



Burn-in & Test Socket Workshop

March 3-6 , 2002

Hilton Phoenix East/Mesa Hotel
Mesa, Arizona

IEEE

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**Burn-in & Test Socket
Workshop**

Technical Program

Session 5

Tuesday 3/05/02 1:00PM

Modeling, Analysis and Characterization

“Electrical Modeling And Contactor Performance In A RF System”

Jim Adley - Johnstech International Corporation

Eric Leung - Johnstech International Corporation

Jeff Sherry - Johnstech International Corporation

“Leaded 2mm Contactors: Measuring And Modeling To 10 GHz”

Tom Strouth - GigaTest Labs

Orlando Bell - GigaTest Labs

Gary Otonari - GigaTest Labs

Eric Bogatin - GigaTest Labs

Jeff Sherry - Johnstech International Corporation

“Force Measurement On Sockets And Contactors”

Richard Block - Advanced Micro Devices

Rafiq Hussain - Advanced Micro Devices

Electrical Modeling and Contactor Performance in a RF Test System

0.5 mm Pitch BGA

Jim Adley, R&D Manager
Eric Leung, R&D Engineer
Jeff Sherry, R&D Engineer
Johnstech International

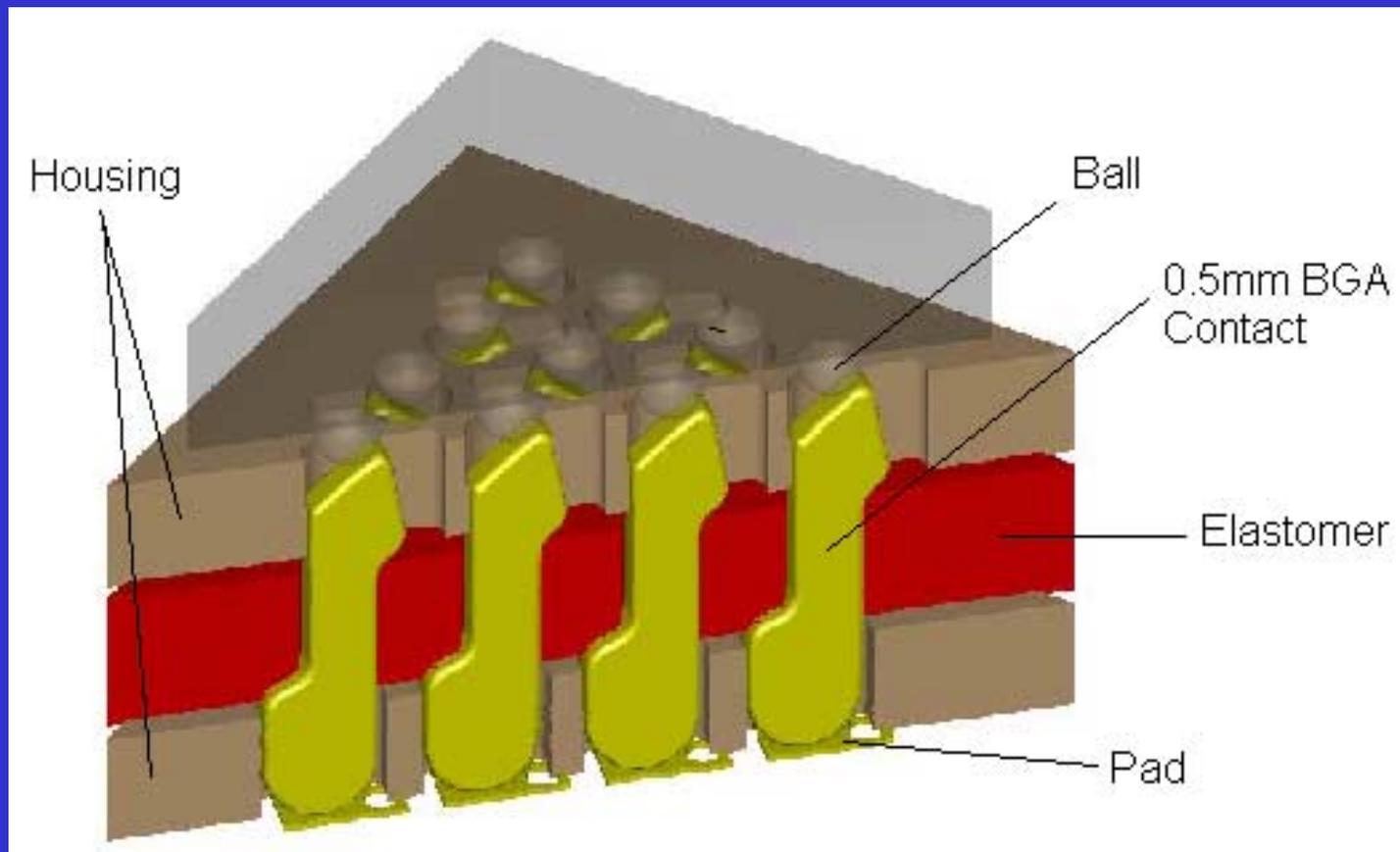
Johnstech™

Discussion Topics

- ▼ Modeled Data
- ▼ Measured Data
- ▼ Comparative Data
- ▼ Equivalent Circuit Model
- ▼ Conclusion

Introduction: 0.5 mm Pitch BGA Contactor

▼ Cross sectional view of a contactor

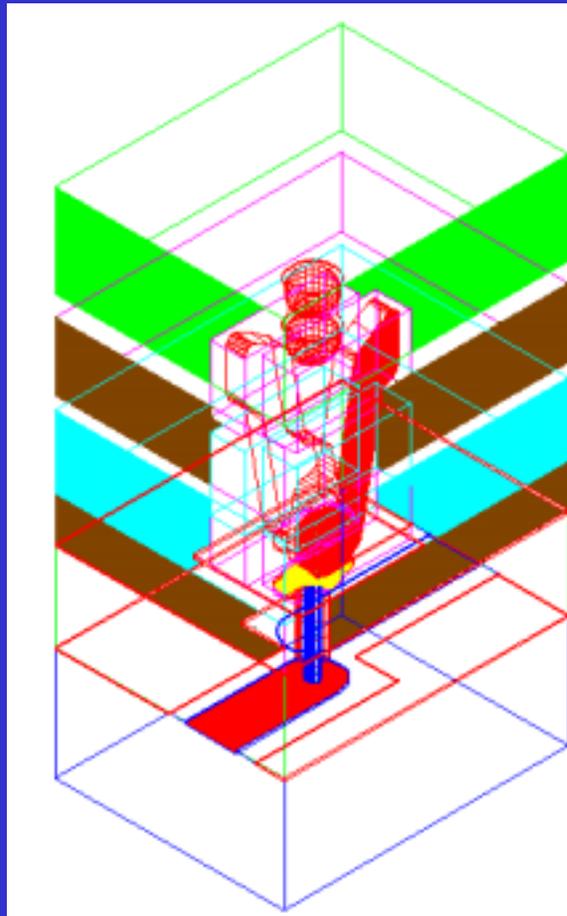


Modeled Data

- ▼ Modeling was done using Agilent HFSS software
- ▼ An AutoCAD drawing, including the actual structure built by GigaTest Labs, was imported into HFSS
- ▼ Data obtained from simulation includes:
 - ▼ Return Loss S_{11}
 - ▼ Insertion Loss S_{21}

