



# Burn-in & Test Socket Workshop

**March 7 - 10, 2004**  
**Hilton Phoenix East / Mesa Hotel**  
**Mesa, Arizona**

## ARCHIVE

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## Session 8

Wednesday 3/10/04 10:30AM

### SOCKETING LEAD-FREE PACKAGES

**“Effect Of Compression Style Contactors On Lead Free Solder”**

Ila Pal – Ironwood Electronic, Inc.

**“Pb-Free Leadframe Devices And Their Impact On Pogo Pin Socket Performance”**

Valts Treibergs – Everett Charles Technologies



**Ironwood  
Electronics, Inc.**

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**Effect of Compression Style  
Contactors on Lead Free Solder**

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**ILA PAL**

# Agenda

- Pb free background
- Experimental objectives
- Contact resistance analysis
- Ball damage analysis
- Electrical performance
- Force characterization
- High speed characterization
- Conclusions

# Why lead free?

- To avoid legislation that would force a change
- To protect our environment
- To meet consumer demand

# National Electronics Manufacturing Initiatives

- Group of 30 different organizations including OEMs, contract manufacturers, solder manufacturers, government agencies, and universities.
- Focus
  - Lead free assembly
  - Solder alloys
  - Components
  - Solder reliability

# National Electronics Manufacturing Initiatives

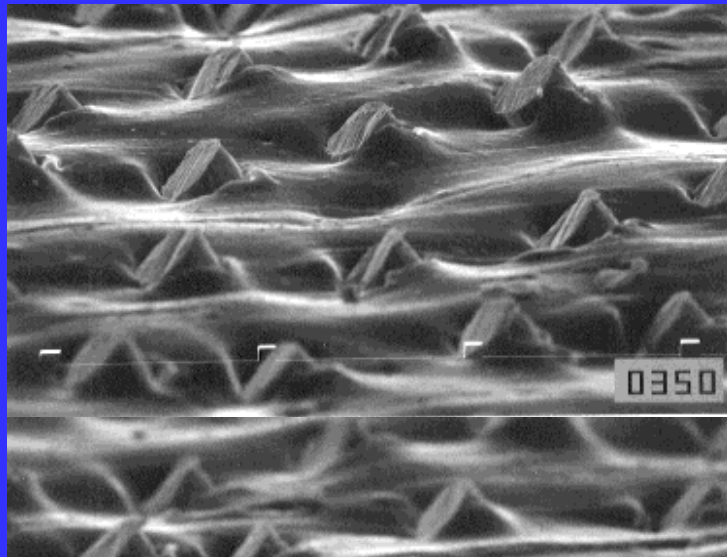
NEMI has developed a ranking system, based on strengths and weaknesses of the major alloy candidates. They have concluded that the SnAgCu alloy family is more viable than the SnAgBi family.



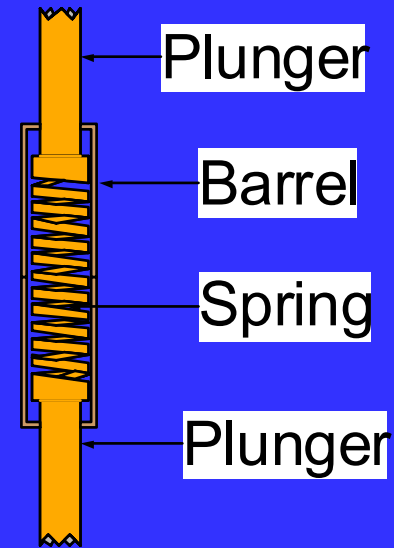
# Experimental Objectives

- Solder alloys
  - 63Sn 37Pb
  - 95.5Sn, 3.8Ag, 0.7Cu
- Compression style contactors
  - Elastomer
  - Spring pin

