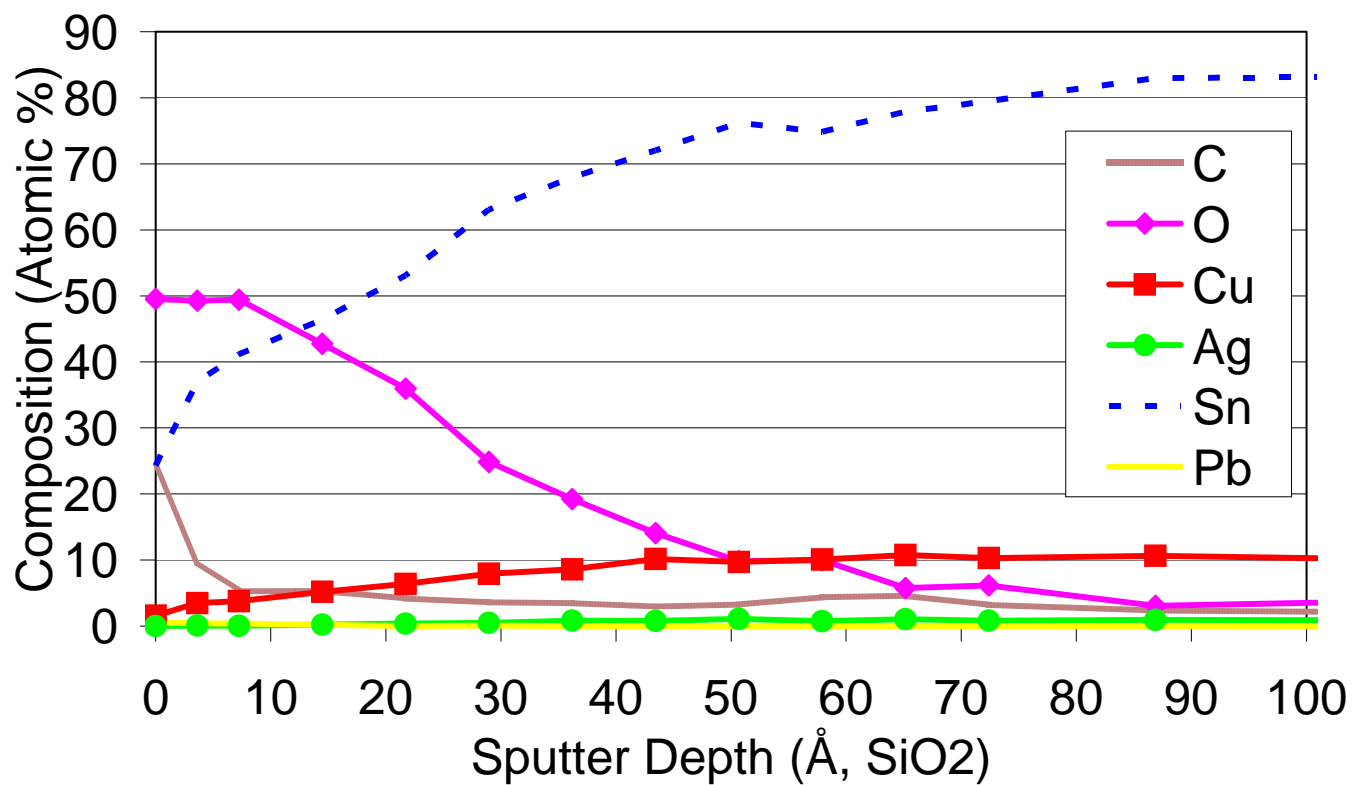
Ag 1.6%

XPS Analysis of SnPb and SnAgCu Balls

- XPS: X-Ray Photoelectron Spectroscopy
- A beam of x-rays was focused on the sample surface, which generates photoelectrons that are energy analyzed and counted.
- The atomic composition and chemistry of the sample surface can be determined from the emitted photoelectrons.
- Oxide thickness was defined as the depth at which the oxygen concentration fell to 50% of its peak value.

XPS Analysis of SnAgCu Balls

Composition vs. Sputter Depth for SnAgCu Ball



Oxide Depth
 $\approx 29\text{\AA}$

$\text{\AA} = 10^{-10}$

angstrom

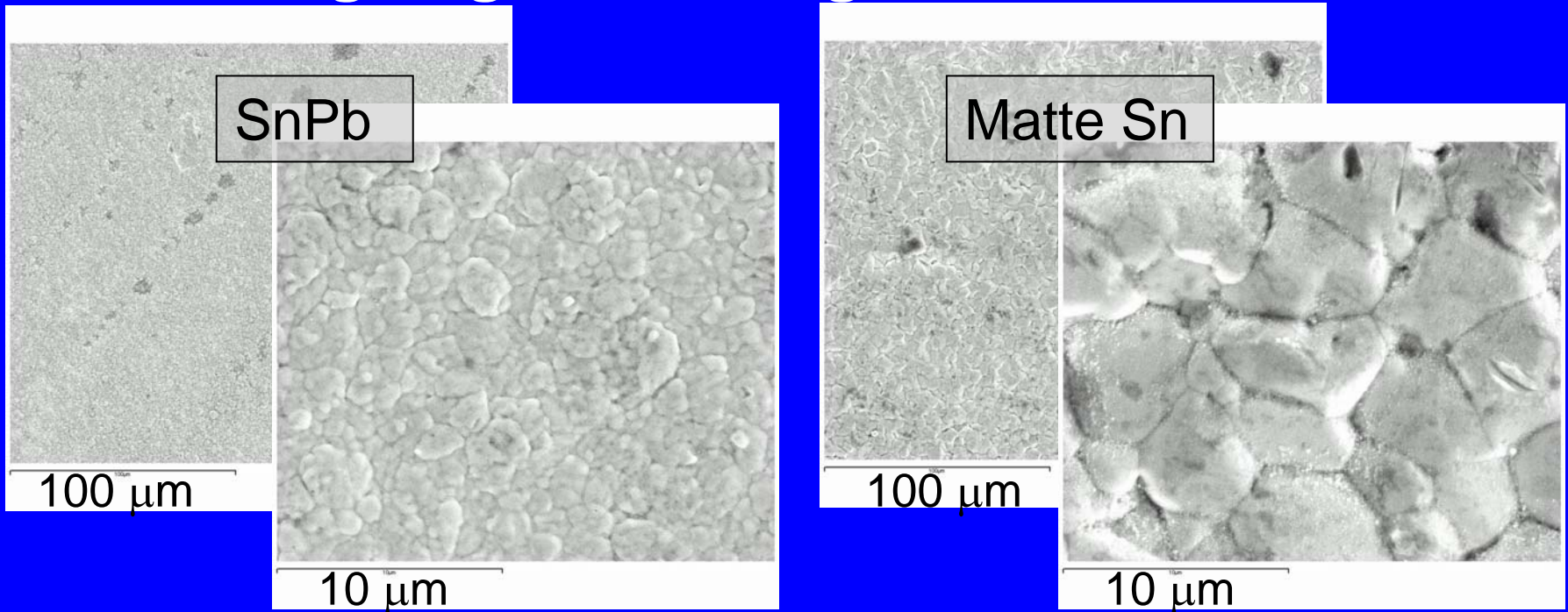
XPS/SEM Analysis of SnPb and SnAgCu Balls

- **Conclusions From XPS and SEM:**
 - Both SnPb and SnAgCu had Sn oxide dominated layers of approx. 29Å.
 - Surface roughness of the SnAgCu was much greater than that of SnPb and caused by pure Sn dendrites.
 - No Sn dendritic growth was observed with SnPb balls.