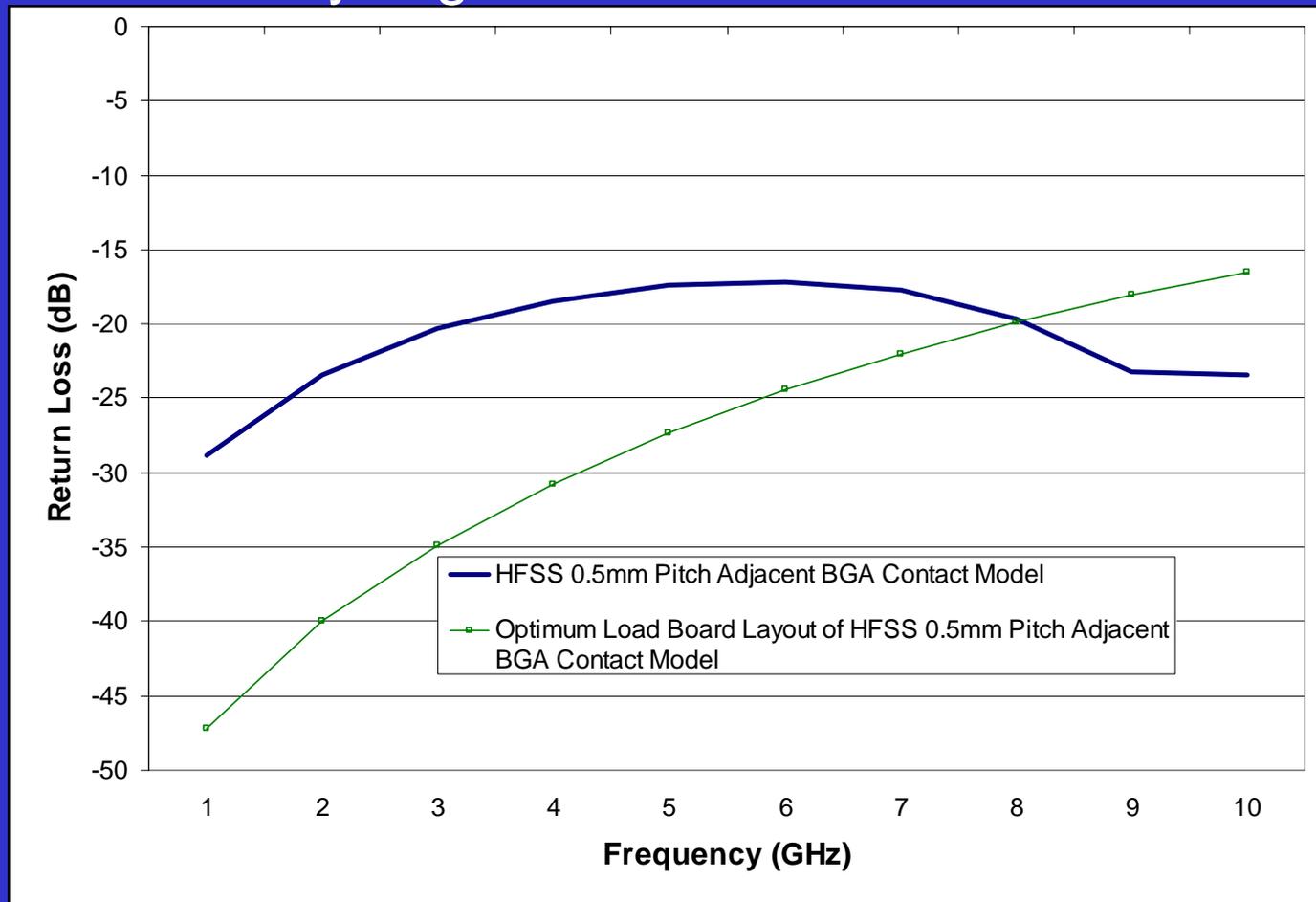
Modeled Data

- ▼ 0.5 mm pitch BGA model from an AutoCAD file



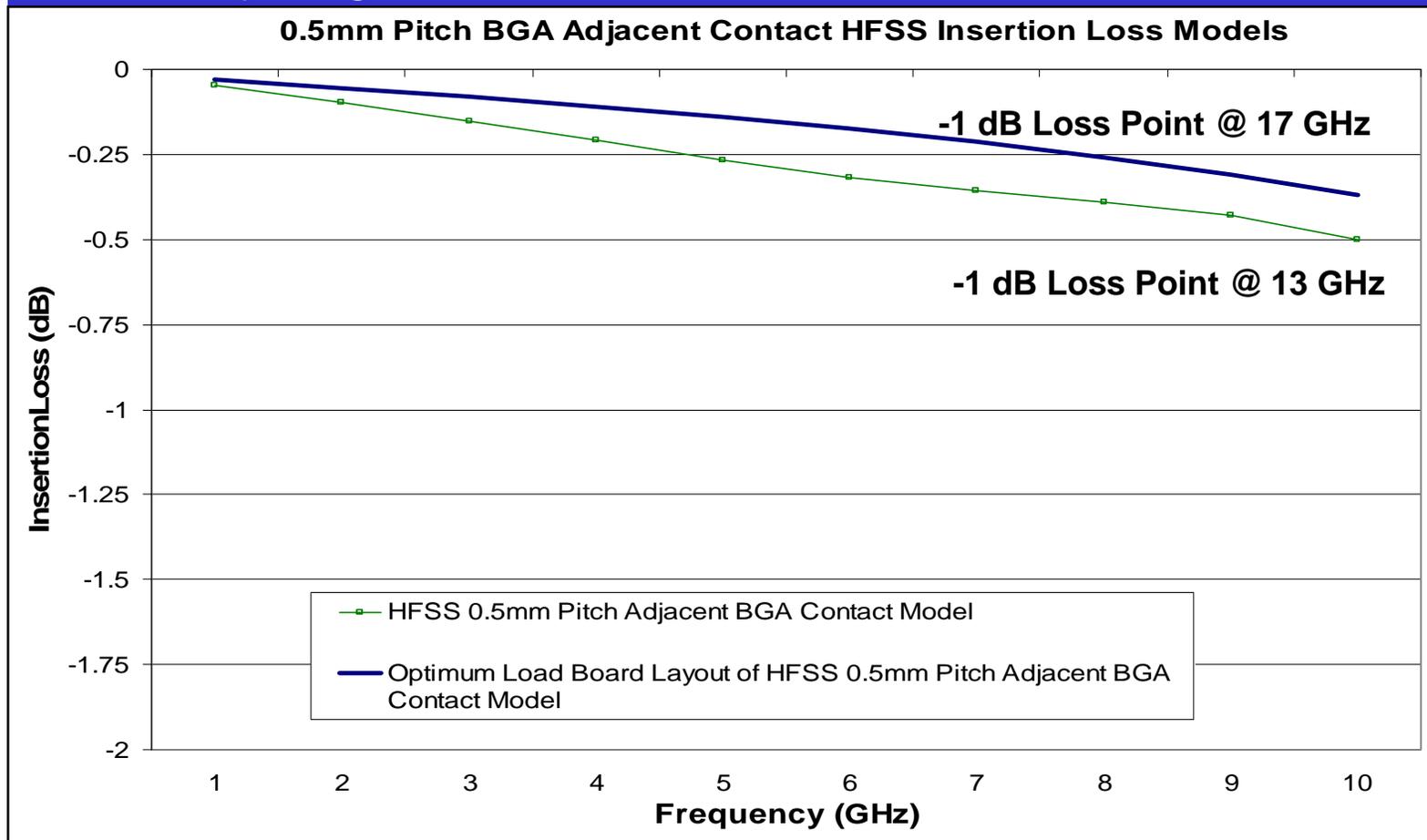
Modeled Data - S_{11}

- ▼ This is data from the HFSS model of return loss by the actual 0.5 mm BGA structure tested by GigaTest Labs



Modeled Data - S_{21} & S_{11}

- ▼ This is data from the HFSS model of return loss by the actual .5 mm BGA structure tested by GigaTest Labs



Modeled Data

▼ HFSS Capabilities

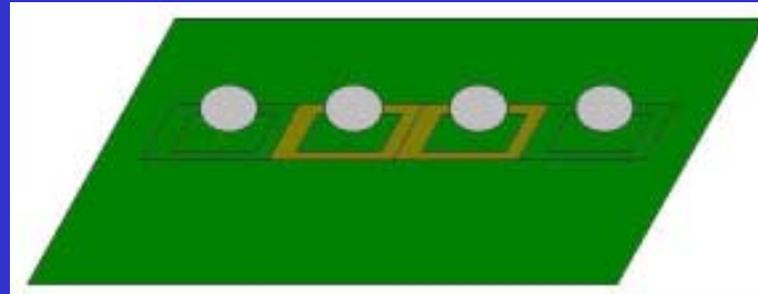
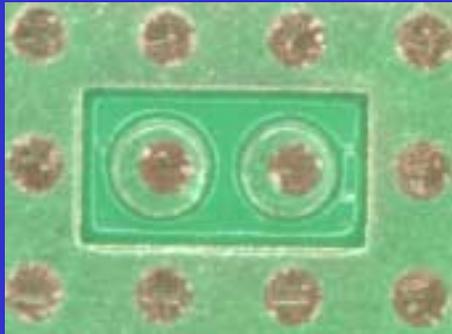
- ▼ Contact design parameters
- ▼ Load board design effects
- ▼ Device pad interactions
- ▼ Expected performance
- ▼ Effects of tolerances
- ▼ Interaction between components in system (device, contactor, handler, etc.)
- ▼ Trends

Measured Data

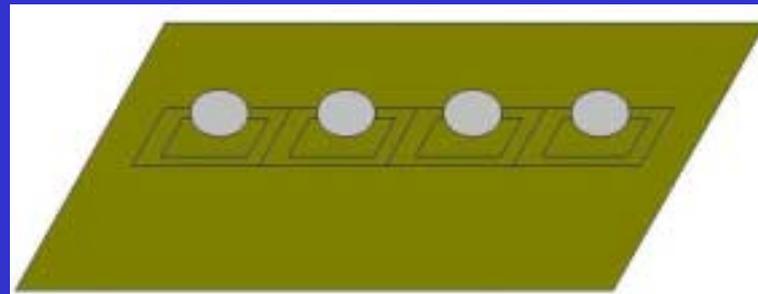
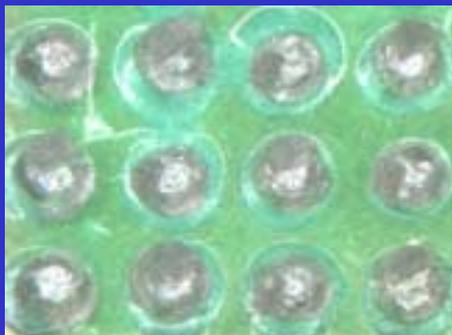
- ▼ GigaTest Labs tested a 0.5 mm pitch Ball Series contactor
- ▼ GigaTest Labs used a surrogate device - Short, Open, Load, Thru (SOLT) to conduct testing
- ▼ Data was measured by GigaTest Labs through probing from the back side of a non-optimized load board