# Compression style contactors

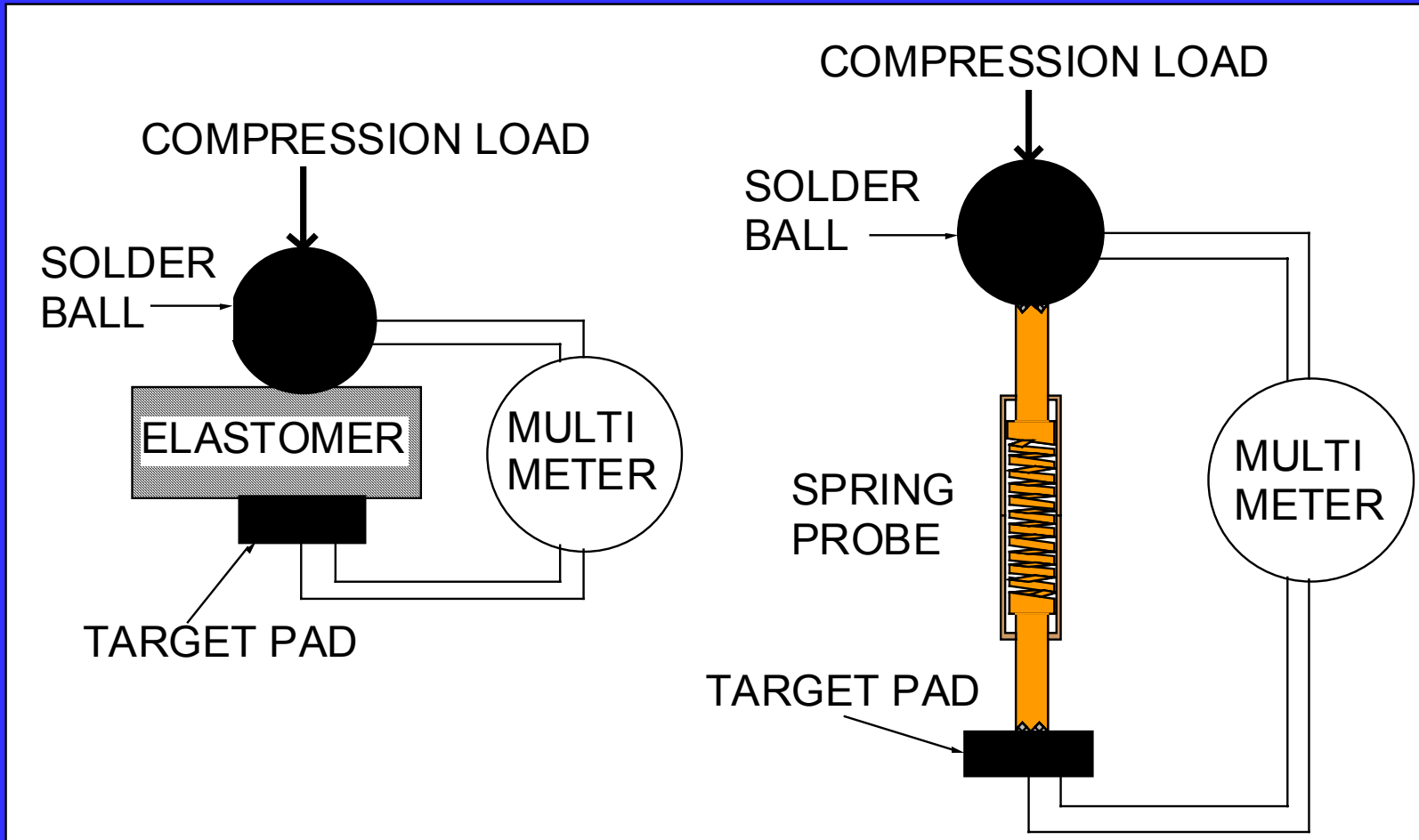


SEM picture of  
Elastomer

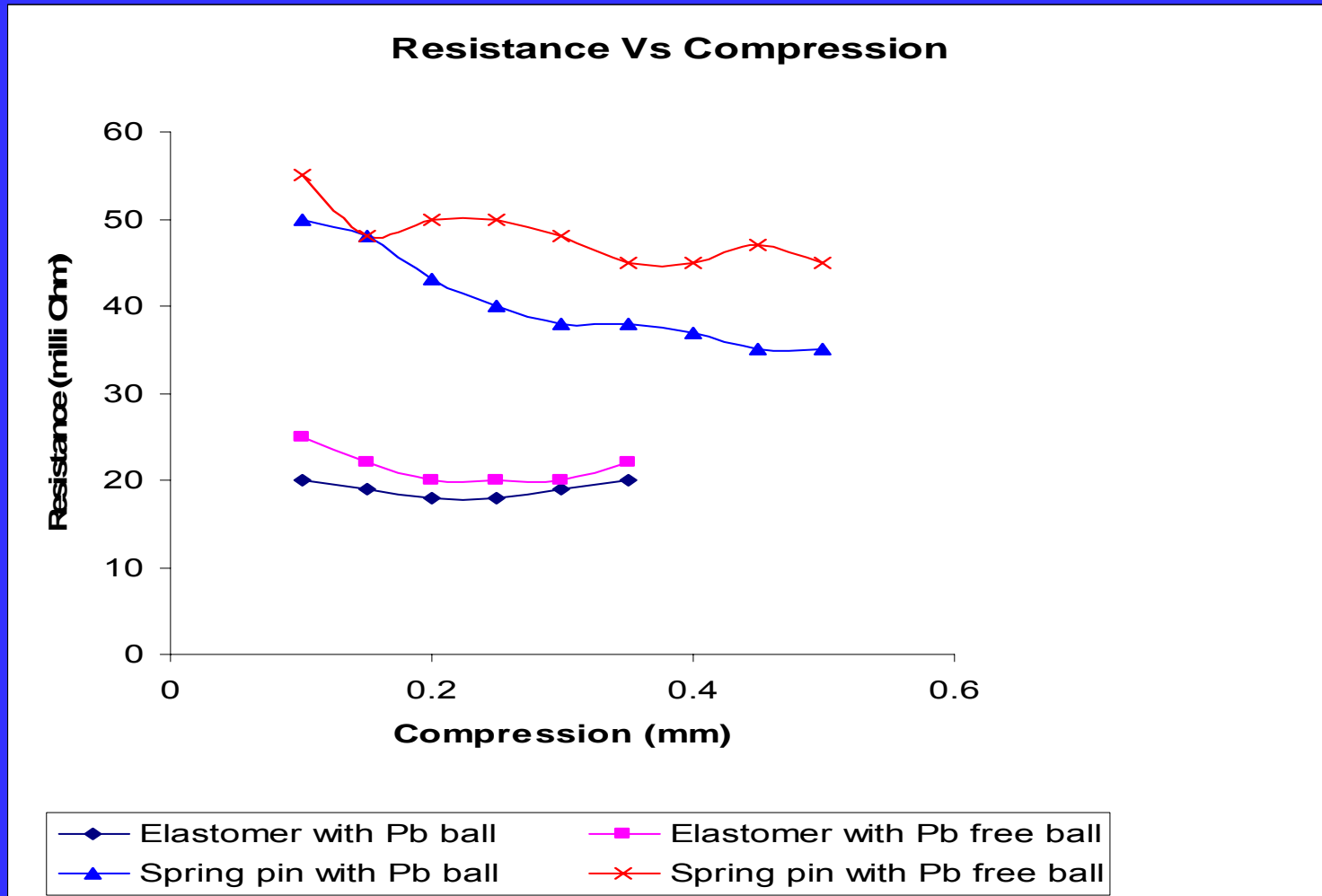


Spring Probe  
Cross Section

# Contact Resistance Experiment



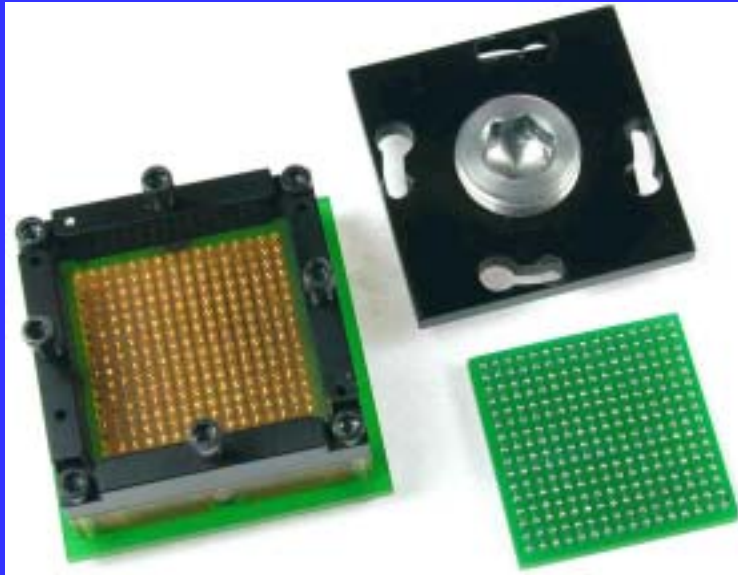
# Contact Resistance Data



# Contact Resistance Experiment at 85C

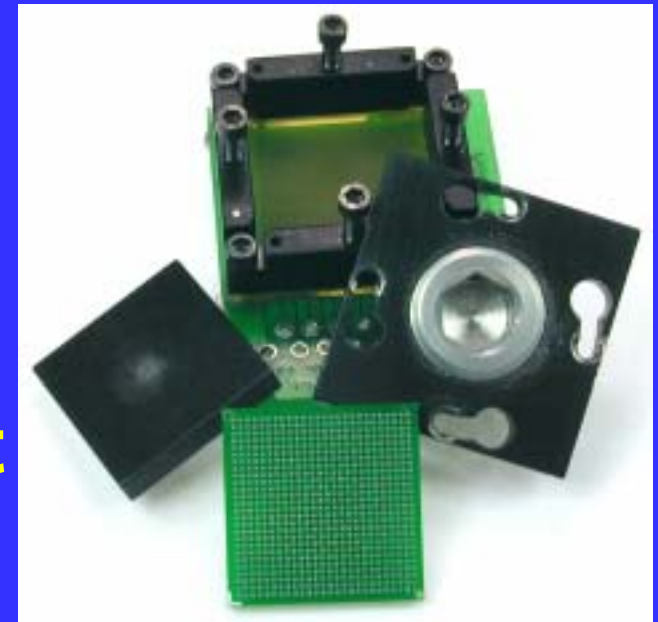
- Elastomer socket and spring probe socket were mounted on a daisy chained test board.
- Daisy chained test chips (with Pb and with Pb free) were placed inside the socket.
- Testing the two end pins, the complete array can be verified and contact resistance per pin can be calculated.
- The two end pins were routed to four pads for Kelvin measurements using 4-wire setting.
- The socket was placed inside an oven at 85C.
- Total contact resistance was measured at regular time intervals.