Matte Sn Pad

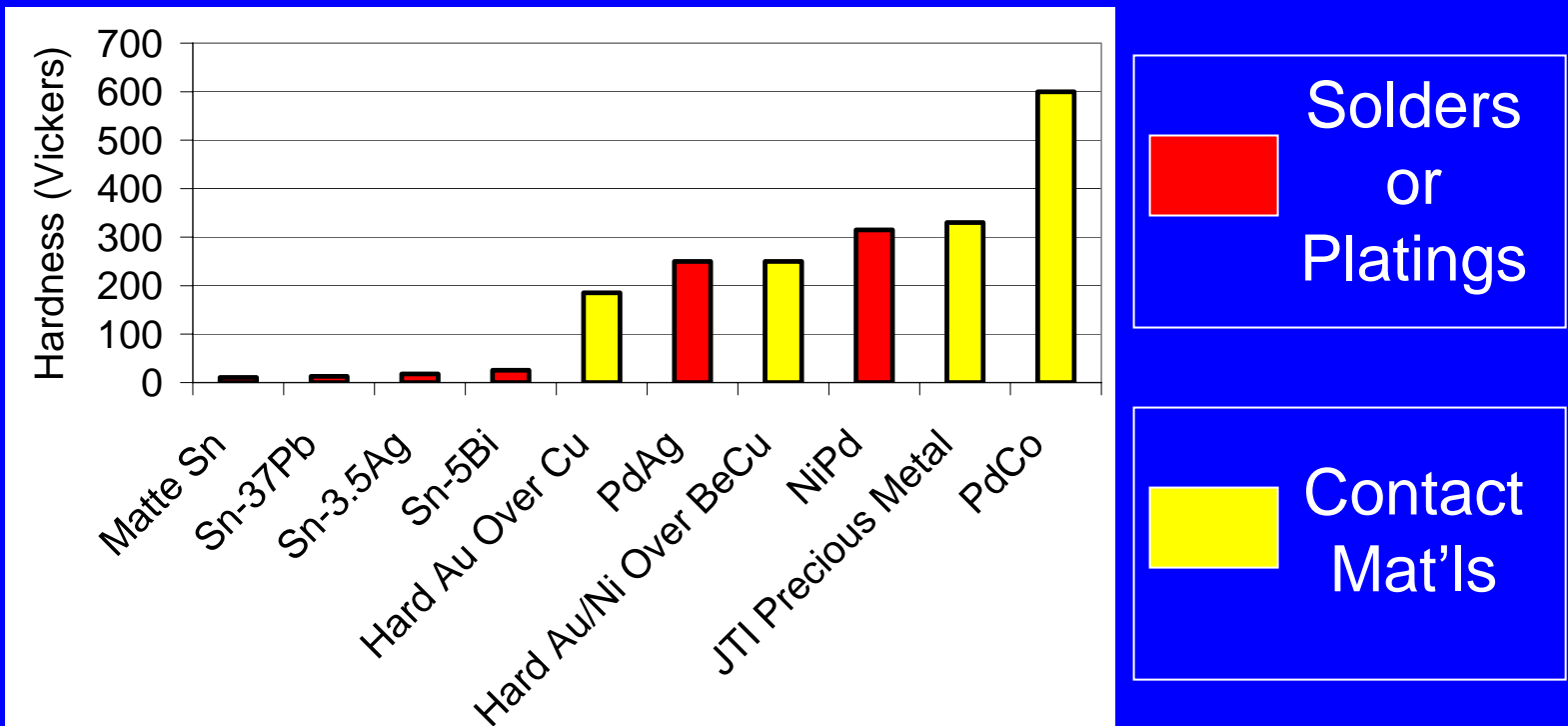
Physical Appearance

- Matte Sn pad surfaces were observed having large, Sn-rich grains.

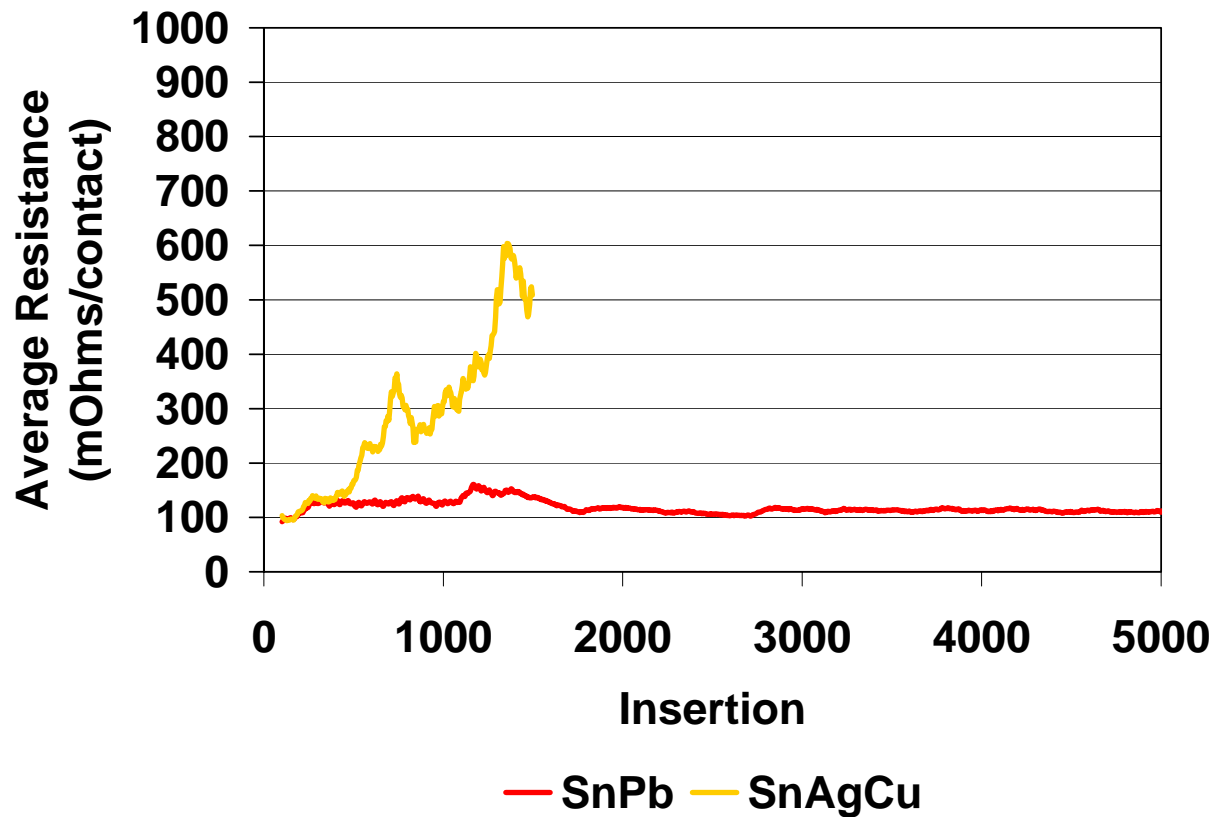


NiPdAu Pad Properties

- NiPdAu plating is approximately 20x harder than standard solder alloys.