Measured Data

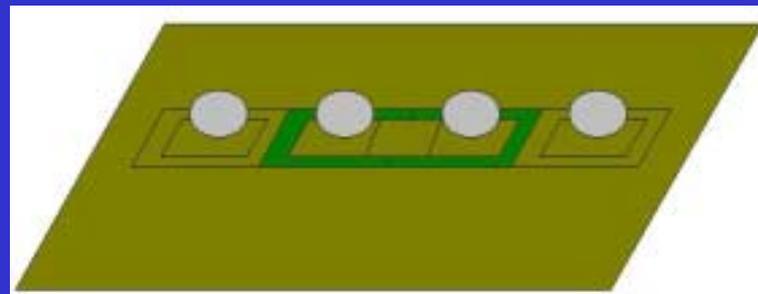
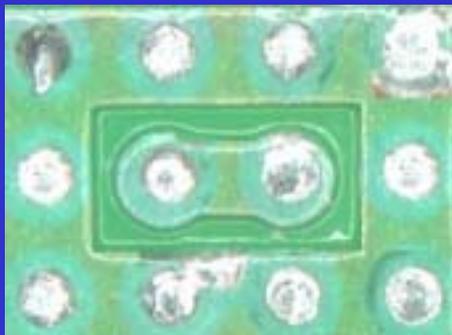
Open



Short



Thru



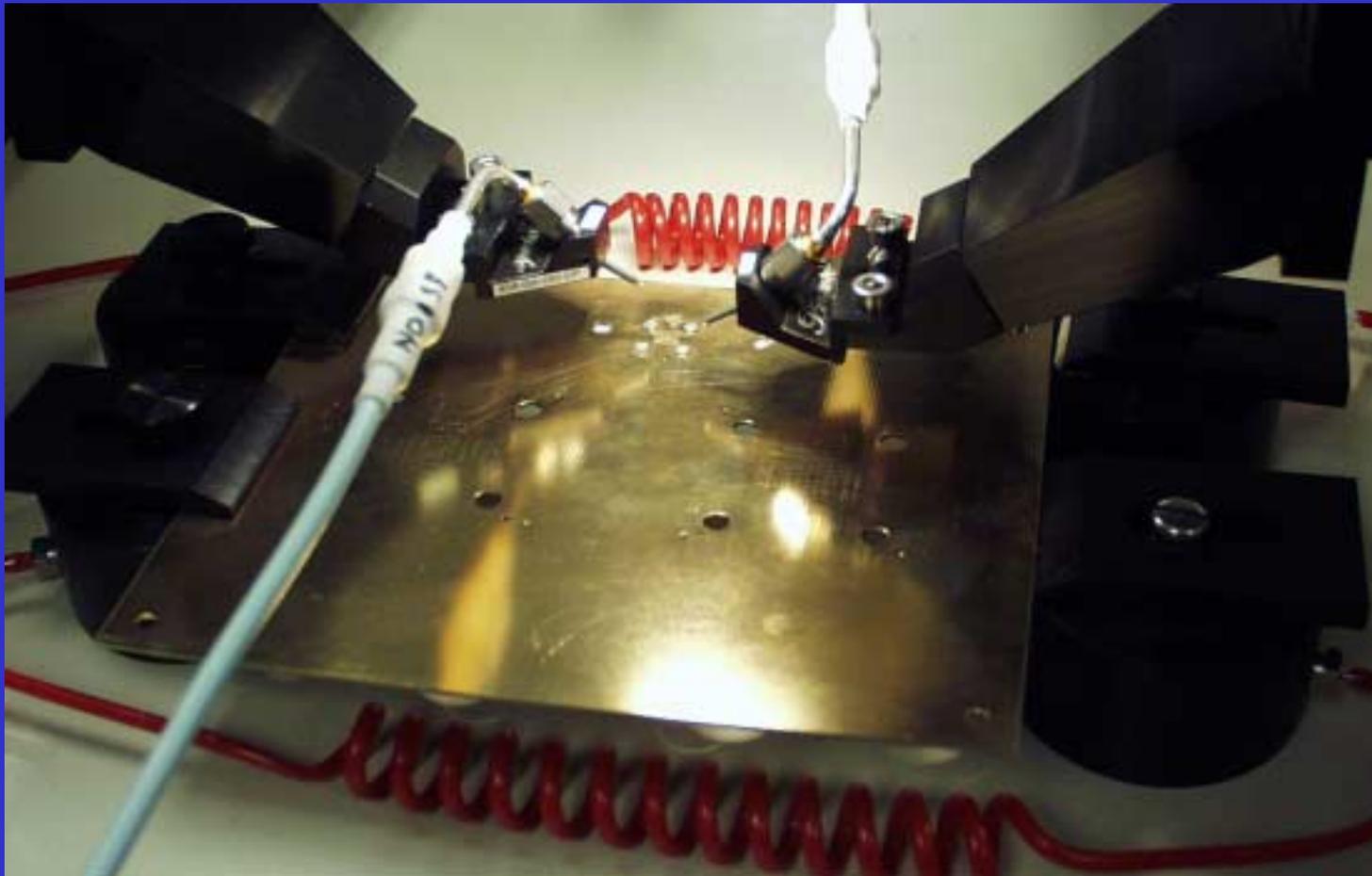
Surrogate

Circuit

Johnstech™

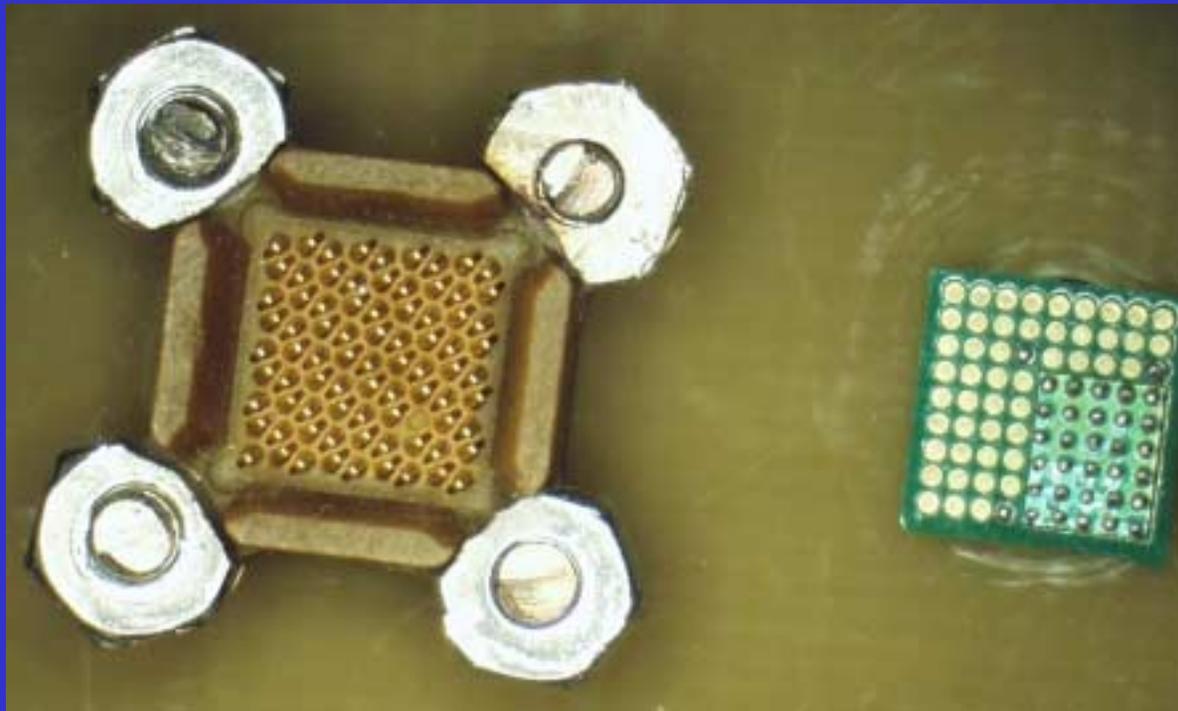
Measured Data

- ▼ GigaTest Labs used a micro probe station for measuring two adjacent contacts S-parameters