# Test components

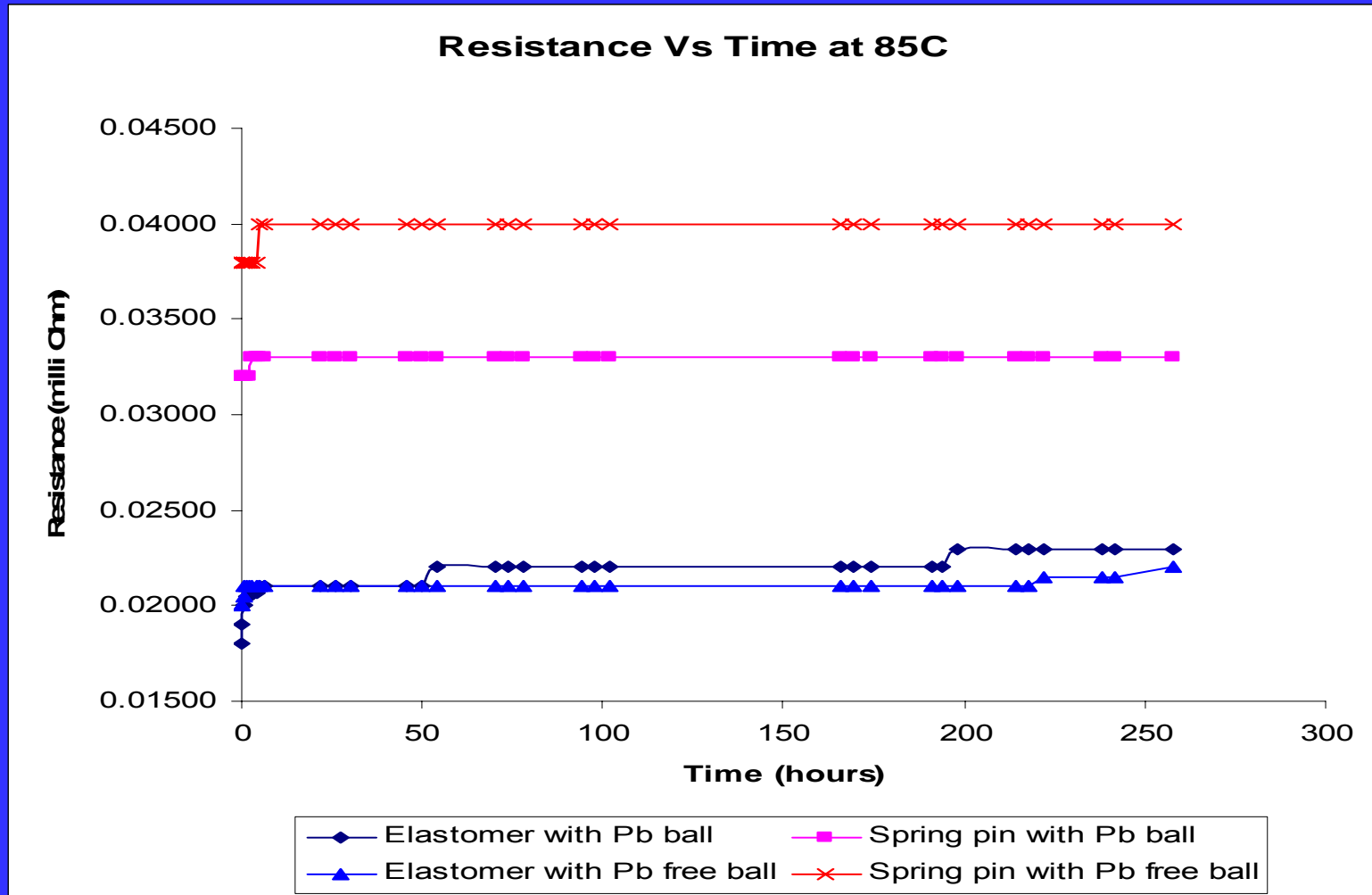


Daisy chain testing of spring pin socket

Daisy chain testing of elastomer socket



# Contact Resistance at 85C

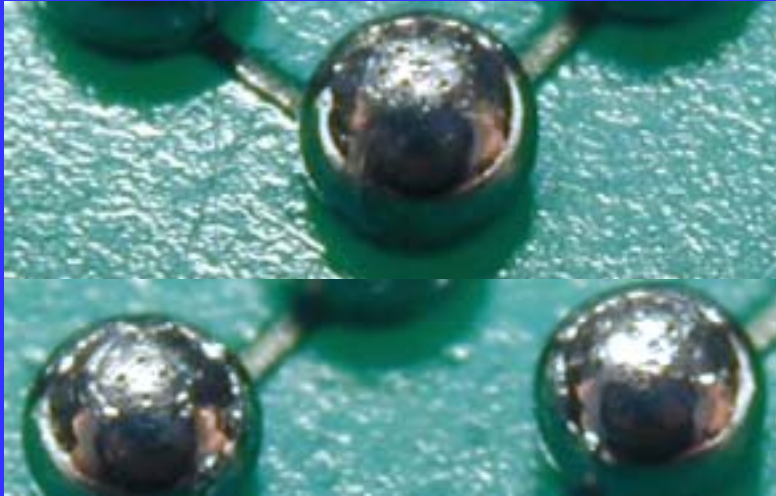


## Ball damage analysis

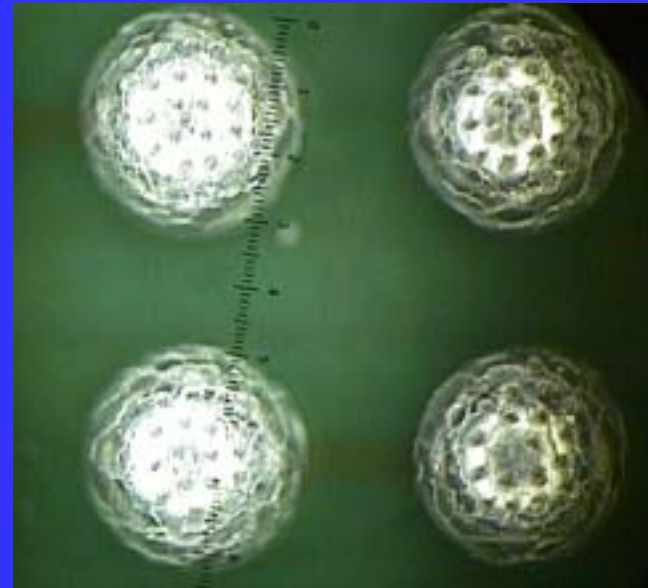
- micro BGA (0.5mm pitch, 0.3mm diameter solder ball) test chip
  - with Pb
  - with Pb free
- micro BGA was compressed to 0.1mm in the elastomer socket and 0.3mm in the spring probe socket.
- same device was placed in and out for 20 cycles.
- device was examined under microscope to determine the ball damage after 20 cycles.



# Ball damage analysis

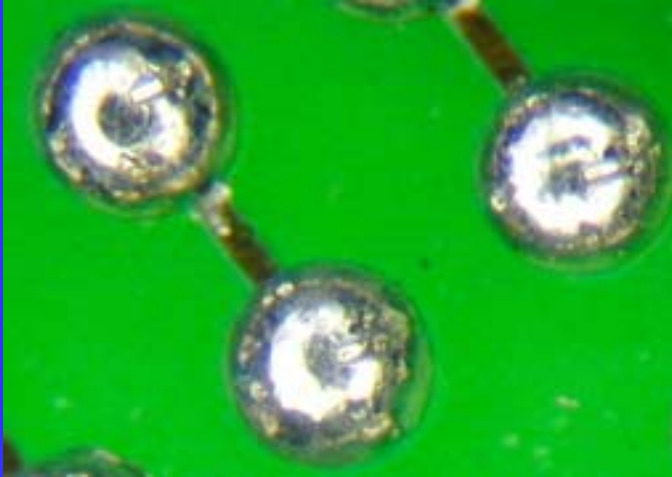


**Elastomer marks  
– with Pb free**

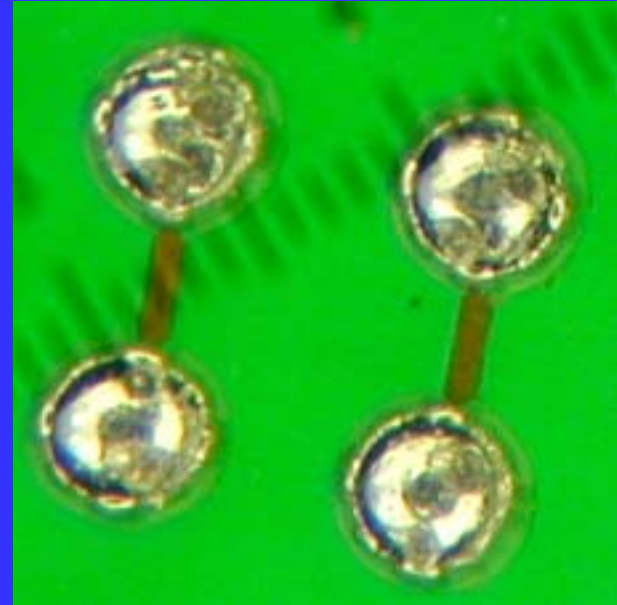


**Elastomer marks  
– with Pb**

# Ball damage analysis



**Spring pin marks  
– with Pb free**

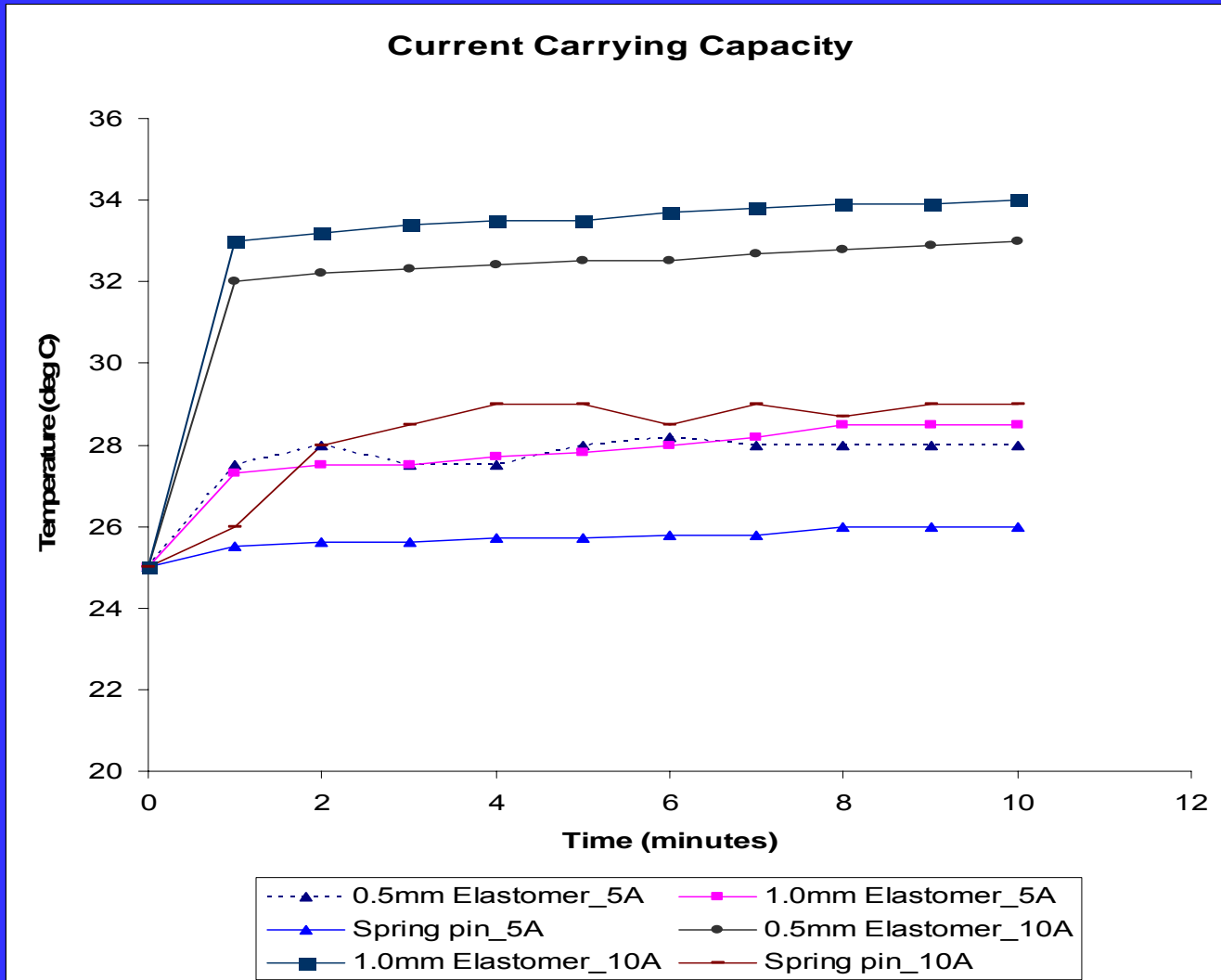


**Spring pin marks  
– with Pb**

# Current carrying capacity

- 1.0mm diameter gold plated pin is compressed 0.25mm down on the elastomer and 0.3mm down on the spring probe.
- The bottom side of the contactor is compressed on a gold plated copper pad.
- Thermo couple was connected to the contactor to measure the change in temperature.
- Power supply was connected in parallel to the gold plated pin and copper pad.
- 5A and 10A current was supplied continuously for 10 minutes and the changes in temperature were recorded.