SnPb vs. SnAgCu BGA Resistance Performance



Approximate
Force = 17gm

SnPb

Avg = 118m Ω

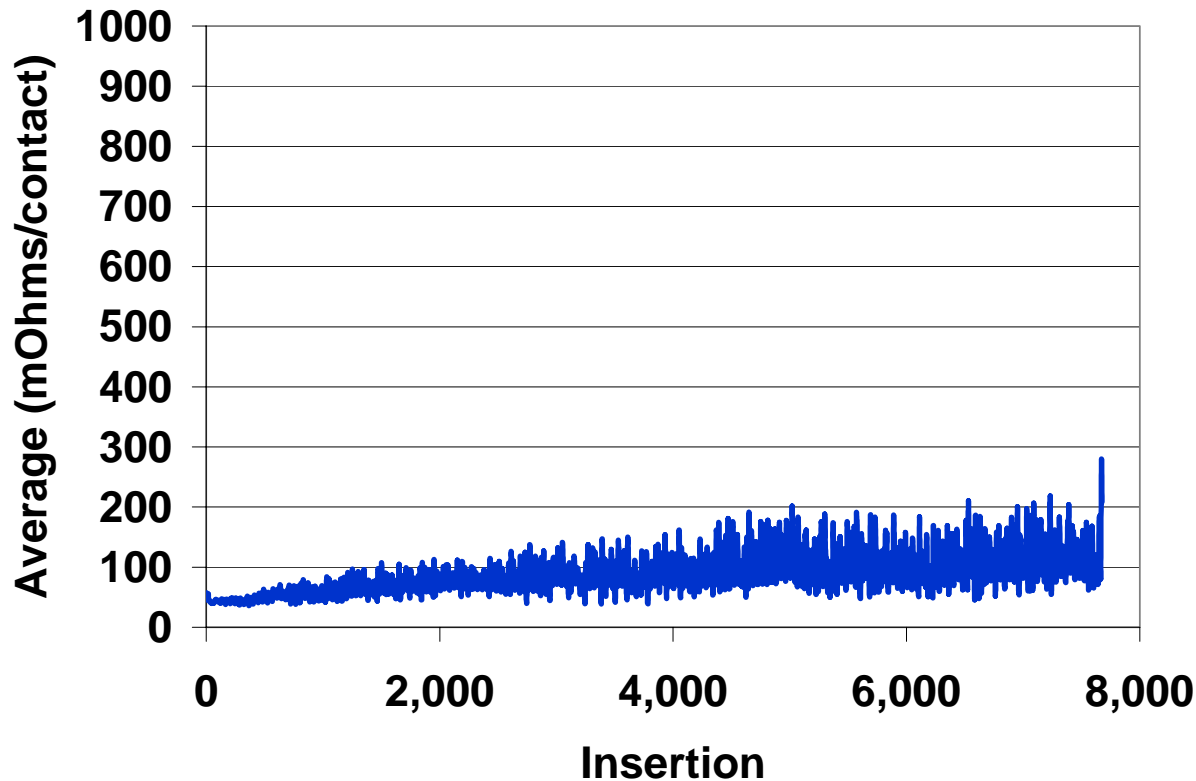
Stdev = 43m Ω

SnAgCu

Avg = 389m Ω

Stdev = 490m Ω

Increased Force BGA SnAgCu Resistance Performance



Approximate
Force = 50gm

SnAgCu

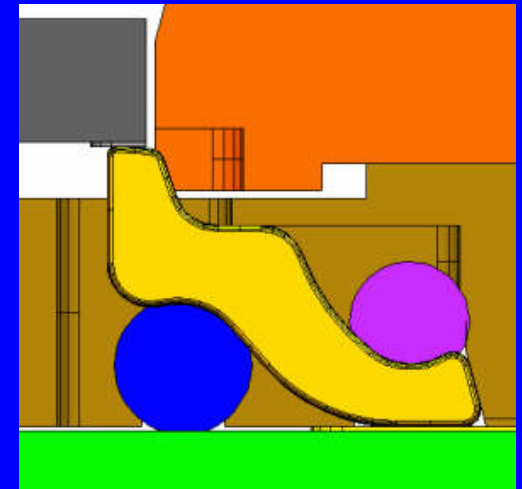
Avg = 91m Ω

Stdev = 47m Ω

Matte Sn and NiPdAu Qualification

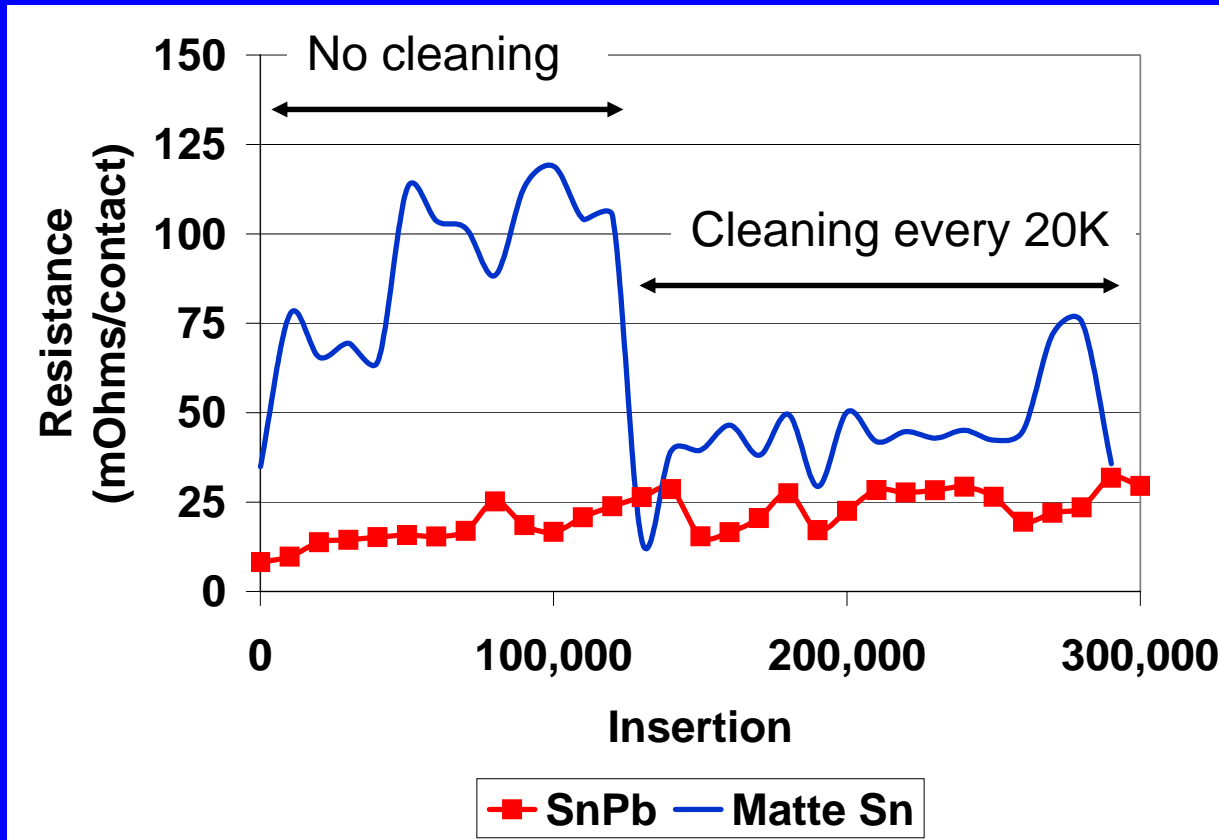
Pad ROL200 Design

- Utilizes non-plated contact of hardness >350 Vickers, with two elastomers to create device and load board bias.
- Tangential scrub action on the device. Contact rolling action on the load board.
- Manufactured for testing with:
 - 48QFN07-0.50