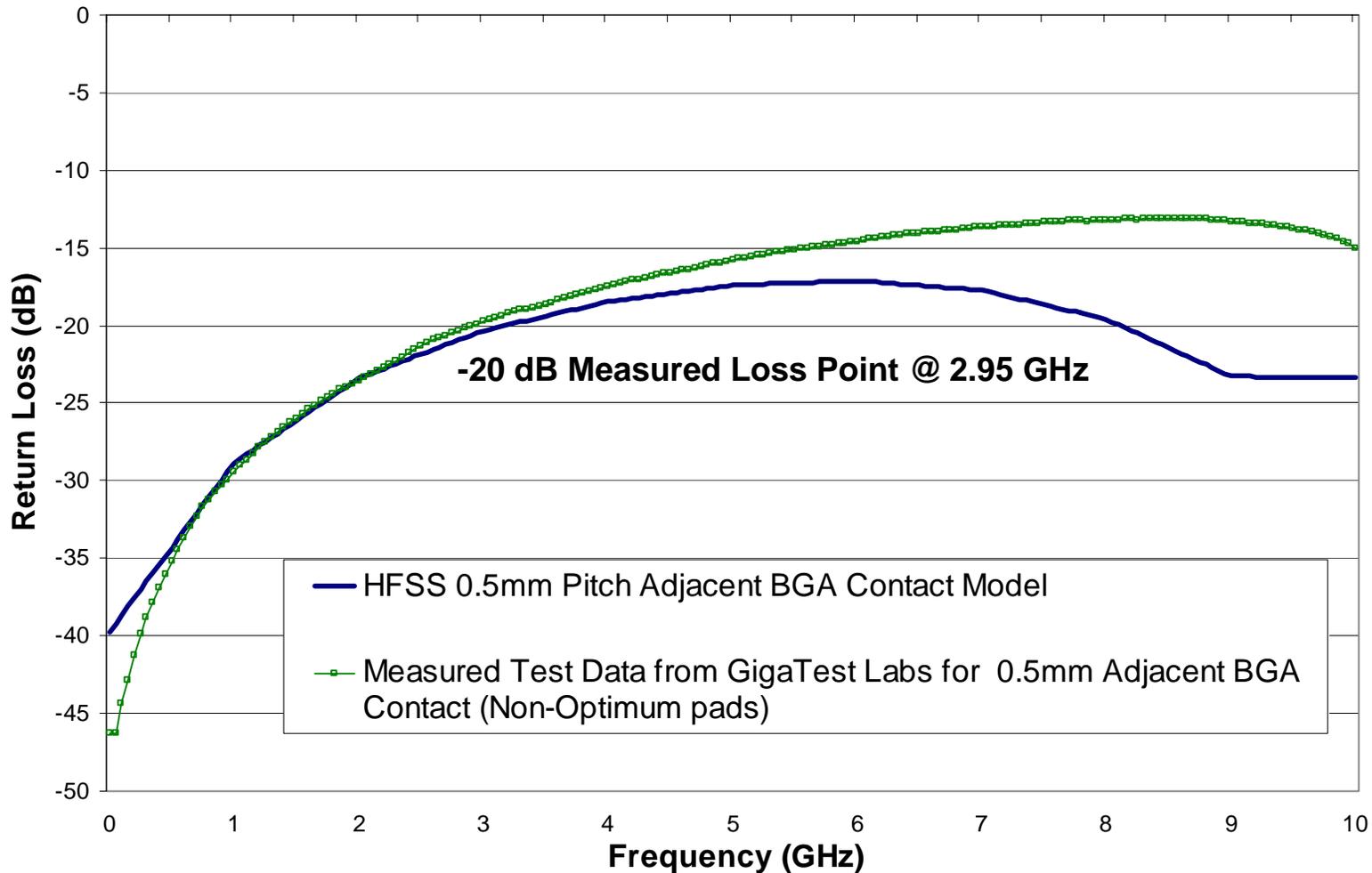
Measured Data

- ▼ The 0.5 mm pitch BGA housing and BGA surrogate package

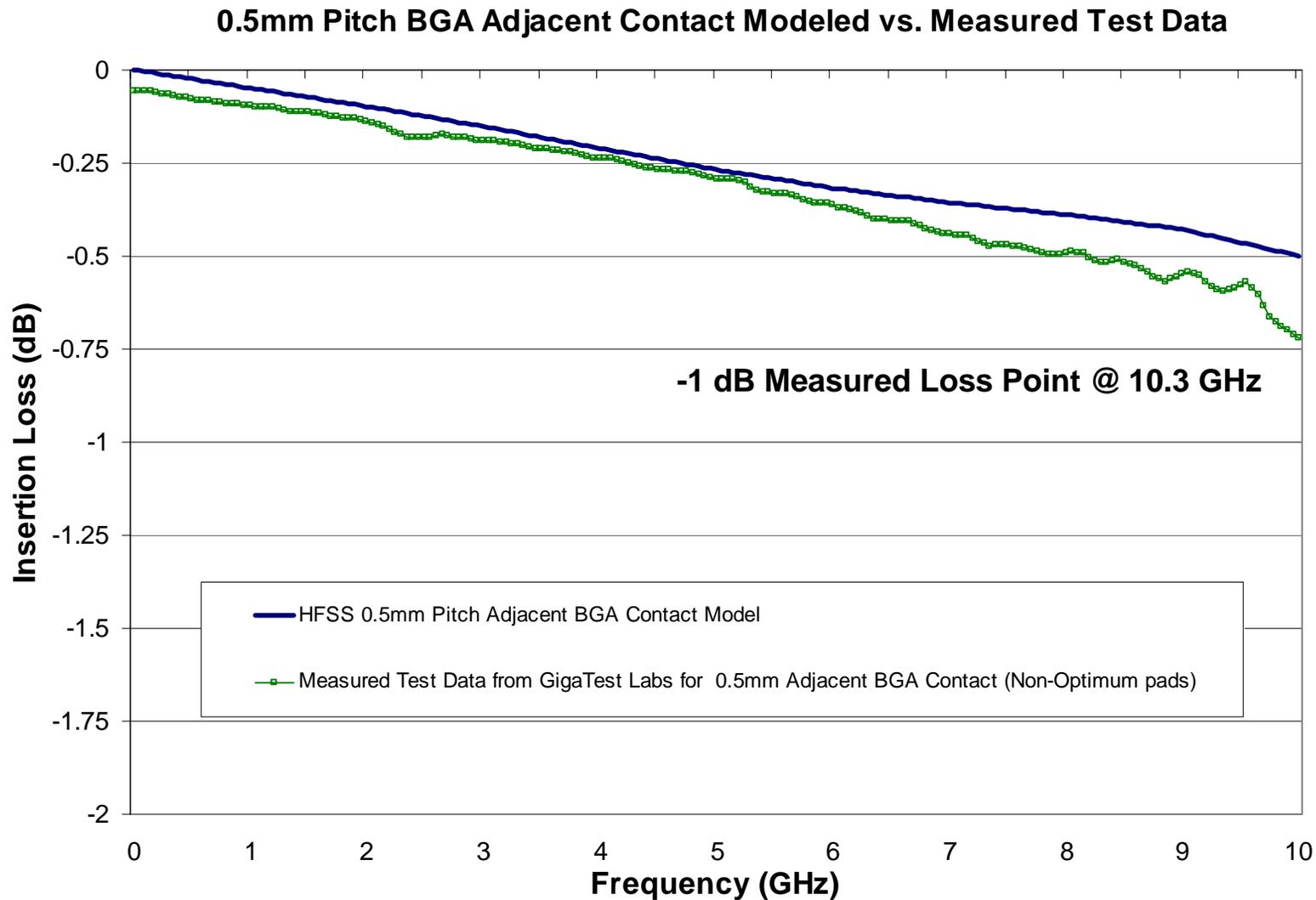


Comparative Data

HFSS Model vs. Measured Test Data for 0.5mm BGA Adjacent Contacts



Comparative Data



Equivalent Circuit Model

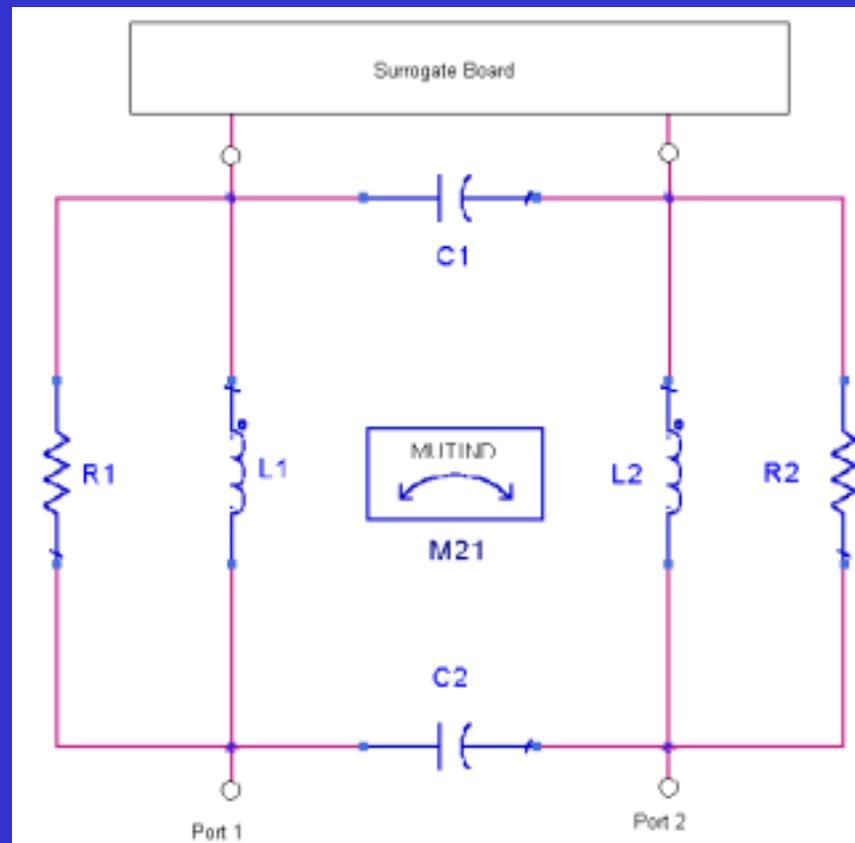
- ▼ Characterize the parasitic effects
- ▼ Simulate the contact with an equivalent circuit for time domain response
- ▼ Integrate the contactor into a system level simulation to:
 - ▼ Reduce test cost and time
 - ▼ Optimize system performance