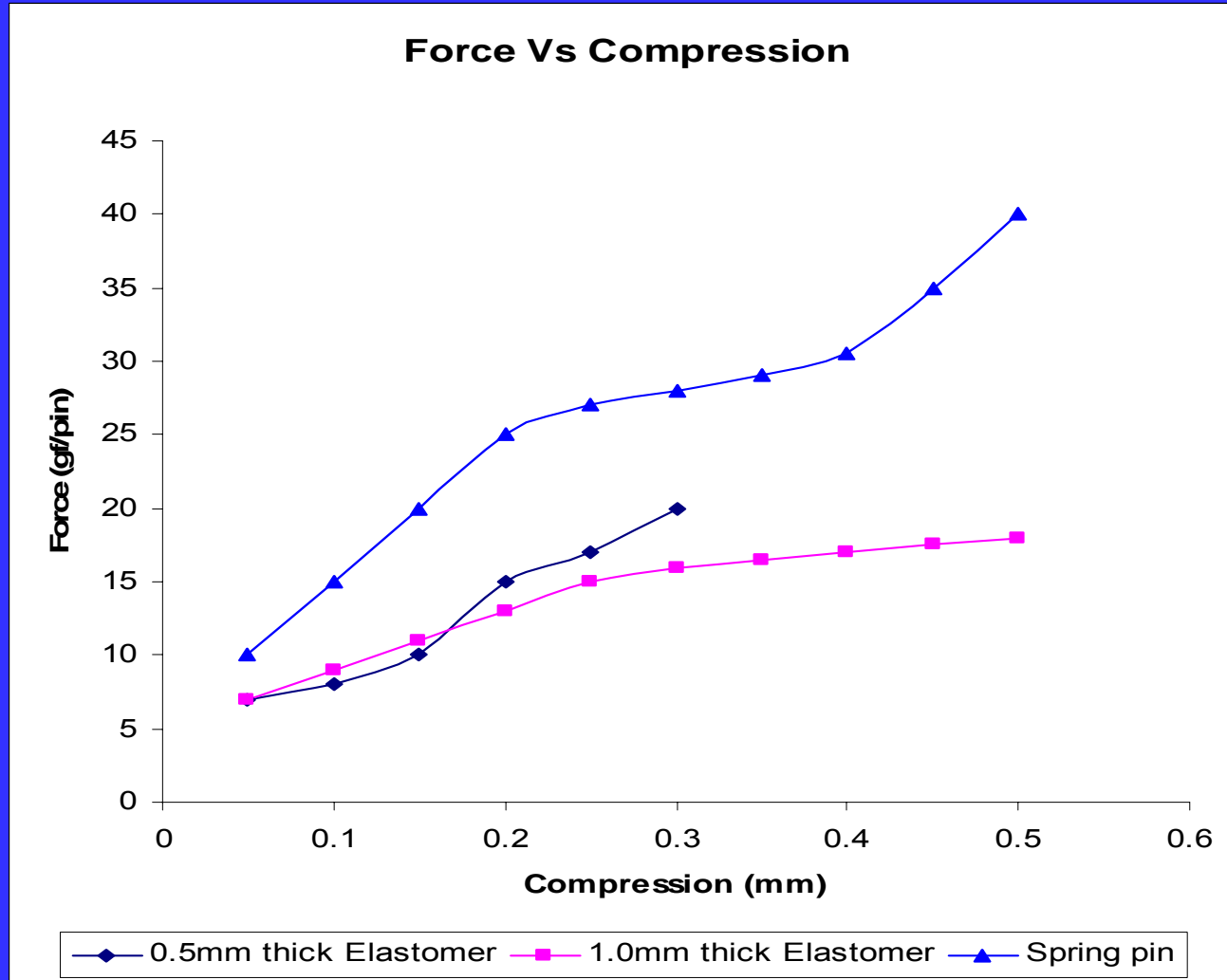
# Current carrying capacity



# Force characterization

- Test system was developed with a force sensor circuit.
- A load cell with flat surface was placed on top of the contactor.
- Force sensor transmits any force variations in terms of voltage drop to a volt meter.
- Measured voltage variations were converted to the corresponding force.

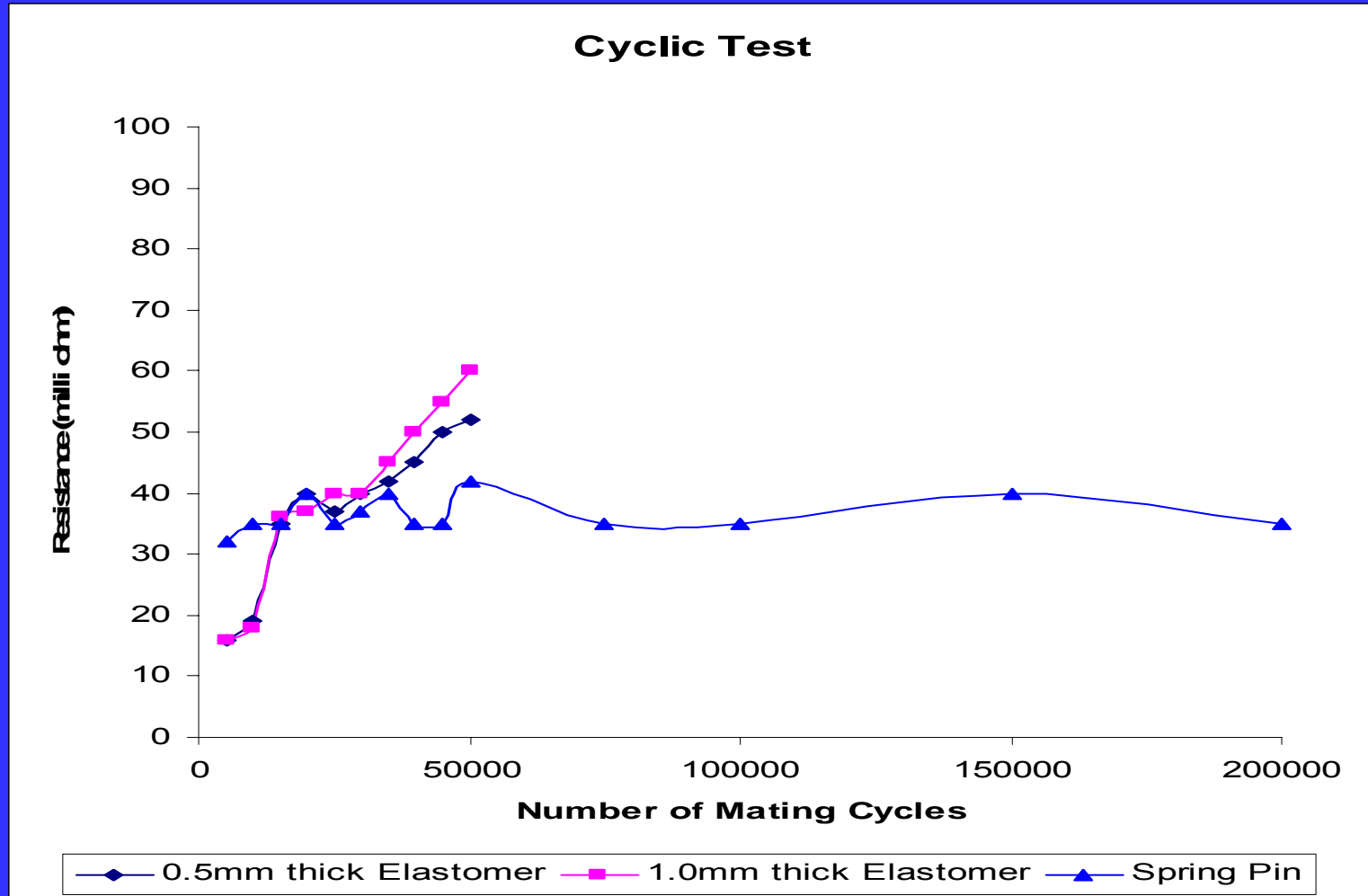
# Force data chart



# Endurance characterization

- Contactor was mounted on a circuit board with gold plated copper pad.
- Gold plated steel ball was used for compressing into the contactor.
- Compression pressure of  $275\text{g/mm}^2$  was applied with 1 second ON and 1second OFF compression cycle.
- Change in resistance was read using HP4338A multi-meter which was connected to the gold plated ball and the copper pad.

# Endurance data chart

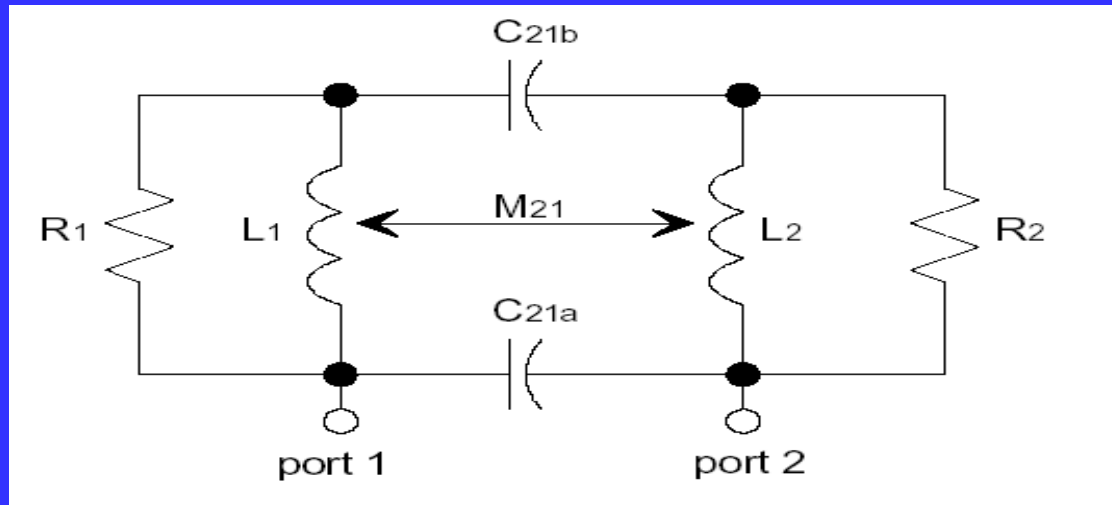




# High speed characterization

- Contactor was mounted onto a custom board, designed to exhibit low parasitic and allows the use of coplanar probes (for probing adjacent pins).
- Test chip with measurement standard pattern was mounted on top of the contactor.
- Setup allows pins to be measured under three conditions (open, shorted and thru).
- Hewlett-Packard MDS (Microwave Design System) software was used to extract an equivalent-circuit model, which is SPICE compatible.
- Hewlett-Packard 8510C network analyzer & GGB Pico-probe™ 450 mm pitch were used.