SnPb vs. Matte Sn Pad ROL200

Resistance Performance



Sn: No Clean

Avg = 92m Ω

Stdev = 43m Ω

Sn: Clean @ 20K

Avg = 48m Ω

Stdev = 35m Ω

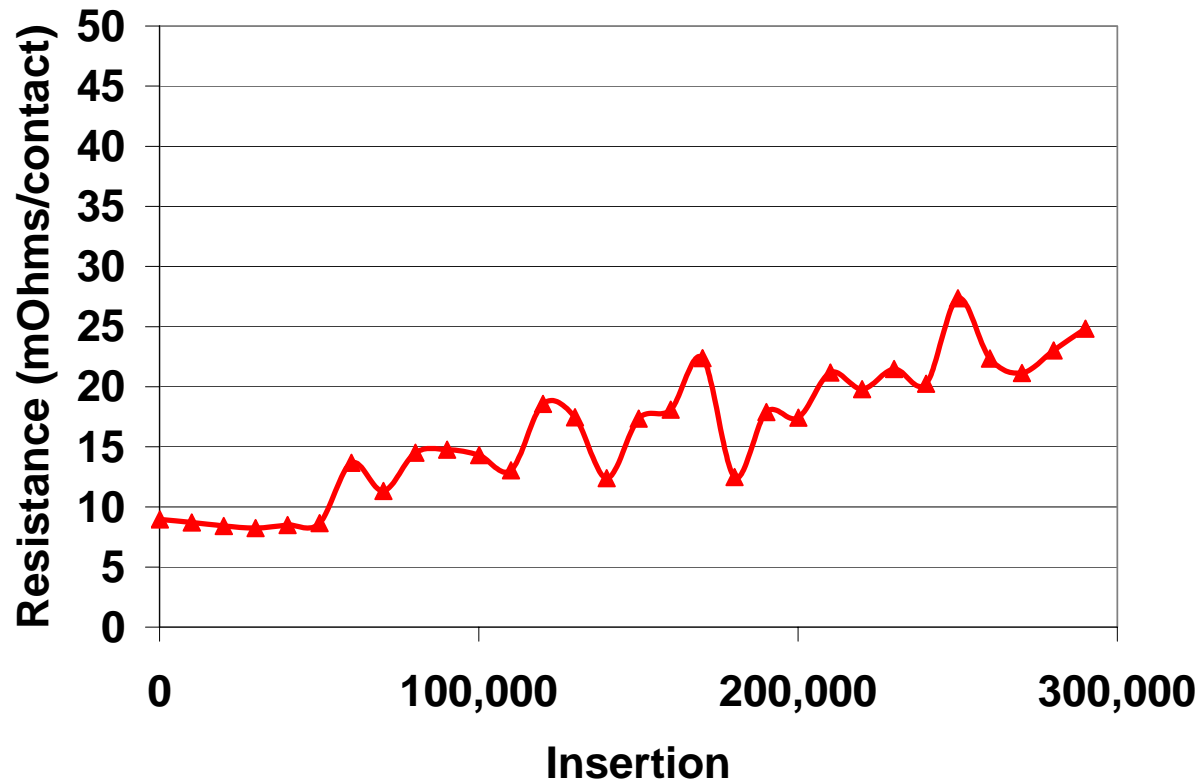
SnPb - No Clean

Avg = 28m Ω

Stdev = 5m Ω

NiPdAu Pad ROL200

Resistance Performance



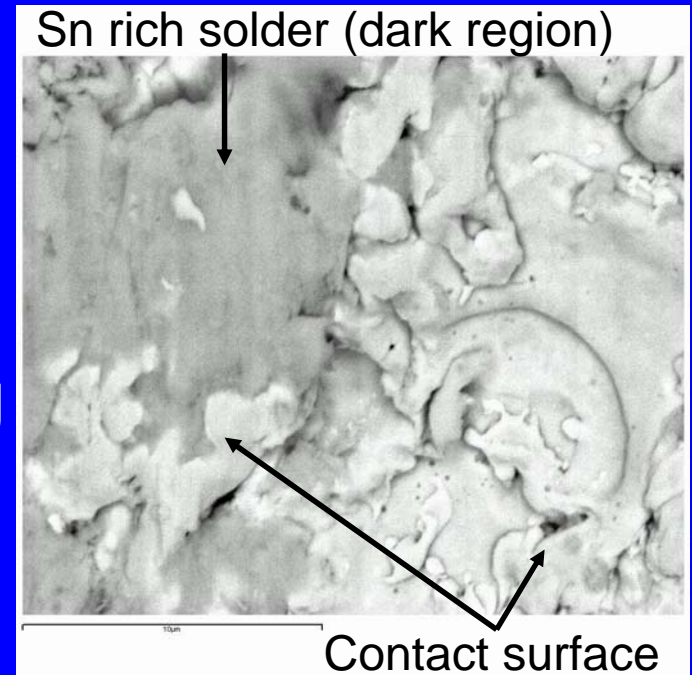
NiPdAu
Avg = 16m Ω
Stdev = 12m Ω

Conclusions

- SnAgCu Evaluation
 - Sn rich solder smears in the contact surface over insertion, creating resistance rise.

$$R_{\text{film}} \gg R_C$$

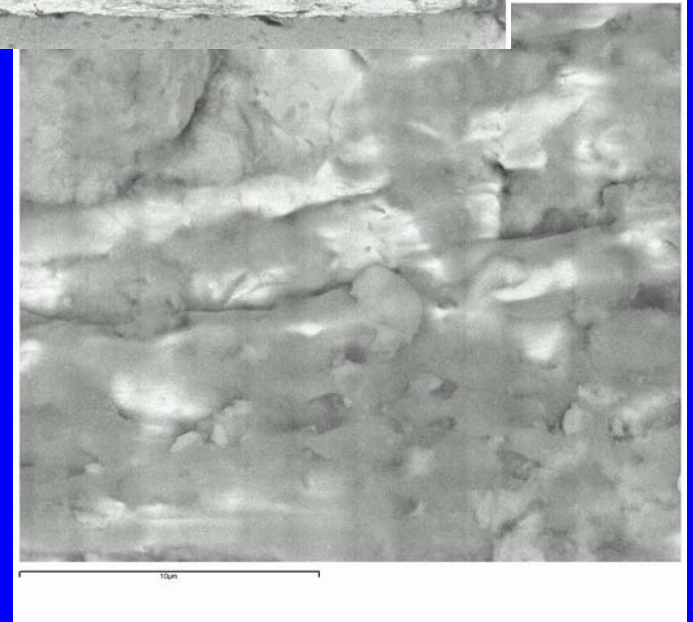
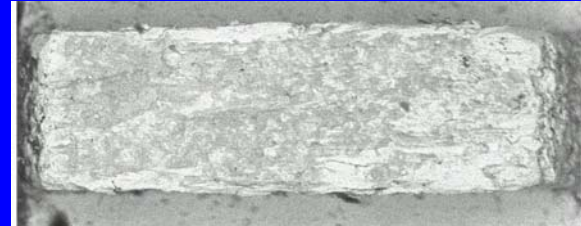
- Increase in force, combined with a self-cleaning function aids in maintaining of nominal resistance performance.



Conclusions

- Matte Sn Evaluation

- Pure Sn tend to smear and cover the contact surface. $R_{\text{film}} \gg R_C$
- A prescribed cleaning cycle aids in maintaining low resistance values, while promoting long contact life.



Conclusions

- NiPdAu Evaluation

- Debris/oxide presence was not detected and does not pose a problem to resistance performance. Cleaning wasn't necessary during this test.
- Wear on un-plated contacts will reduce the force over insertion, thus increasing the variation in contact resistance.

$$R_c \propto F^{-1/2}$$

Proposition for Interconnect Success

- **SnAgCu and Matte Sn (Maintain Low R)**
 - The right combination of force and self-cleaning scrub eliminate Sn build-up on the contacts which will reduce cleaning frequency. (Reduce down time)
- **NiPdAu (Promoting Long Life)**
 - Un-plated contacts with material hardness of >350 (Vickers) to ensure improved contact life.

Future Work

Understanding Sn

- **The mechanism for the increase in resistance due to the matte Sn pads and SnAgCu balls needs to be understood.**
- **An increase in force may reduce the need to clean as frequently, but also may reduce contact life.**

Application of Socket Cleaning and Contact Restoration to Reduce Burn-In, Test & Device Programming Cost

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Erik Orwoll - Nu Signal LLC
Jason Hughes - IBM Microelectronics

Interconnect Restoration

- ❖ *Solder Contamination*
- ❖ *Interconnect Failure*
- ❖ *Yield & Capacity (Production) Loss*
- ❖ *Restoration Process & Results*

Interconnect Restoration

Process Applied To

Burn-In Boards

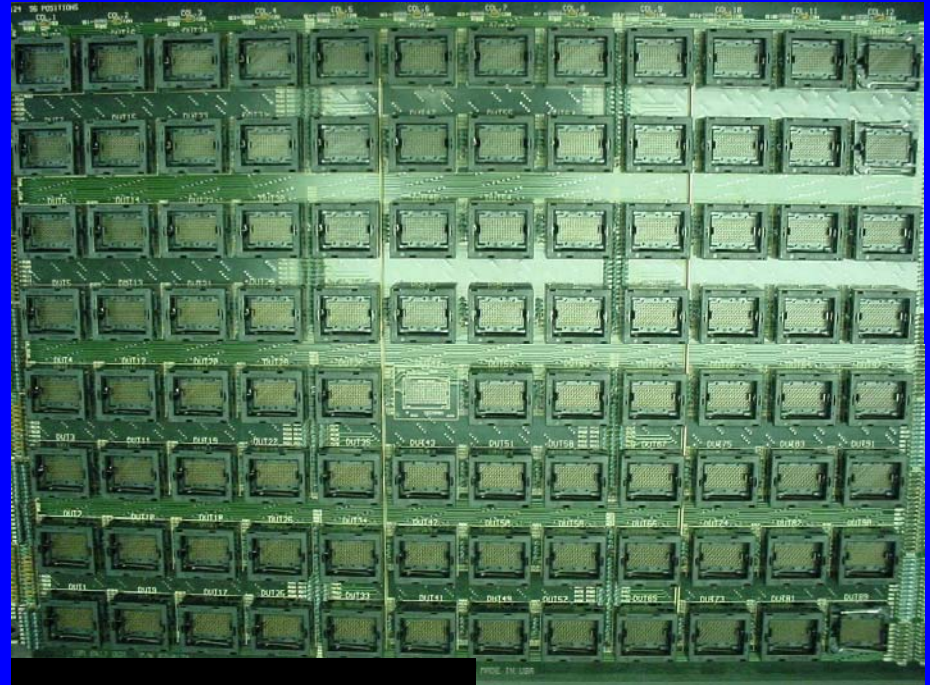
Test Sockets: Pogo Pins (Spring Probes)

Programming Sockets

Burn-In

Board Stats:

- 96 Socket Positions
- 153 Pin BGA
- Pinch Style Contact
- Auto Load – Open Top



Burn-In: Solder Contamination



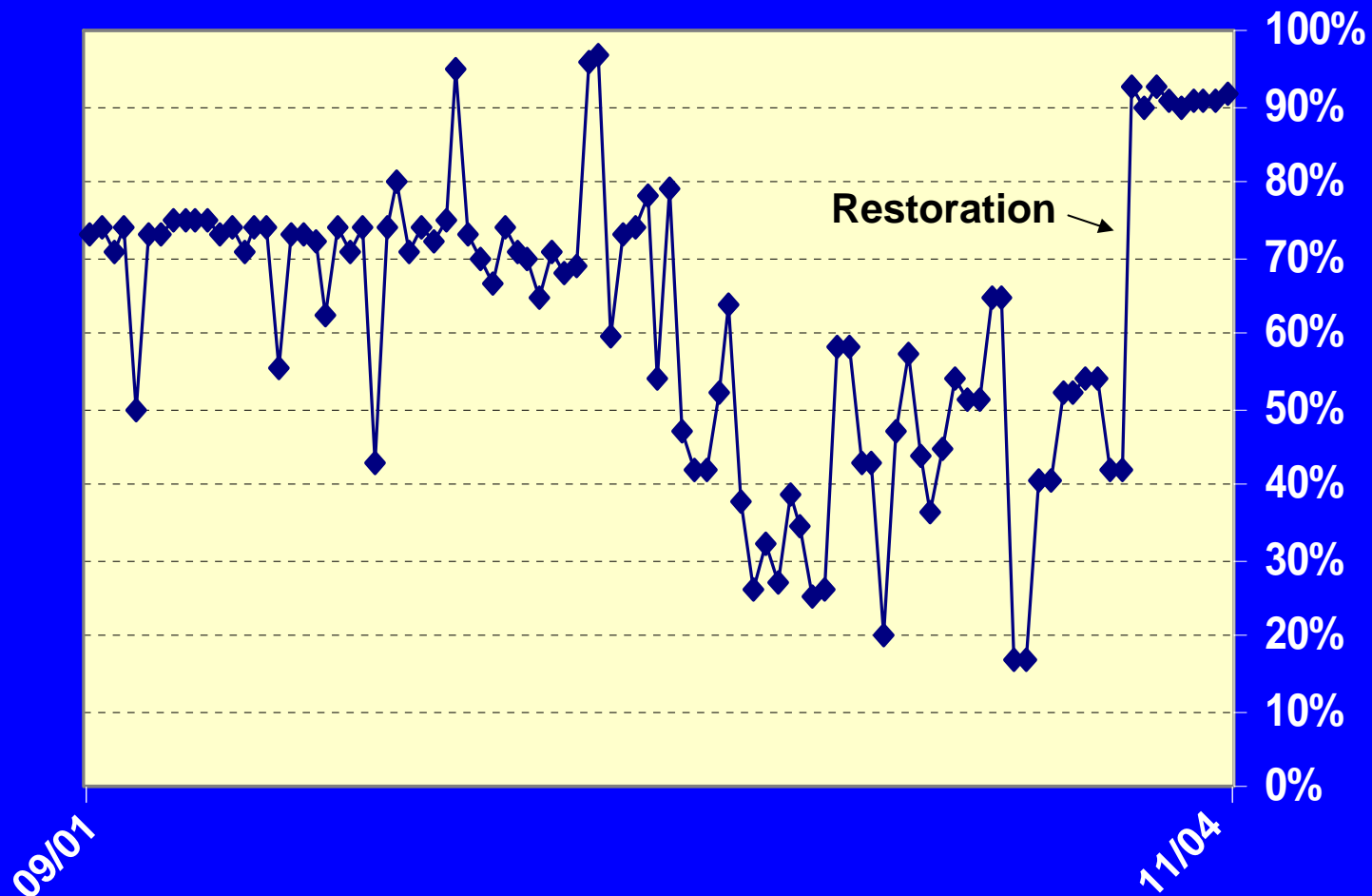
Burn-In

Socket Functionality (Board 4378)



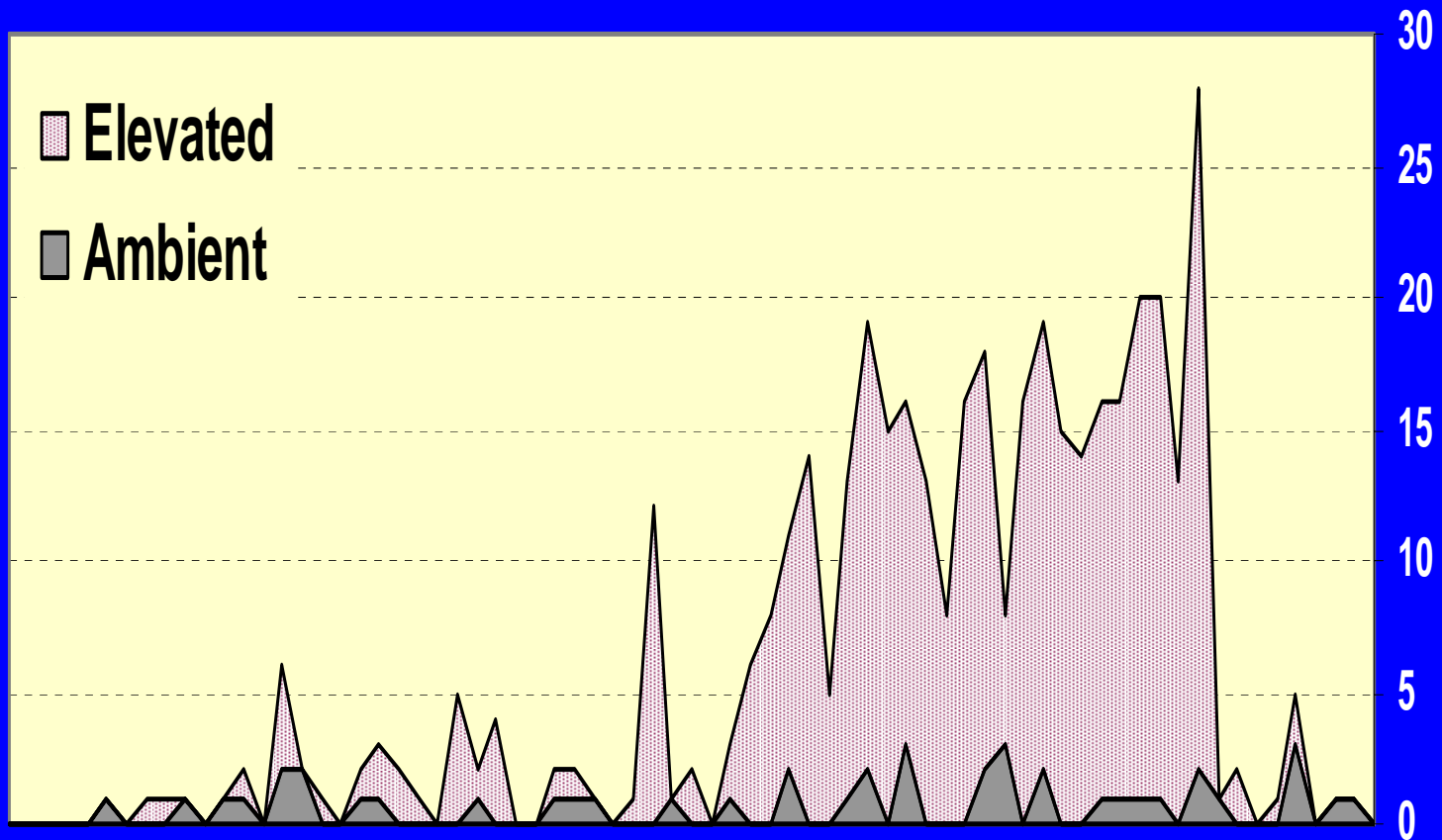
Burn-In

Socket Functionality (Board 434C)