Equivalent Circuit Model

- ▼ Measure the S-parameters for short-, open- and thru- fixtures from two adjacent contacts
- ▼ Use measured data and Agilent Advanced Design System (ADS) for model extraction and verification
- ▼ Compare measured and ADS simulated insertion and return loss

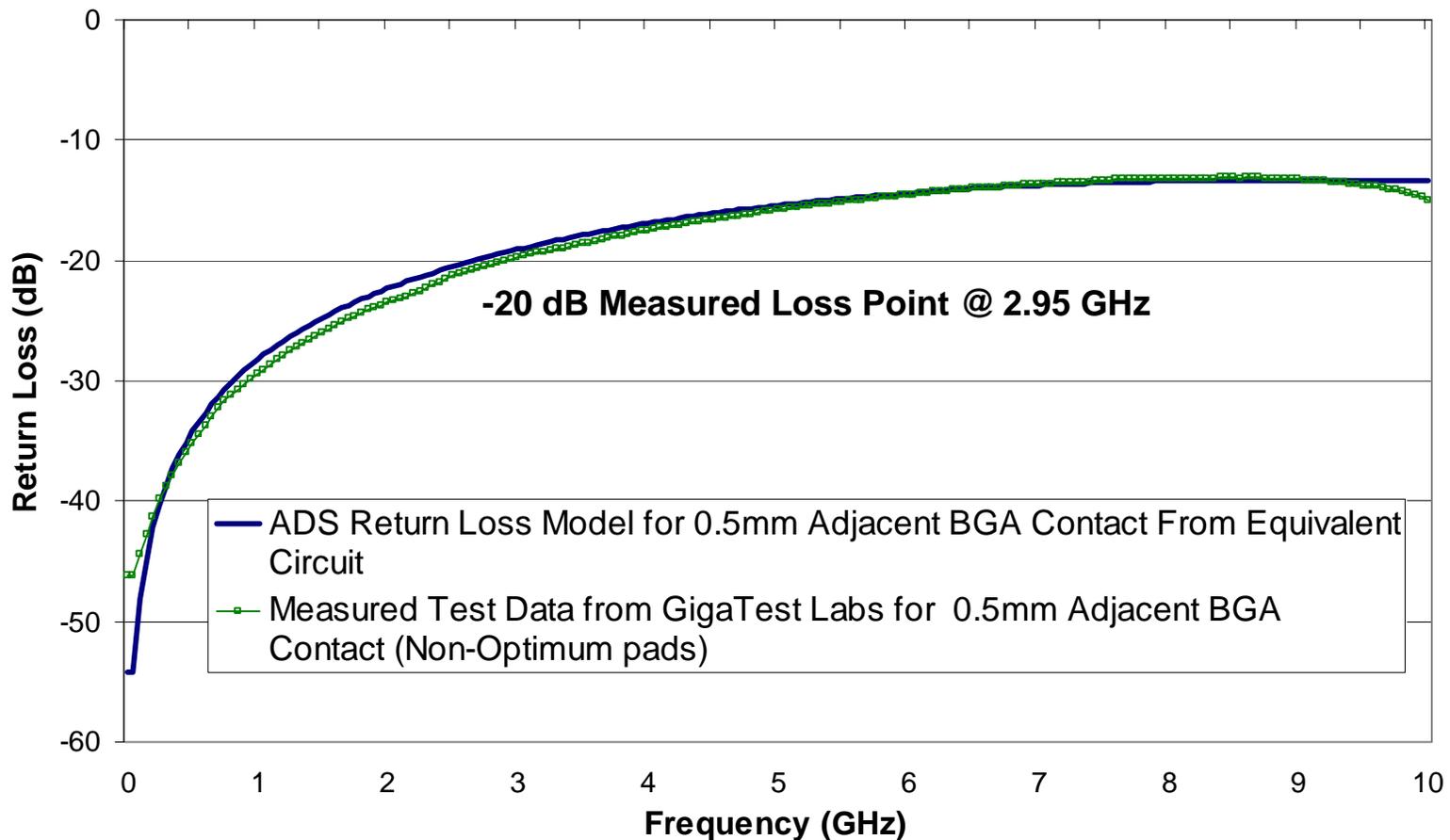
Equivalent Circuit Model

- ▼ This figure shows the Equivalent Circuit Model for two adjacent 0.5 mm BGA contacts



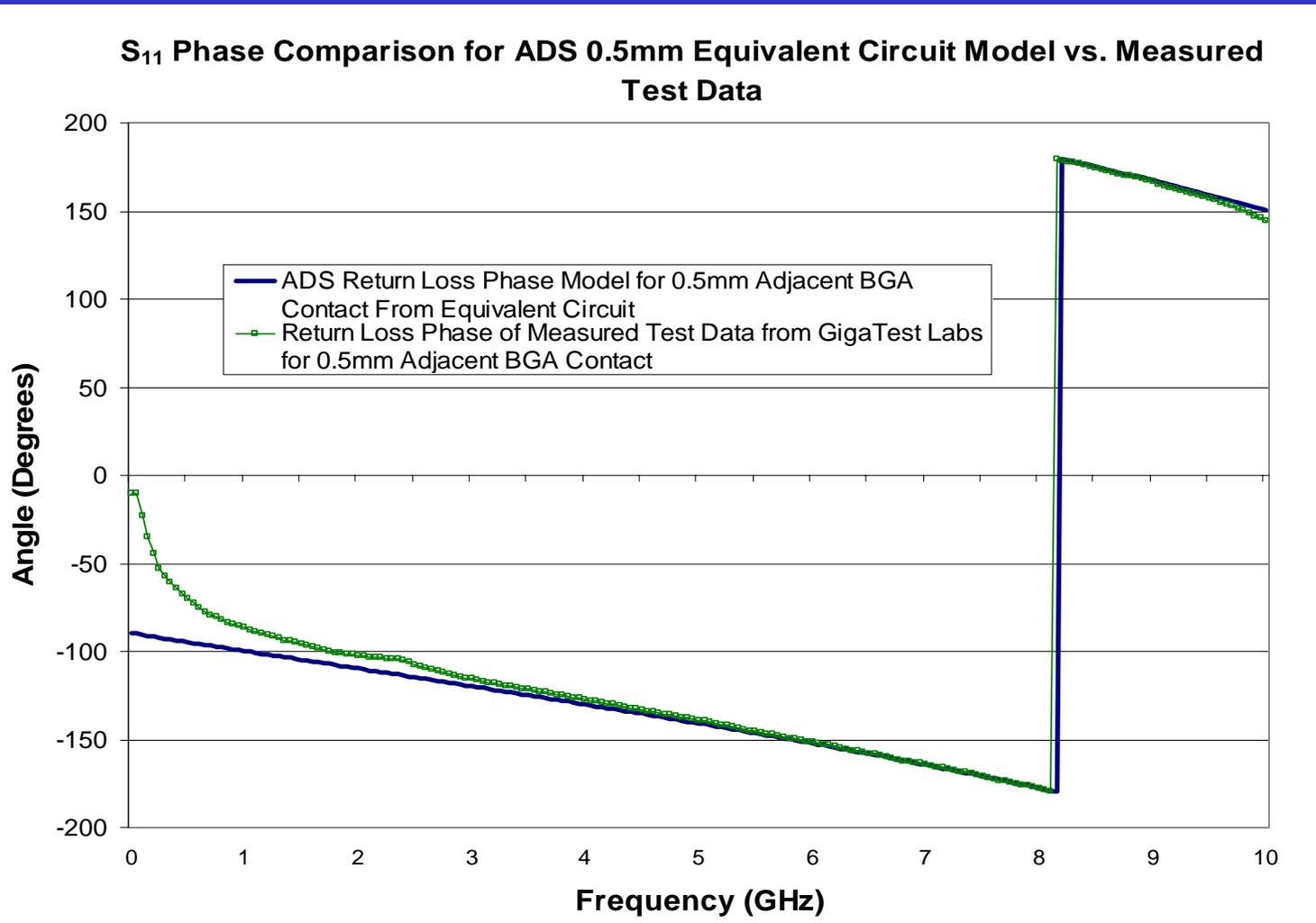
Equivalent Circuit Model

0.5mm Pitch BGA Adjacent Contact ADS Equivalent Circuit Model vs. Measured Test Data