# Equivalent circuit model



$L_1, L_2$ : Pin self inductance

$M_{21}$ : Mutual inductance between adjacent pins

$R_1, R_2$ : Shunt resistance of inductors  $L_1$  and  $L_2$ , used to model high frequency loss due to skin effect and dielectric loss

$C_{21a}$ : Mutual capacitance between adjacent pins on PCB side

$C_{21b}$ : Mutual capacitance between adjacent pins on IC side

# Results

Pins	Field Adjacent	Edge Adjacent	Diagonal Adjacent	Corner Adjacent
L1, L2 (nH)	0.15	0.23	0.15	0.26
M21 (nH)	0.025	0.04	0.002	0.05
R1, R2 ( $\Omega$ )	700	700	700	700
C21a (pF)	0.01	0.02	0.003	0.03
C21b (pF)	0.015	0.03	0.004	0.03

**0.5mm Elastomer**

# Results

Pins	Field Adjacent	Edge Adjacent	Diagonal Adjacent	Corner Adjacent
L1, L2 (nH)	0.37	0.39	0.37	0.46
M21 (nH)	0.035	0.09	0.002	0.05
R1, R2 ( $\Omega$ )	700	700	700	700
C21a (pF)	0.014	0.04	0.005	0.05
C21b (pF)	0.015	0.04	0.007	0.05

**1mm Elastomer**

# Results

Pins	Field Adjacent	Edge Adjacent	Diagonal Adjacent	Corner Adjacent
L1, L2 (nH)	2.2	2.3	2.2	2.4
M21 (nH)	0.3	0.4	0.09	0.3
R1, R2 ( $\Omega$ )	700	700	700	700
C21a (pF)	0.03	0.04	0.005	0.05
C21b (pF)	0.06	0.09	0.01	0.05

**Spring probe**

# Conclusions

- Pb and Pb free balls exhibit similar contact resistance.
- Elastomer provides better contact resistance than the spring probe.
- Spring probe exhibits better thermal performance than the elastomer.
- Pb balls have more witness marks than Pb free balls.

# Conclusions

- Spring probe sustains better current rating than elastomer.
- Spring probe withstands 200K mating cycles as opposed to elastomer (10K).
- Elastomer demonstrates far superior results than spring pin for high speed testing.

# Conclusions

- Universal socket footprint – Standardization
- Replacement modules
  - Conductive elastomer
  - Spring probe
  - Compliant metal contact
  - Other compression contact technologies





EVERETT CHARLES  
TECHNOLOGIES  
Testing the Limits



***Pb-FREE  
LEADFRAME  
DEVICES AND  
THEIR IMPACT ON  
POGO PIN SOCKET  
PERFORMANCE***

Valts Treibergs, ECT-Semiconductor Test Group - MN

# ***Presentation Topics***

- Why Pb-Free Packaging?
- Challenges for Test
  - » Package Lead Hardness
- Proposed Pogo Pin Solution
- Validation Testing
  - » Test Sequence
  - » Test Apparatus
- Results
  - » Resistance vs. Pogo Cycle
  - » Solderability
- Next Steps



# *Why the Shift to Pb-Free Packaging?*

- Many IC customers are requiring 'green' microelectronic packaging
  - » The push is being seen particularly by Japanese and European customers
- Worldwide directives / legislation to protect the environment:
  - » NEMI - North America
  - » WEEE, RoHS - Europe
  - » MITI - Japan
  - » Others pending

# ***Most Common Pb-Free Options for Leadframe IC's***

***Post-plate Matte Tin or Pre-plate NiPdAu or NiPd***

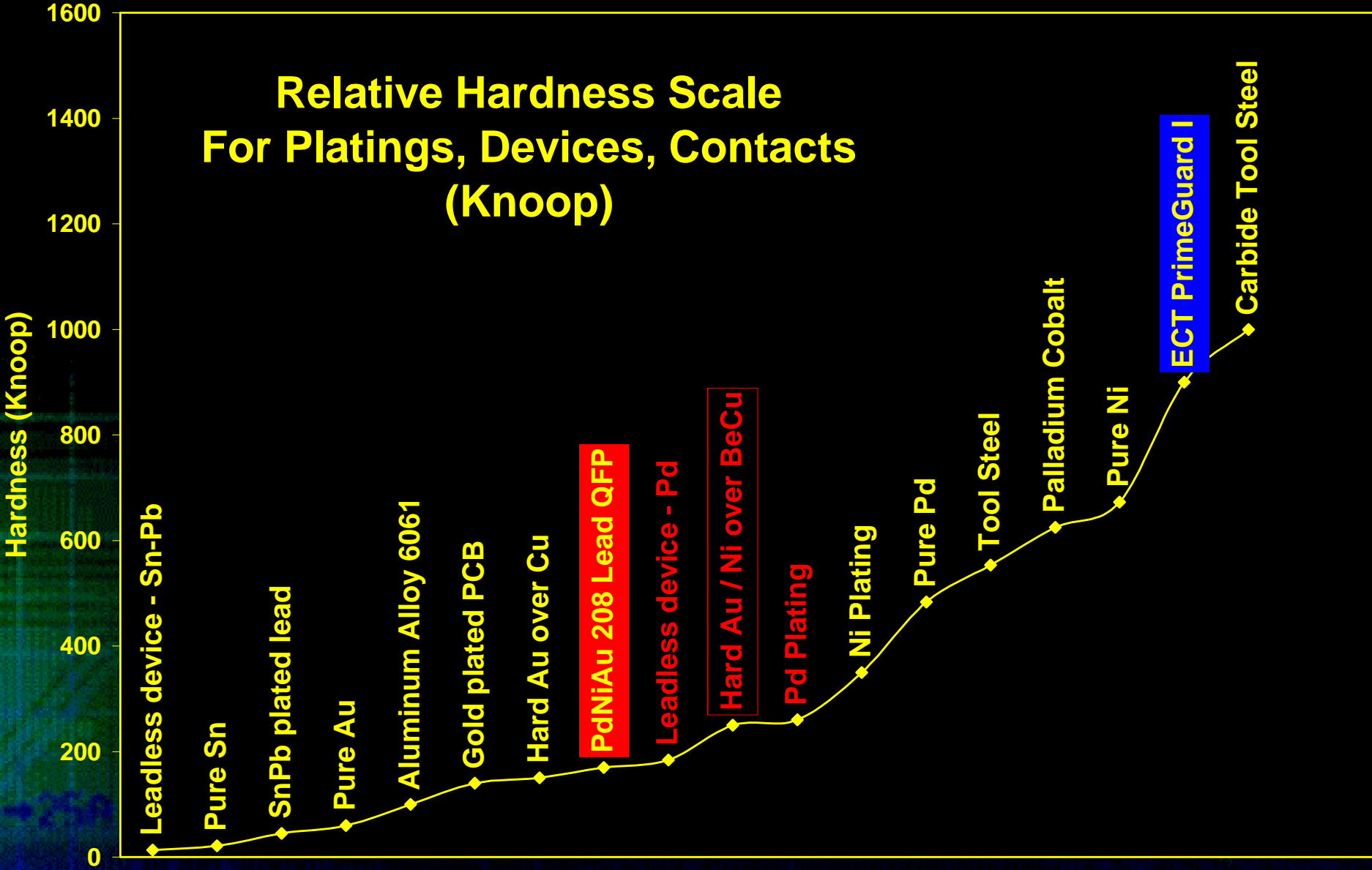
- Finish options are dependent on IC type and/or application
- Also dependent on assembly facility process
- Many IC manufacturers are shipping these now - many others in conversion
- Extensive reliability studies have been done
  - solderability, whisker growth, reflow, etc.

# NiPd - Challenges for Test

- Preplated NiPd and NiPdAu have been proven to be very abrasive to contact technologies
- Very early wear-out has been observed using hard gold over nickel - pogo and cantilever technologies
- Plating wear exposes base material (BeCu or steel) and accelerates corrosion and increases contact resistance. YIELD drops after <10K insertions



# Package Lead Hardness Comparison



# Proposed Pogo Pin Solution

- A contact metallurgy is needed that is significantly harder than the NiPdAu leadframe
  - » Hard gold / Nickel over BeCu
    - Not hard enough - too close to NiPdAu
  - » Palladium Cobalt a possible option
    - Not tested in production for leadframe contacting
  - » **ECT PrimeGuard-I**
    - A proven HVM solution for pre-plated NiPd leadframe contacting for 3+ years



# Validation Testing

- Pb-Free device samples were limited - available parts were not bussed or daisy chained. Gold nest designed and built to allow LLCR contact measurements
- Most important factors to investigate contactor solutions:
  - » LLCR stability at room temperature to 100K cycles min
  - » Pogo pin wear - no wear to 100K cycles min
  - » No post-contacting solderability issues on DUT leads
- Concentrate on Pogo pin tip to DUT lead contact interface
  - » Test does not include variation of internal Pogo resistance (well proven and documented in other studies)



# ***Test Sequence***

- All testing at room temp.(20°C)
- Used single Pogo Pin plunger used for each sequence
- 40 unprocessed Pb-Free 208 lead QFP devices used per sequence
- Robot probed each lead 5 or 15 times (simulating standard process flow) per lead - recording force and LLCR when mounted in a gold plated nest
- 30g and 50g probe normal forces investigated
- Samples marked and returned to customer for solderability 'Dip & Look' test