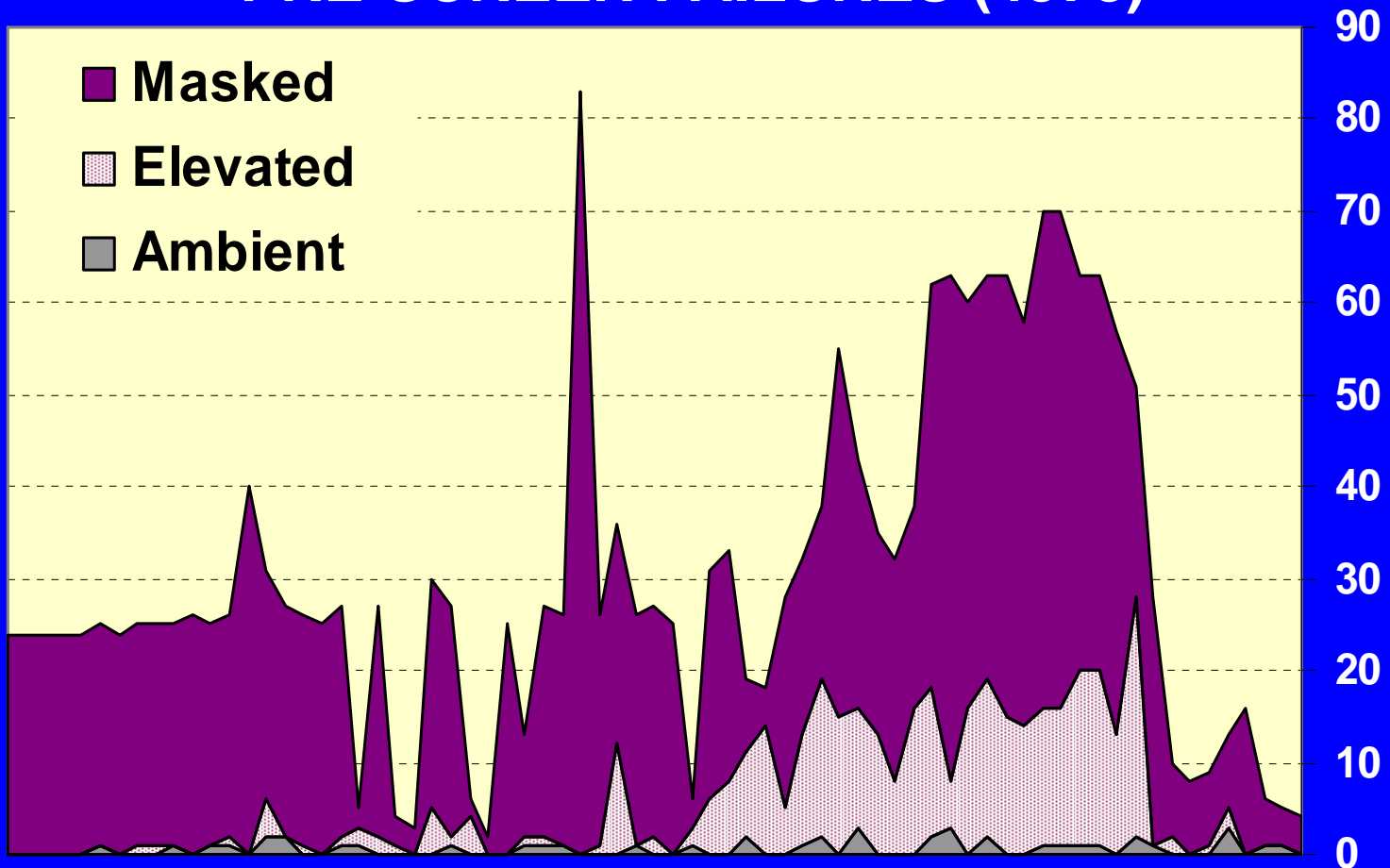
Burn-In

PRE-SCREEN FAILURES (4378) Masked Sockets Excluded



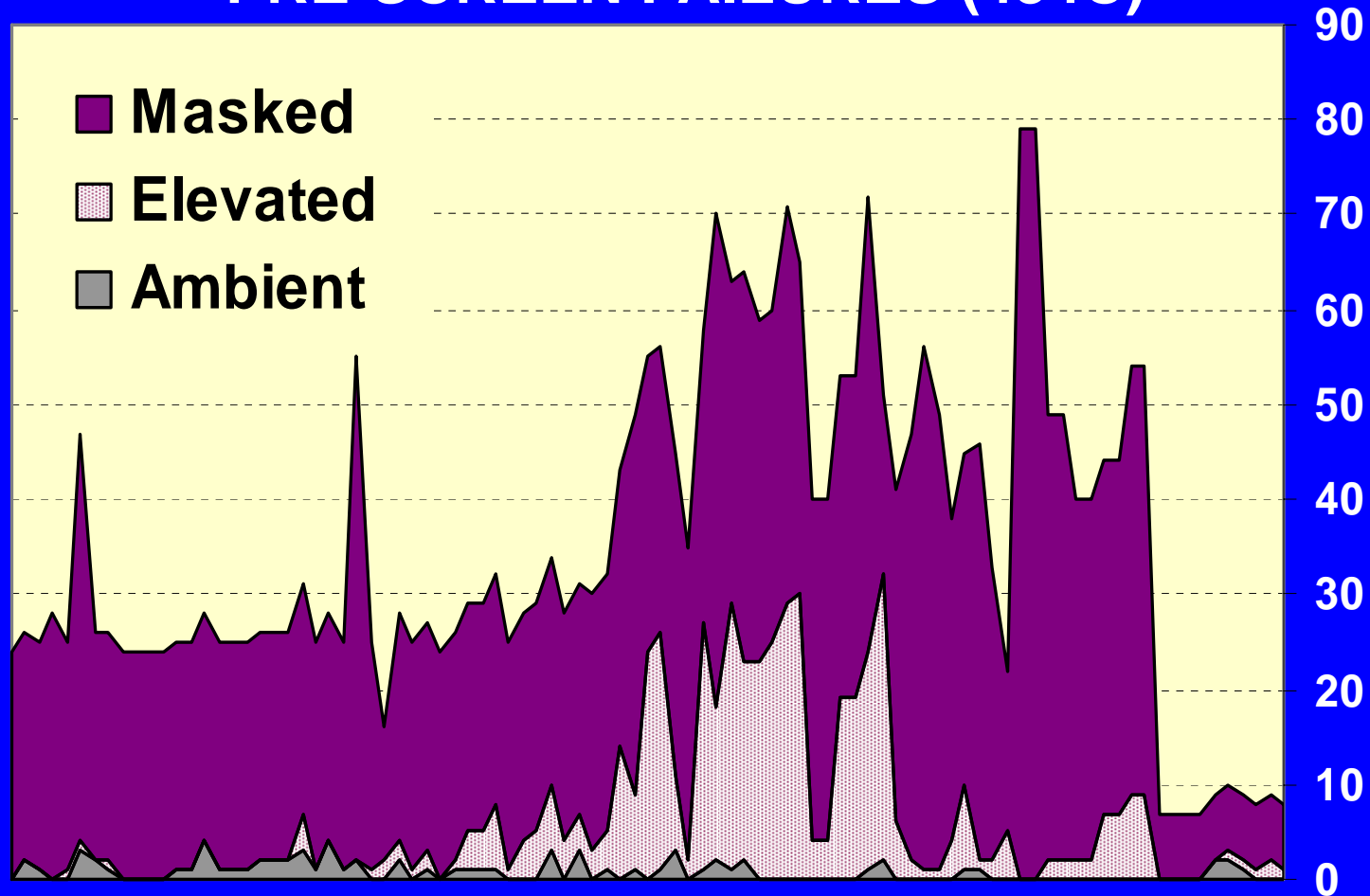
Burn-In: Contact Failure at Temp

PRE-SCREEN FAILURES (4378)



Burn-In: Contact Failure at Temp

PRE-SCREEN FAILURES (434C)

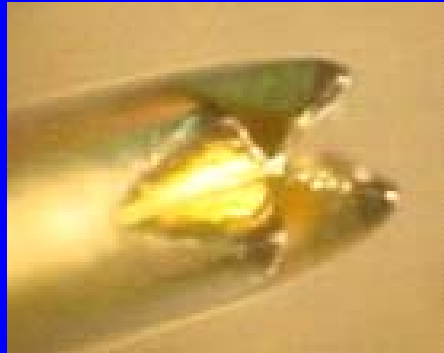


Burn-In: Benefits Summary

- **Reduces/Eliminates Board Replacement Cost**
- **Reduces Labor: Board Handling & Pre-Screen**
- **Increases Oven Space Utilization**
- **Decreases Facility Power Consumption**
- **Increases Production Capacity (+112%)**

Test

POGO PIN / SPRING PROBE RESTORATION



Test

- **Spring Probe (Pogo Pin) Socket**
- **144 Pin BGA Device**
- **53K Initial Use Cycle Count**
- **45K Post Process (Average)**

Test

FAILED SOCKET - CONTACT RESISTANCE

MAX 12022 / MIN 118 / AVG 1558 / STD DEV 2338 (milliohm)

| | A | B | C | D | E | F | G | H | J | K | L | M |
|----|------|------|------|------|------|-------|------|-------|------|------|------|------|
| 1 | 8243 | 1404 | 695 | 1201 | 203 | 298 | 6248 | 535 | 835 | 389 | 598 | 511 |
| 2 | 1352 | 2224 | 4121 | 432 | 3405 | 11186 | 172 | 151 | 503 | 2421 | 175 | 1268 |
| 3 | 691 | 2735 | 298 | 584 | 2221 | 6852 | 581 | 701 | 382 | 304 | 1591 | 217 |
| 4 | 268 | 426 | 1317 | 638 | 2854 | 6690 | 1192 | 696 | 132 | 193 | 1854 | 916 |
| 5 | 6195 | 301 | 1687 | 6124 | 3451 | 1949 | 198 | 198 | 1249 | 902 | 583 | 583 |
| 6 | 197 | 2081 | 896 | 397 | 1511 | 121 | 147 | 528 | 182 | 1114 | 194 | 653 |
| 7 | 427 | 263 | 269 | 2625 | 118 | 182 | 168 | 182 | 593 | 714 | 9883 | 176 |
| 8 | 581 | 5113 | 402 | 447 | 237 | 506 | 504 | 165 | 346 | 184 | 645 | 288 |
| 9 | 2325 | 534 | 1108 | 1474 | 225 | 137 | 1233 | 6824 | 674 | 119 | 958 | 571 |
| 10 | 174 | 1105 | 126 | 8483 | 480 | 4868 | 518 | 149 | 143 | 1502 | 6987 | 2644 |
| 11 | 927 | 138 | 970 | 199 | 675 | 522 | 9286 | 12022 | 618 | 185 | 1227 | 812 |
| 12 | 141 | 4003 | 382 | 142 | 542 | 1867 | 1962 | 234 | 254 | 963 | 2718 | 905 |