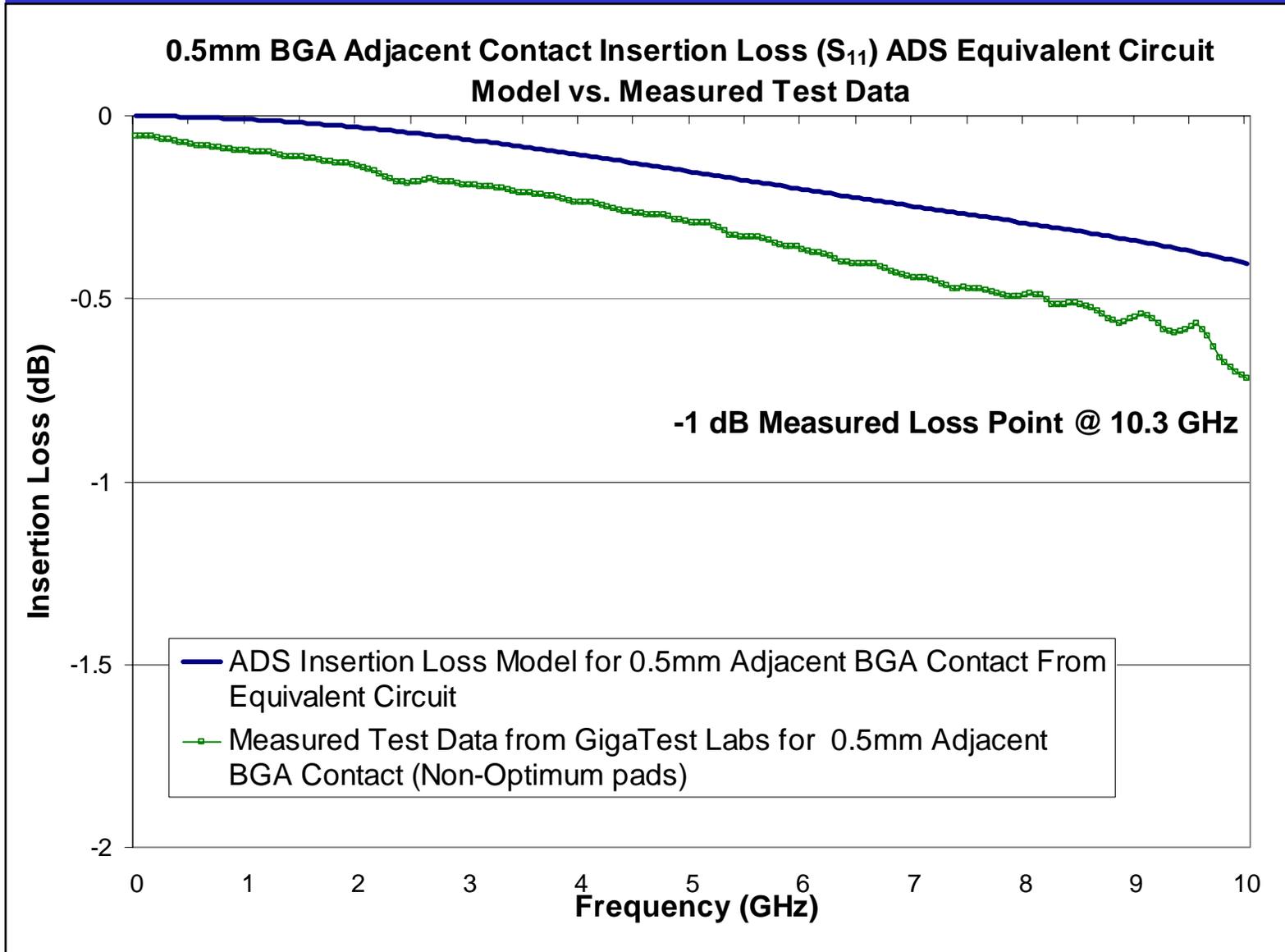


Equivalent Circuit Model

- ▼ Phase comparison shows that the contact is linear over the frequency model

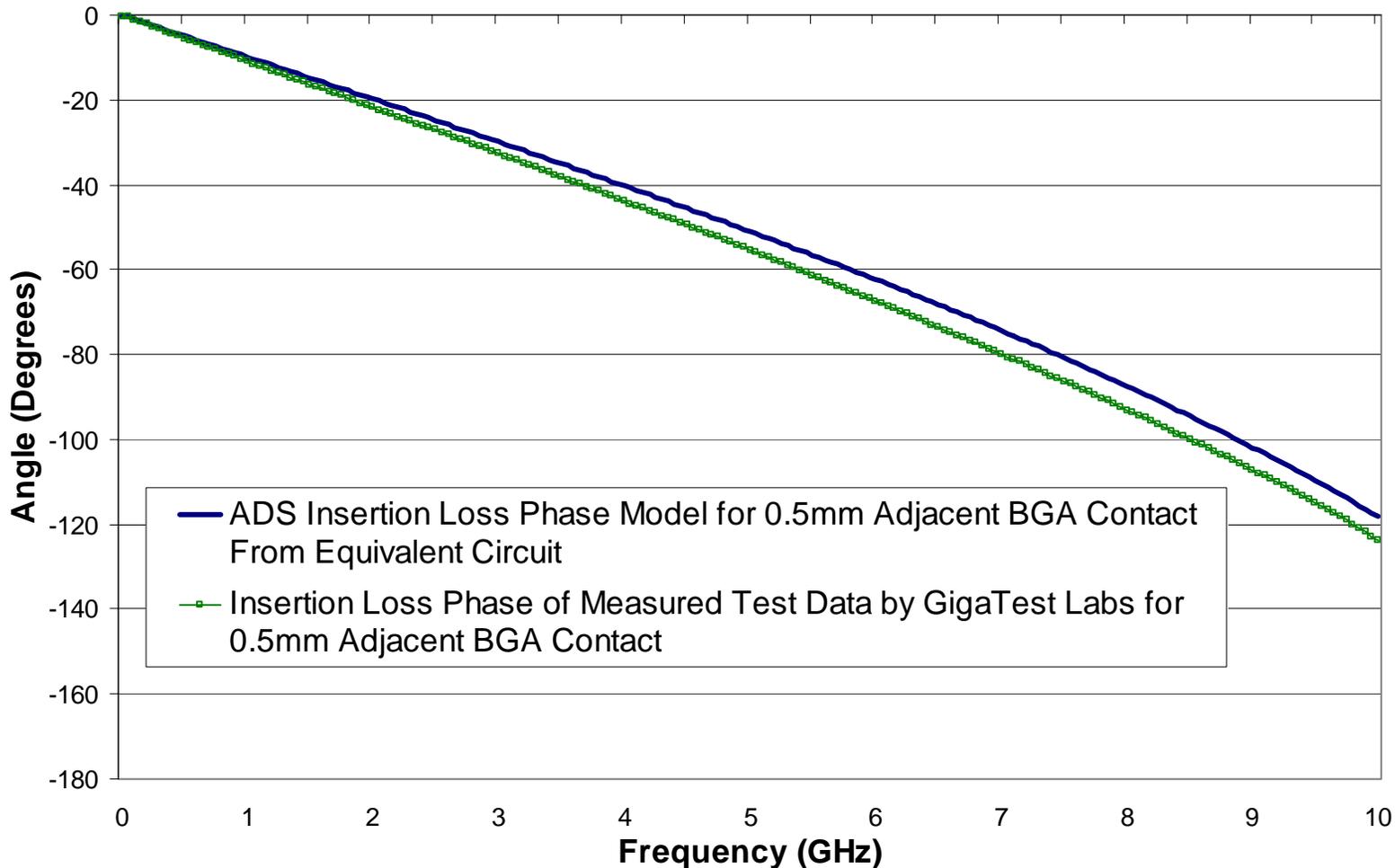


Equivalent Circuit Model Development



Equivalent Circuit Model Development

S₂₁ Phase Comparison for ADS 0.5mm BGA Equivalent Circuit Model vs. Measured Test Data



Conclusion

- ▼ For leading edge RF applications such as 0.5 mm pitch, modeling is helpful to achieve optimal system performance
- ▼ Accurate equivalent circuit models can represent contact behavior and help in determining complete system response
- ▼ Modeling can help RF engineers save time and money in development by correctly predicting system results and eliminating or reducing hardware builds and test iterations