# Test Sequence

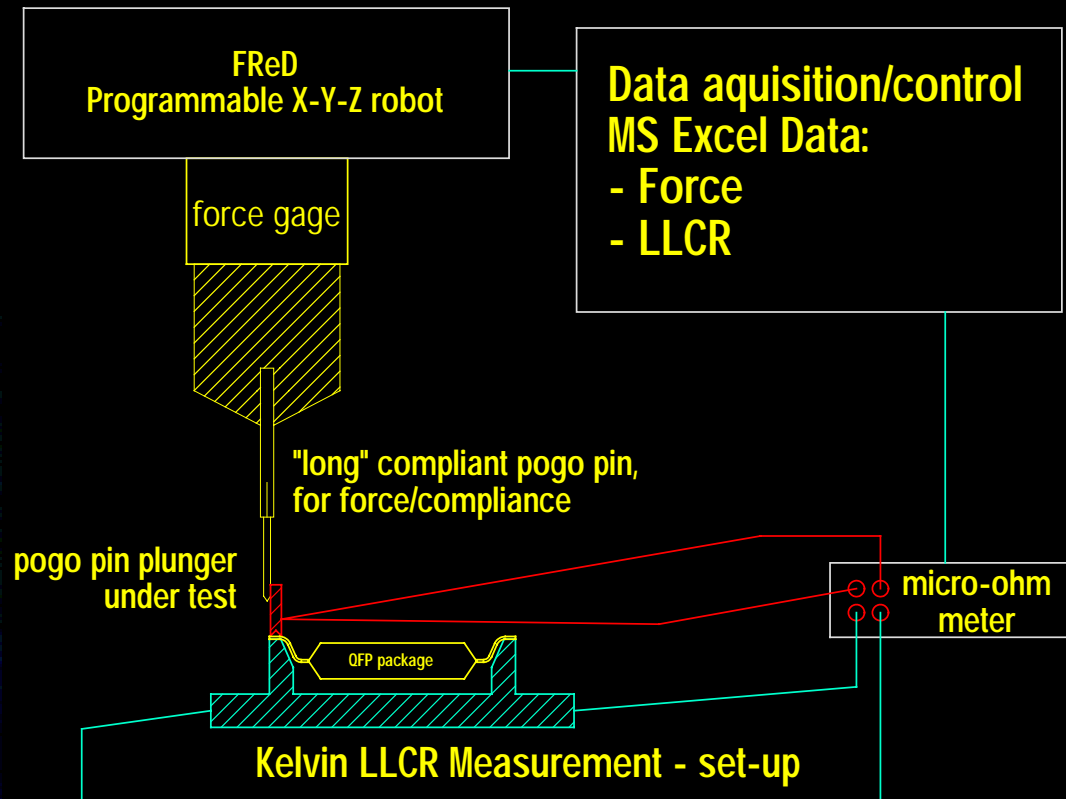
SEQUENCE	1	2	3	4
APPLIED FORCE	30g	50g	30g	50g
TOUCHDOWNS PER LEAD	5 hits	5 hits	15 hits	15 hits
TOTAL # TOUCHDOWNS	41600	41600	124800	124800
Dip & Look	10 pcs	10 pcs	10 pcs	10 pcs

Dip & Look Parameters

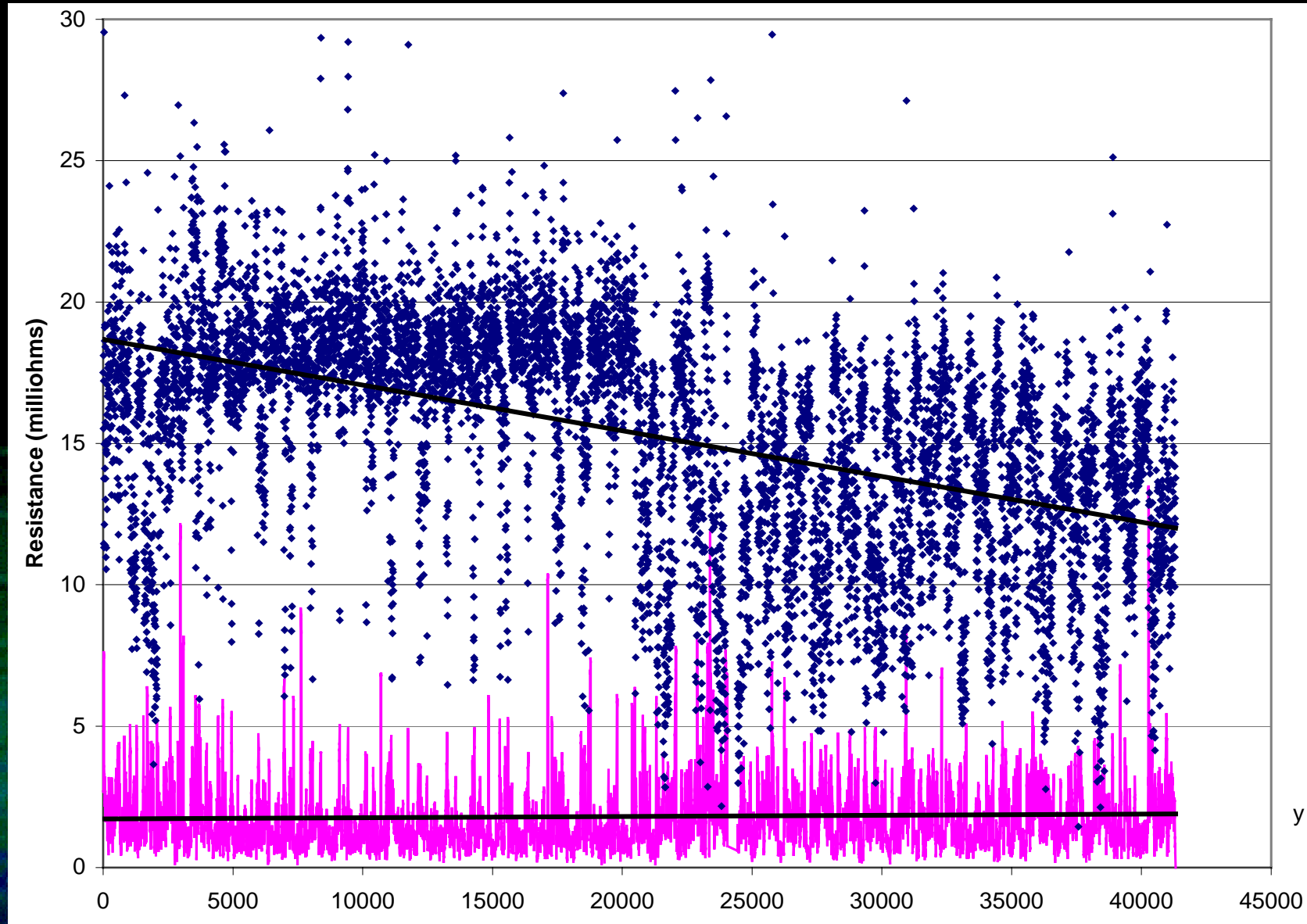
SOLDER BATH	PRECONDITIONING STEP
SnPb	8 hours bake at 150° C
SnPb	8 hours steam age 85/85
SnAgCu	8 hours bake at 150° C
SnAgCu	8 hours steam age 85/85

# Test Apparatus

- ECT FReD robot used to probe single POGO interfaces on 208 QFP package
- Gold plated package nest used to hold DUT during test
- Set-up isolates pin-DUT interface



# Results - Sequence 1 (5 Hits @ 30g)



# Witness Marks / Solderability - Seq. 1

Unprobed DUT lead



Typical lead mark  
with 5x hits @ 30g

Dip & Look:

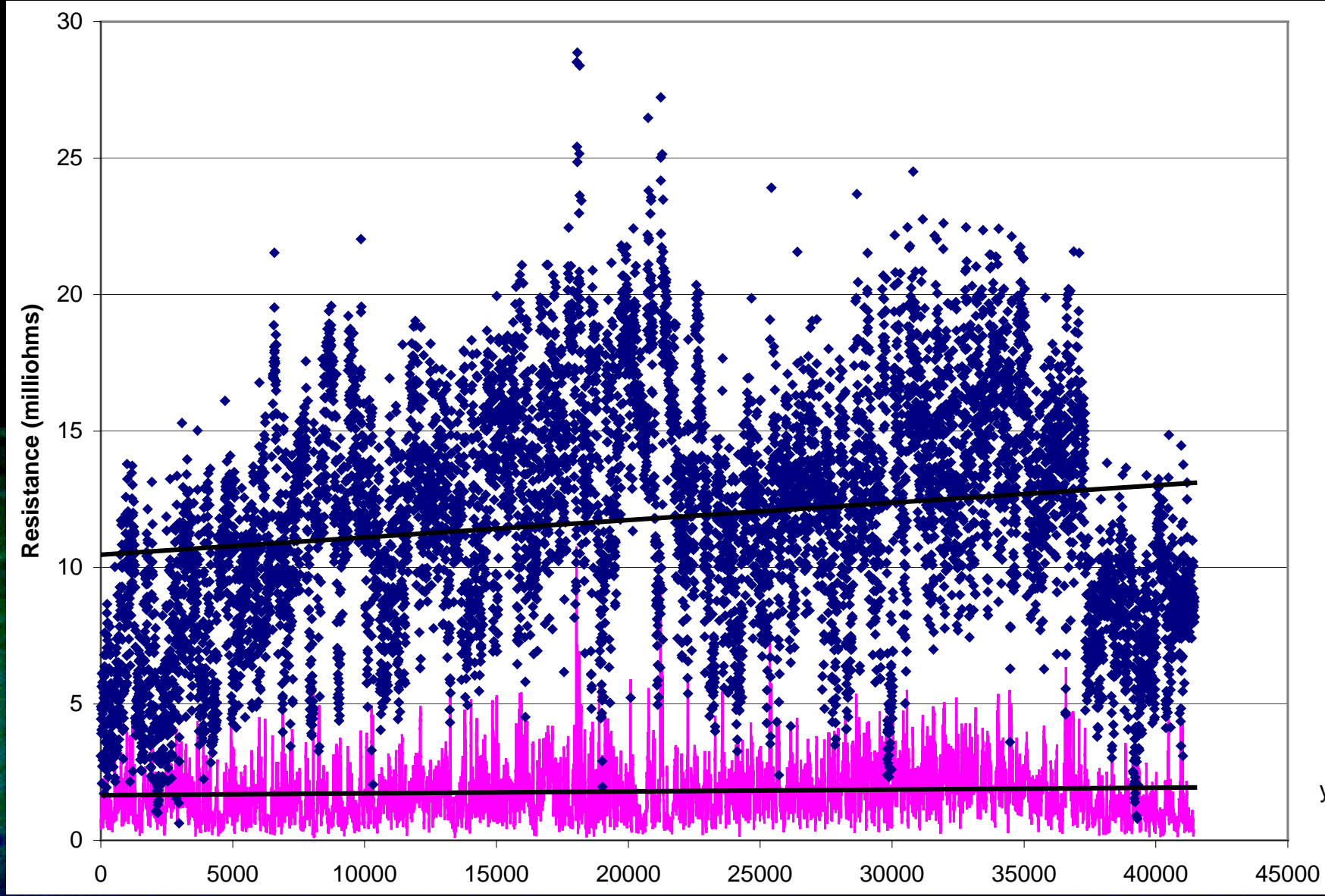


Dip & Look:  
NW with  
SnAgCu heat  
aged failure



Pogo tip condition after seq. 1  
- MINIMAL WEAR

# Results - Sequence 2 (5 Hits @ 50g)



# Witness Marks / Solderability - Seq. 2

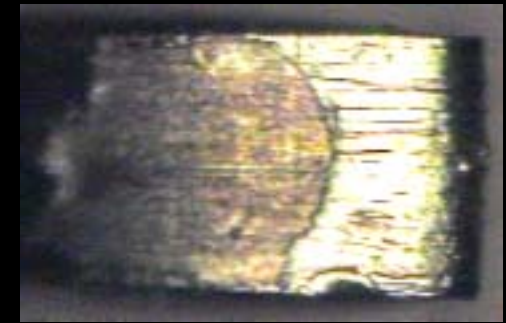
Unprobed DUT lead



Typical lead mark with 5x hits @ 50g

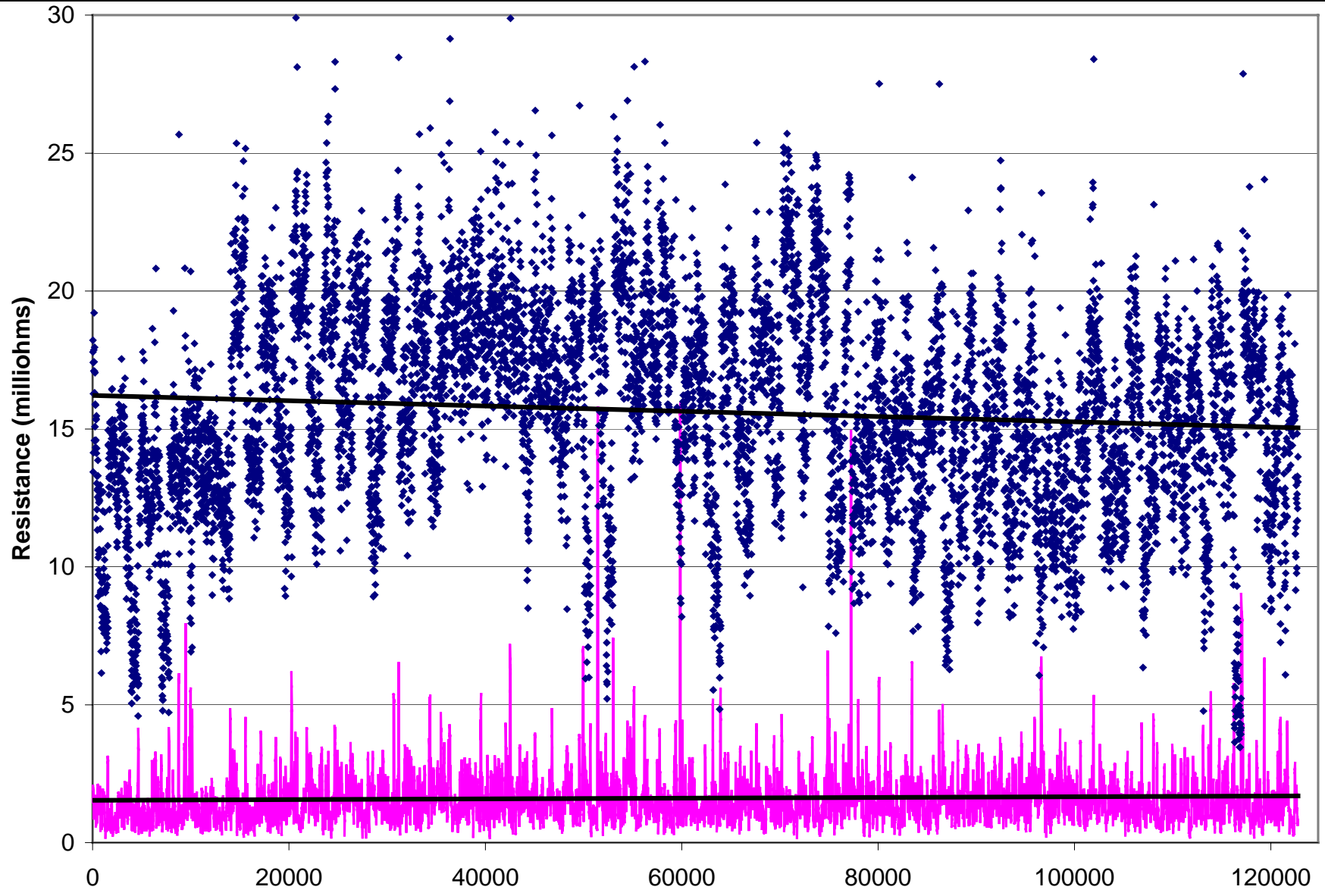


Dip & Look results - NW patterns not related to probe marks



Pogo tip condition after seq. 2 - some tip flattening observed

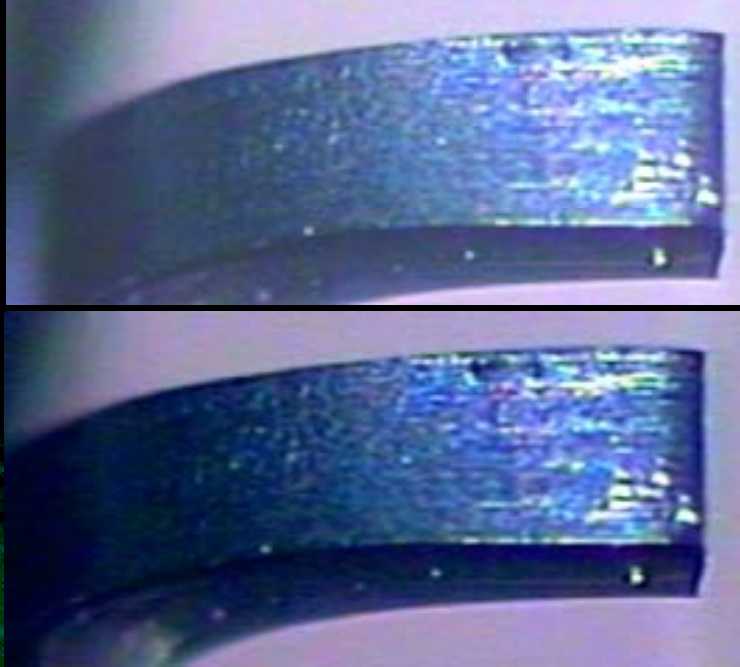
# Results - Sequence 3 (15 Hits @ 30g)



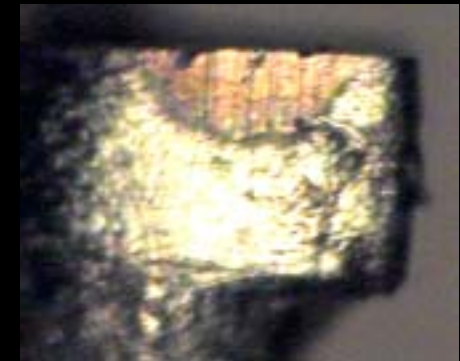


# Witness Marks / Solderability - Seq. 3

Unprobed DUT lead



Dip & Look:  
NW with  
SnPb heat  
aged failure -  
probe related  
???