Test

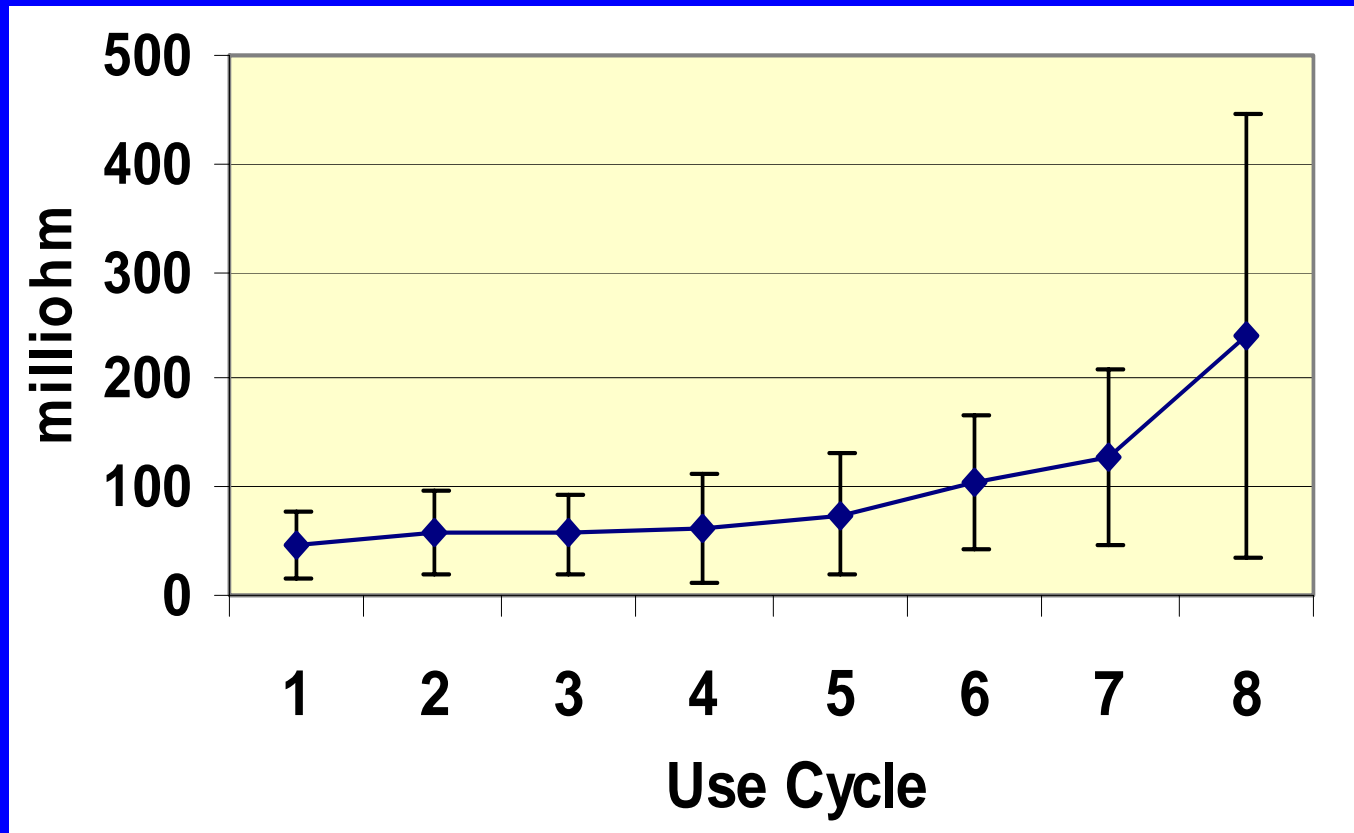
RESTORED SOCKET - CONTACT RESISTANCE

MAX 385 / MIN 31 / AVG 59 / STD DEV 40 (milliohm)

| | A | B | C | D | E | F | G | H | J | K | L | M |
|----|------|------|------|-------|------|------|-------|------|-------|-------|------|------|
| 1 | 42.4 | 31.2 | 39.4 | 41.1 | 47.4 | 88.9 | 34.8 | 45.8 | 47.1 | 102.3 | 56.4 | 35.1 |
| 2 | 63.6 | 54.8 | 49.5 | 58 | 60.4 | 34.7 | 40.7 | 59 | 42.8 | 61 | 50.8 | 40.3 |
| 3 | 48 | 39.7 | 61.4 | 49.5 | 52.9 | 44 | 57.3 | 54.5 | 45.2 | 54.4 | 74.9 | 57.5 |
| 4 | 42.9 | 47.5 | 44.4 | 385.1 | 334 | 48.2 | 103.6 | 66.2 | 49.7 | 56.8 | 54 | 67.8 |
| 5 | 46.7 | 53.1 | 57.8 | 42.8 | 58.8 | 42.7 | 44.3 | 56.1 | 77.4 | 47.1 | 51.4 | 42.3 |
| 6 | 44.3 | 42.4 | 49.4 | 70 | 42.7 | 55.2 | 35.7 | 59.1 | 187 | 64.9 | 42.3 | 57.4 |
| 7 | 40.1 | 45.6 | 52.3 | 57.3 | 41.4 | 50.5 | 55.7 | 64.1 | 45.7 | 41.1 | 54.5 | 68.3 |
| 8 | 47.6 | 57.1 | 54.7 | 48 | 45.2 | 40.3 | 44.8 | 47.7 | 76 | 51.9 | 64.2 | 92.9 |
| 9 | 55.6 | 56.9 | 67.8 | 45.2 | 52.8 | 43.6 | 46.2 | 60 | 44.5 | 57.1 | 47.7 | 39.9 |
| 10 | 51 | 52.9 | 49.1 | 69.6 | 45.8 | 78 | 53.3 | 55.6 | 76.4 | 51 | 64.8 | 41 |
| 11 | 77.6 | 75.7 | 48.1 | 45.1 | 63.8 | 46.5 | 83.9 | 43.4 | 107.9 | 48 | 56.4 | 42.9 |
| 12 | 55 | 63.2 | 44.1 | 59.5 | 65.2 | 51.3 | 77.2 | 49.8 | 46.7 | 42.5 | 62.3 | 46.3 |