Leaded 2 mm Contactors: Measuring and Modeling to 10 GHz

Tom Strouth, Orlando Bell, Gary Otonari, Eric Bogatin

GigaTest Labs, www.GigaTest.com

and

Jeff Sherry

[Johnstech](http://Johnstech.com), www.Johnstech.com

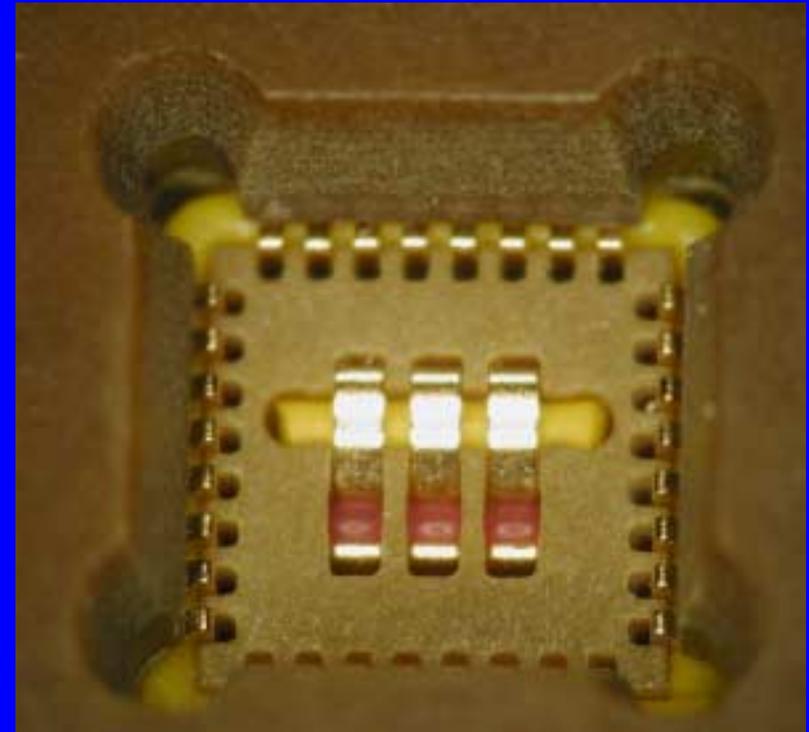
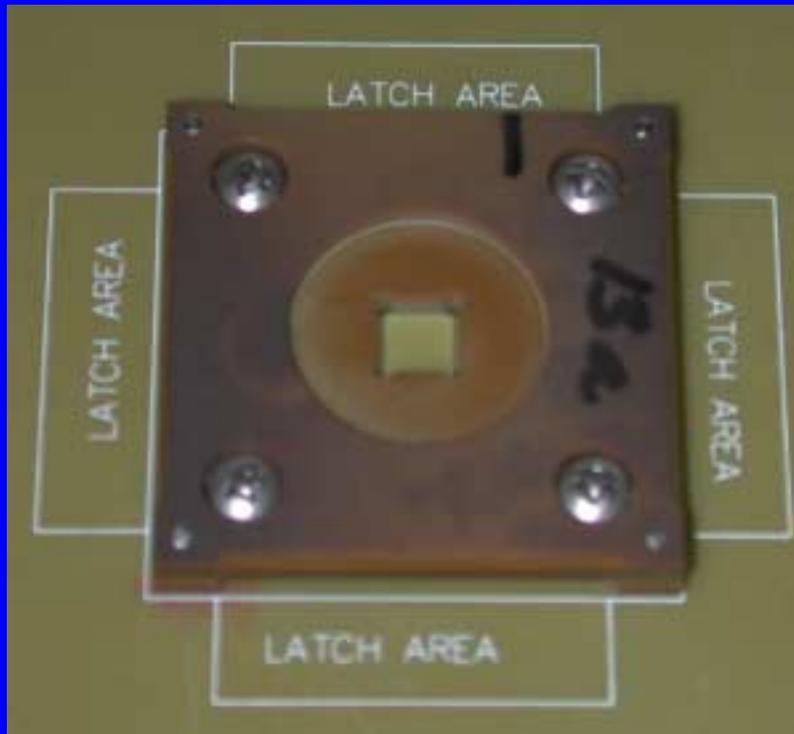
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Outline

- **Contactors**
- **Fixturing**
- **Measurement set up**
- **Modeling process**
- **Results**
- **Using the model for simulation**