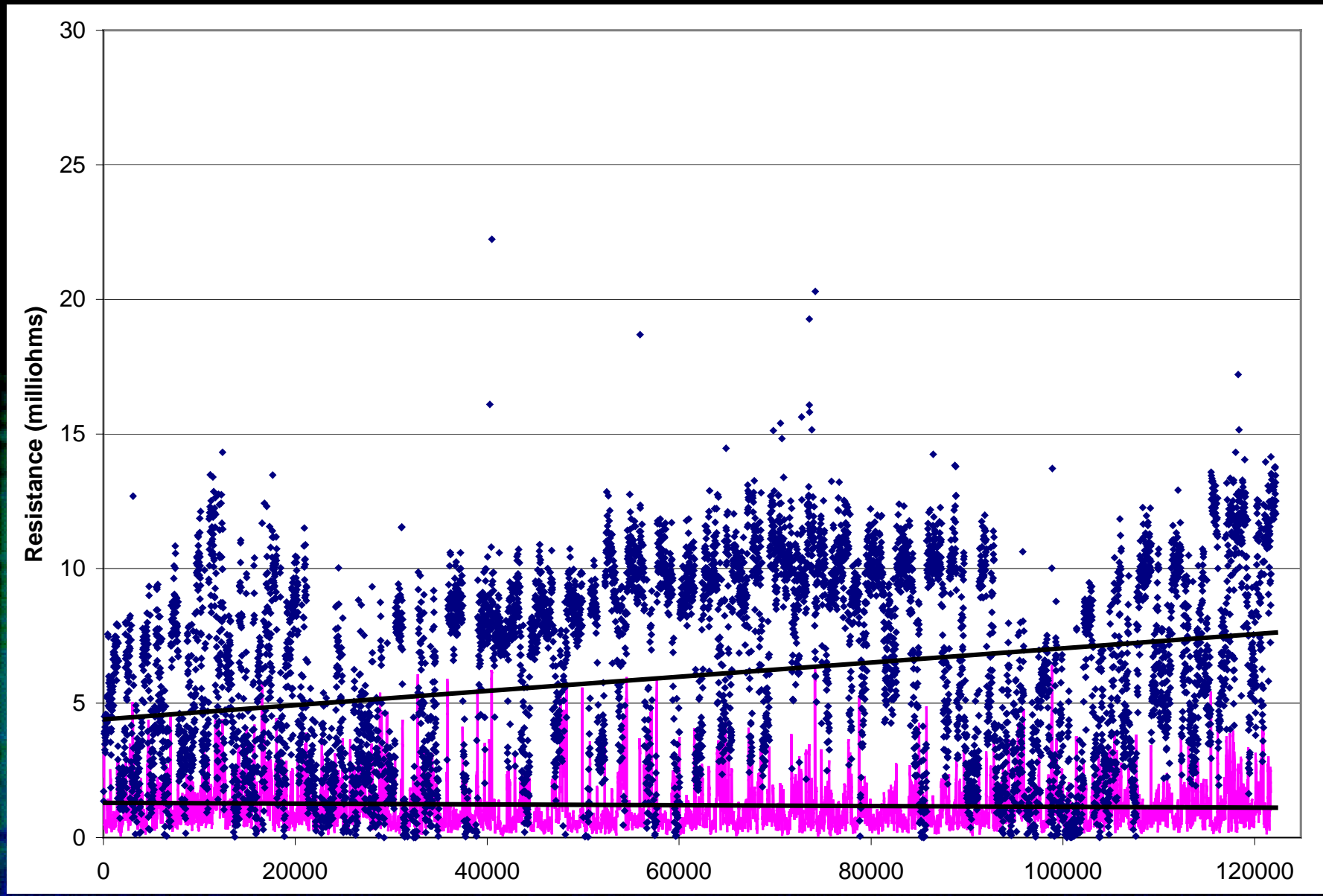


Typical lead mark  
with 15x hits @ 30g



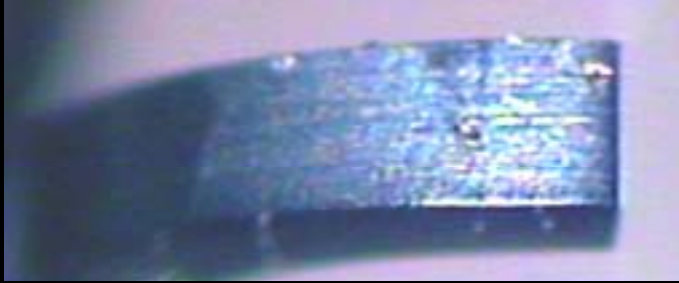
Pogo tip condition after seq. 3  
- MINIMAL WEAR

# Results - Sequence 4 (15 Hits @ 50g)



# Witness Marks / Solderability - Seq. 4

Unprobed DUT lead



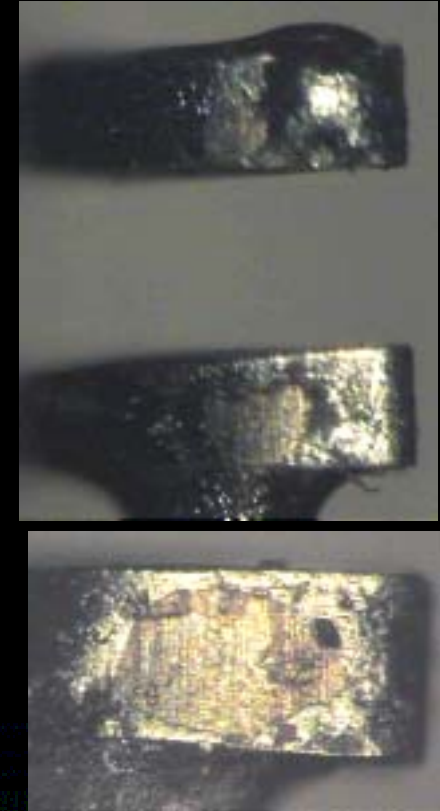
Typical lead mark  
with 15x hits@50g



Pogo tip condition after seq. 4 -  
some tip flattening and debris  
build-up observed

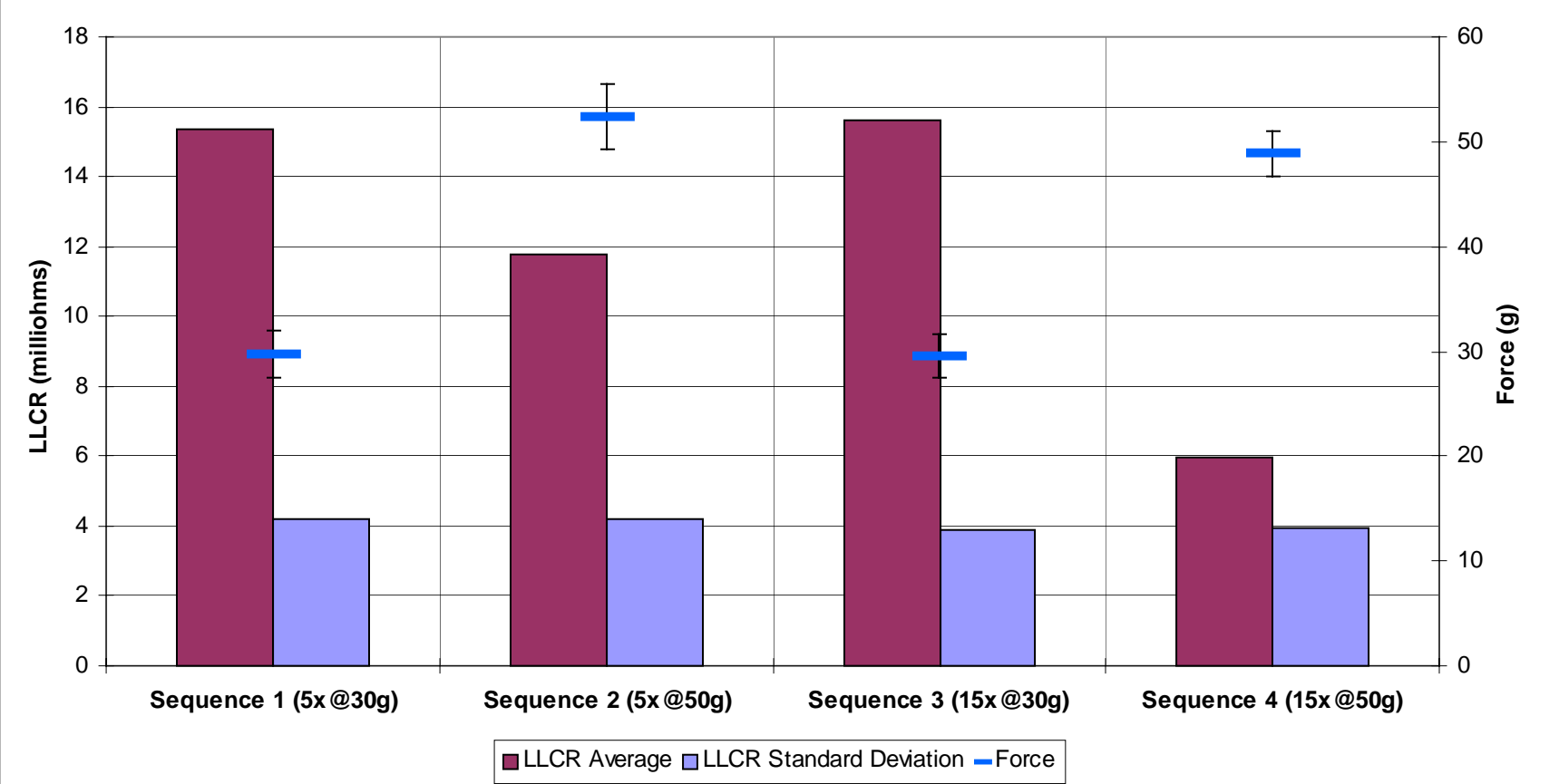
Dip & Look:

Dip & Look:  
NW with  
SnAgCu and  
SnPb heat  
aged failure



# Results Summary - Interface Resistance

- As expected - higher normal force resulted in a lower LLCR
- 15 touchdowns at 50g seemed to scrub the leads clean
- In any case - LLCR was within acceptable values - deviation all about the same



# Results Summary - Solderability

SEQUENCE	1 (5x@ 30g)	2 (5x@ 50g)	3 (15x@ 30g)	4 (15x@ 50g)
SnPb	9 pcs NW < 5% 1 pcs – no defects ACCEPTED	9 pcs – NW < 5% 1 pcs NW > 5% INVESTIGATE	8 pcs – NW < 5% 2 pcs NW > 5% INVSTIGATE	9 pcs – NW < 5% 1 pcs NW > 5% INVESTIGATE
SbPb 85/85	10 pcs NW < 5% ACCEPTED	10 pcs NW < 5% ACCEPTED	10 pcs NW < 5% ACCEPTED	10 pcs NW < 5% ACCEPTED
SnAgCu	8 pcs – NW < 5% 2 pcs NW > 5% INVESTIGATE	10 pcs NW < 5% ACCEPTED	10 pcs NW < 5% ACCEPTED	8 pcs – NW < 5% 2 pcs NW > 5% INVESTIGATE
SnAgCu 85/85	2 pcs - no defects 8 pcs – NW <5% ACCEPTED	1 pcs - no defects 8 pcs – NW <5% 1 pc – NW > 5% INVESTIGATE	10 pcs NW < 5% ACCEPTED	10 pcs NW < 5% ACCEPTED

- Some non-wetting noted
- Percentage of non-wetting similar to baseline data for Pb-Free leads after heat and 85/85 conditioning
- Pb-Free generally more difficult to solder

# Where Do We Go from Here?

- Other observations from the test:
  - » LLCR was dependent on QFP position on the nest - bulk resistance varied slightly in set-up depending on what lead was probed
  - » Slight LLCR variations were seen, depending on accuracy of probe on DUT foot - 1-2 crown points touching had lower LLCR than 3-4 crowns touching
- We need to understand behavior at temperature extremes: (125°C & -40°C) - fixture developed - test in process
- What about Sn plated leads? - test in process.
- BGA? Similar test have been done, however, not all Pb-Free BGA is the same.....

# ***Acknowledgments***

- Everett Charles Technologies
  - » Ken Snyder
    - Contact Products Division
    - Pomona CA
  - » Randy Thill
    - Semiconductor Test Group - Contactors
    - St. Paul MN

***THANK YOU!***

***QUESTIONS?***