Test

POGO PIN CONTACT RESISTANCE

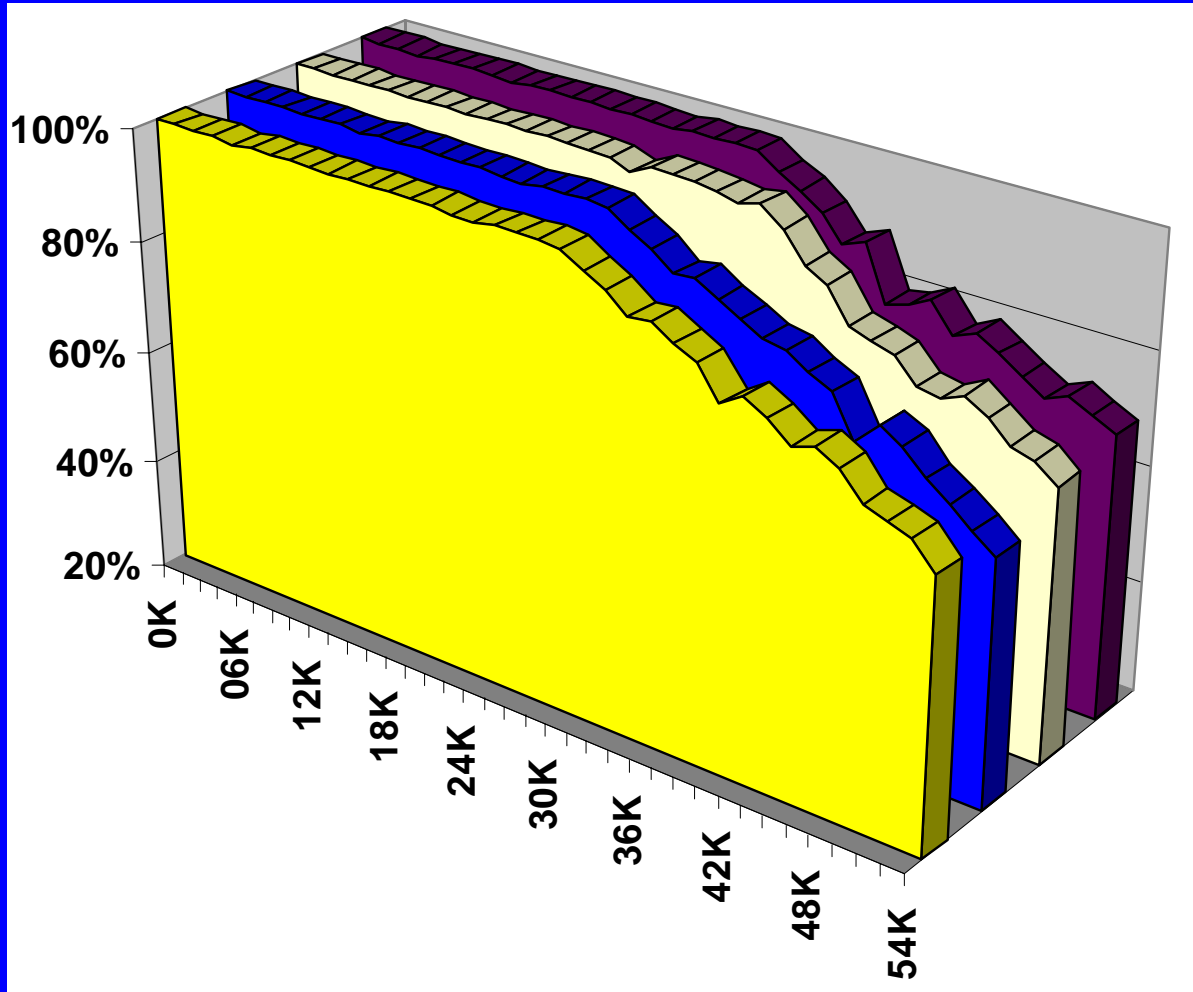


Device Programming

- Programming Yield
- Solder Contamination → Reduced Yield
- Yield Restoration
- Production Results

Device Programming

YIELD VS. DEVICES PROGRAMMED (Typical)

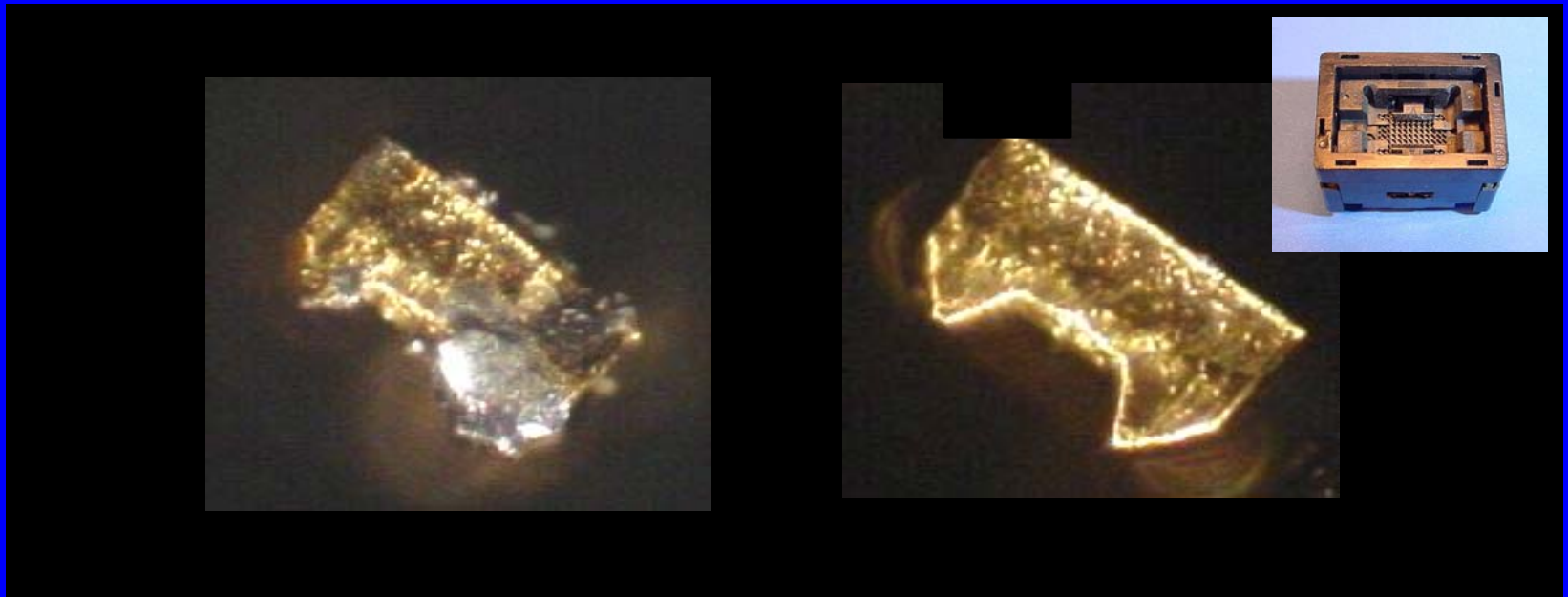


Device Programming

Solder Contamination

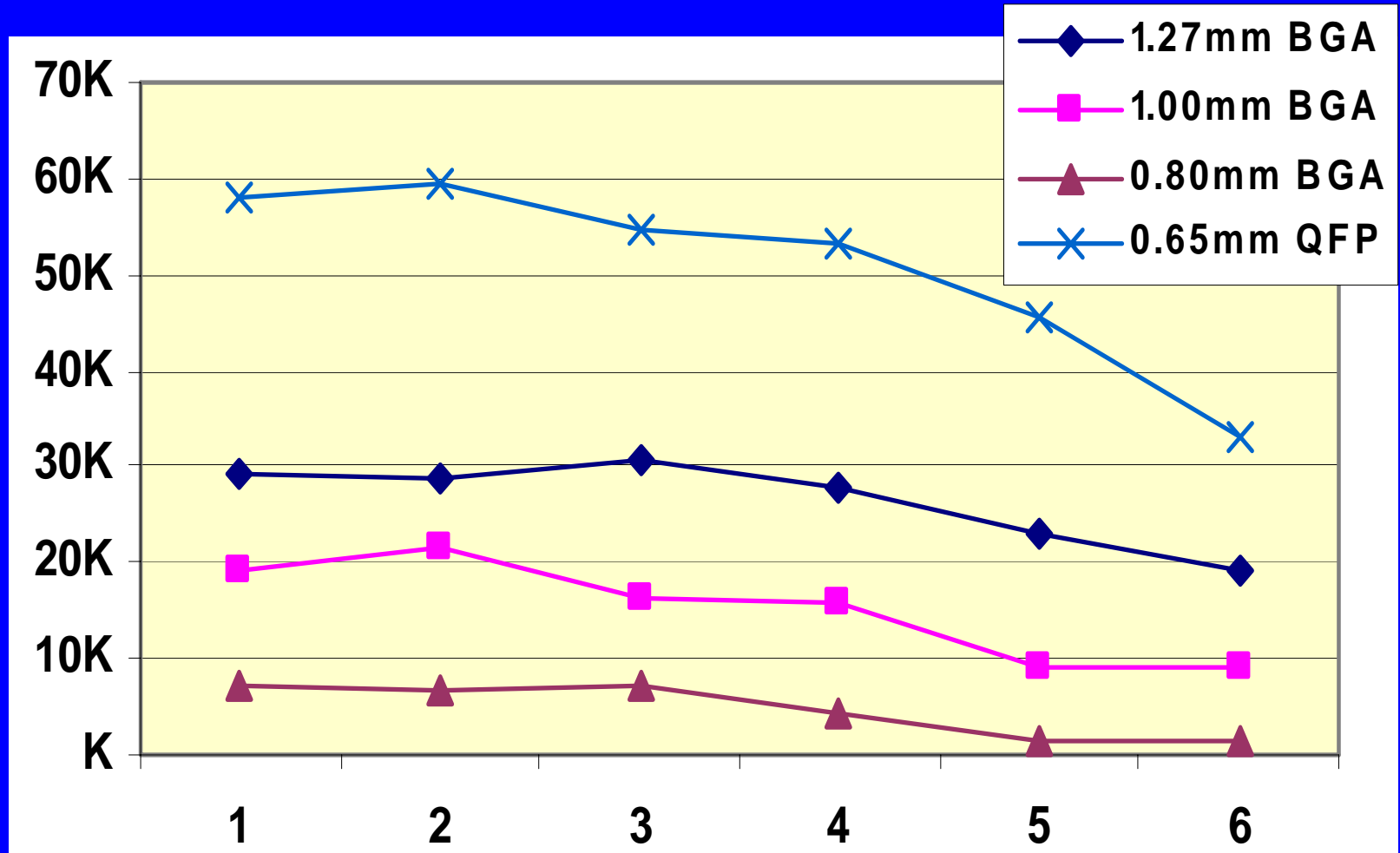
Increased Contact Resistance

Reduced Yield



Device Programming

Socket Restoration



Thank You!