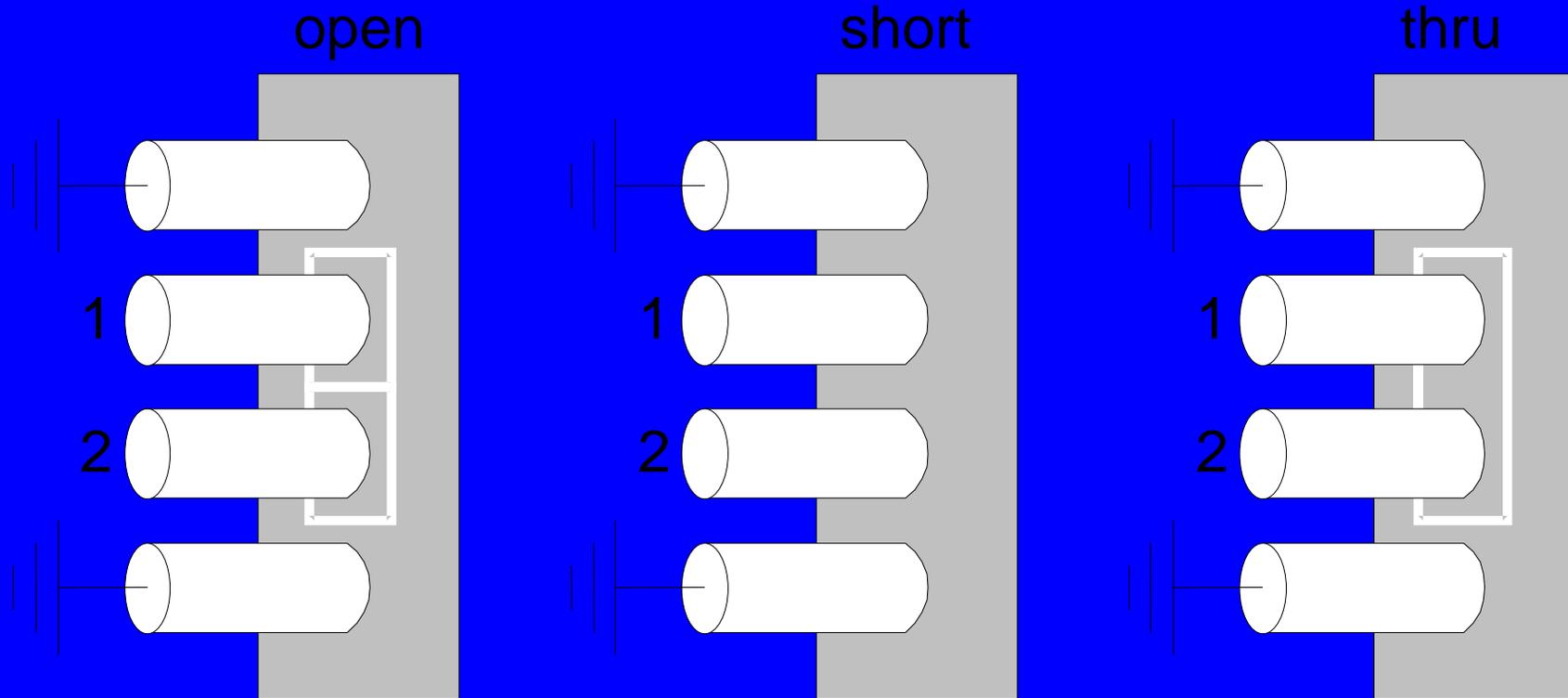
32 lead MLP2 Contactor



Analysis

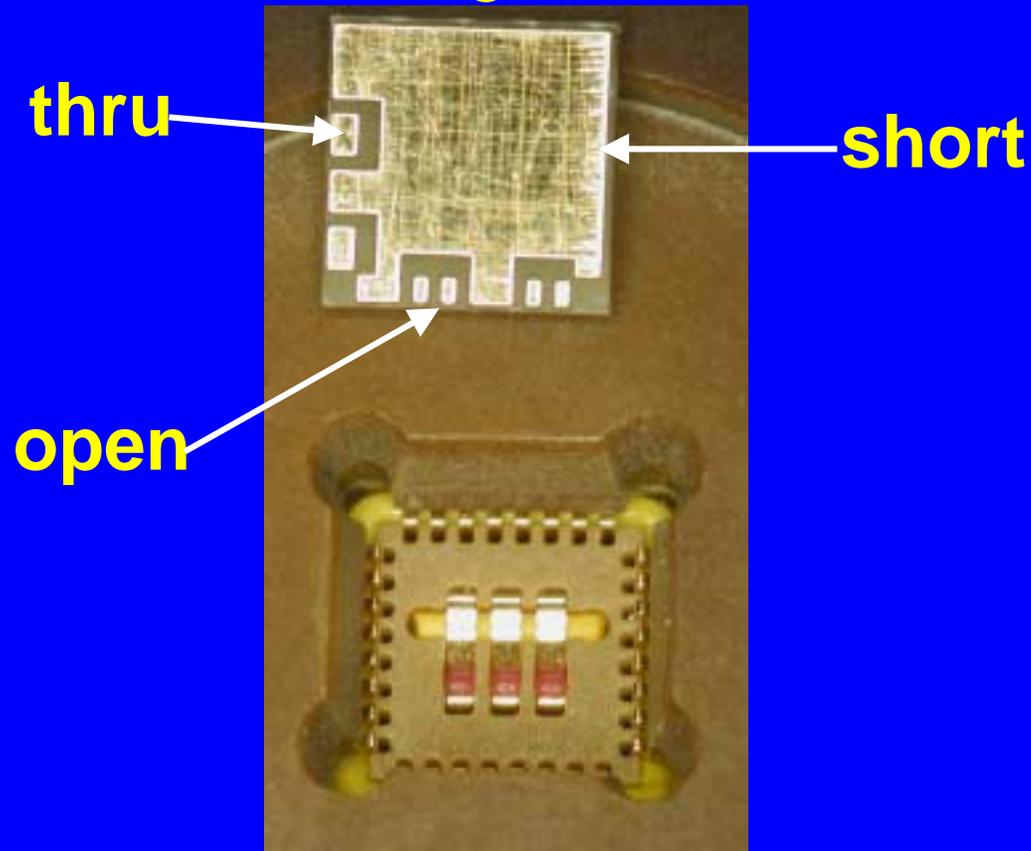
- Goal
 - ✓ Create an equivalent circuit model for two adjacent leads that predicts the measured S parameters
 - ✓ Use this verified, high bandwidth model for performance evaluation
- Strategy
 - ✓ Use measurements of open, short, thru topologies
 - ✓ De-embed the fixturing
 - ✓ Use simplest model for accurate, 10 GHz bandwidth
 - ✓ Use SPICE model of de-embedded contactor for performance simulation

Measurement Configurations

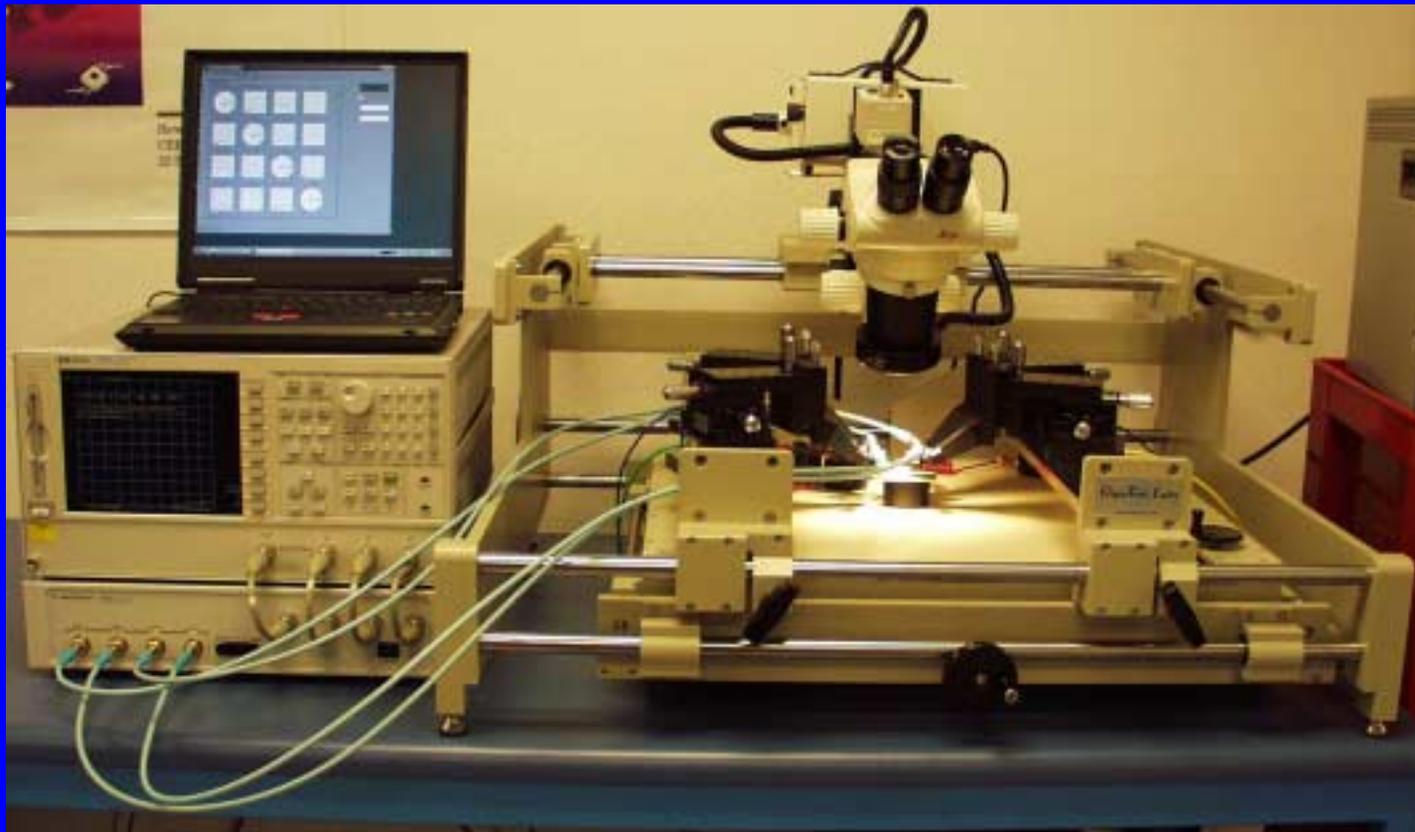


Surrogate Package:

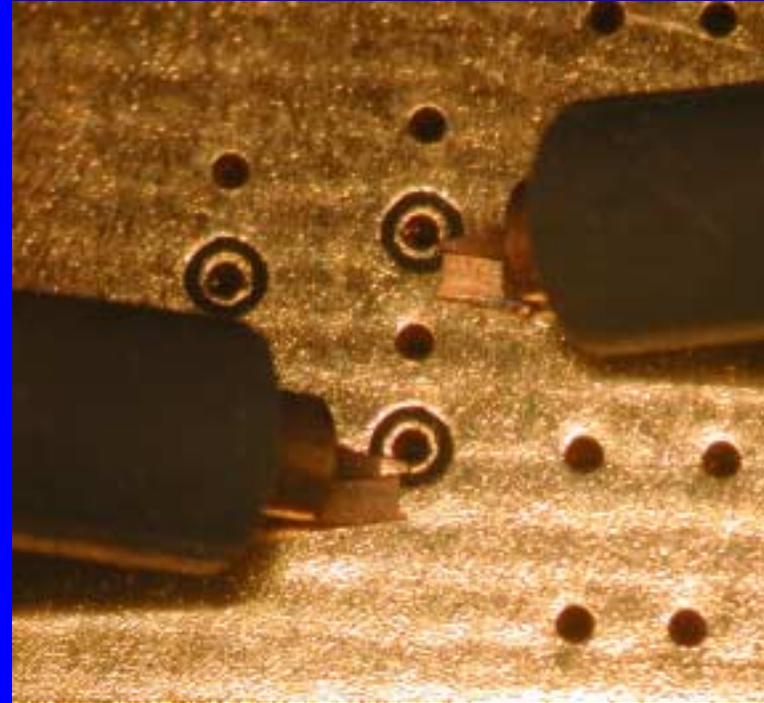
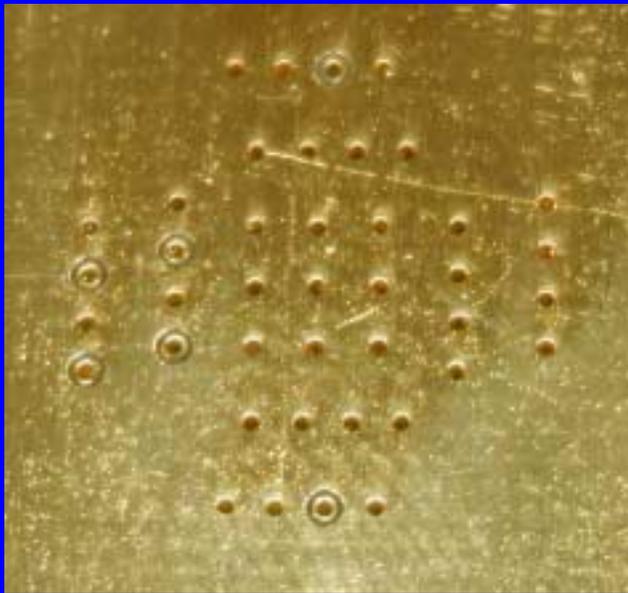
Enables configuring open, short, thru connections for edge and corner leads



Instrument Set Up

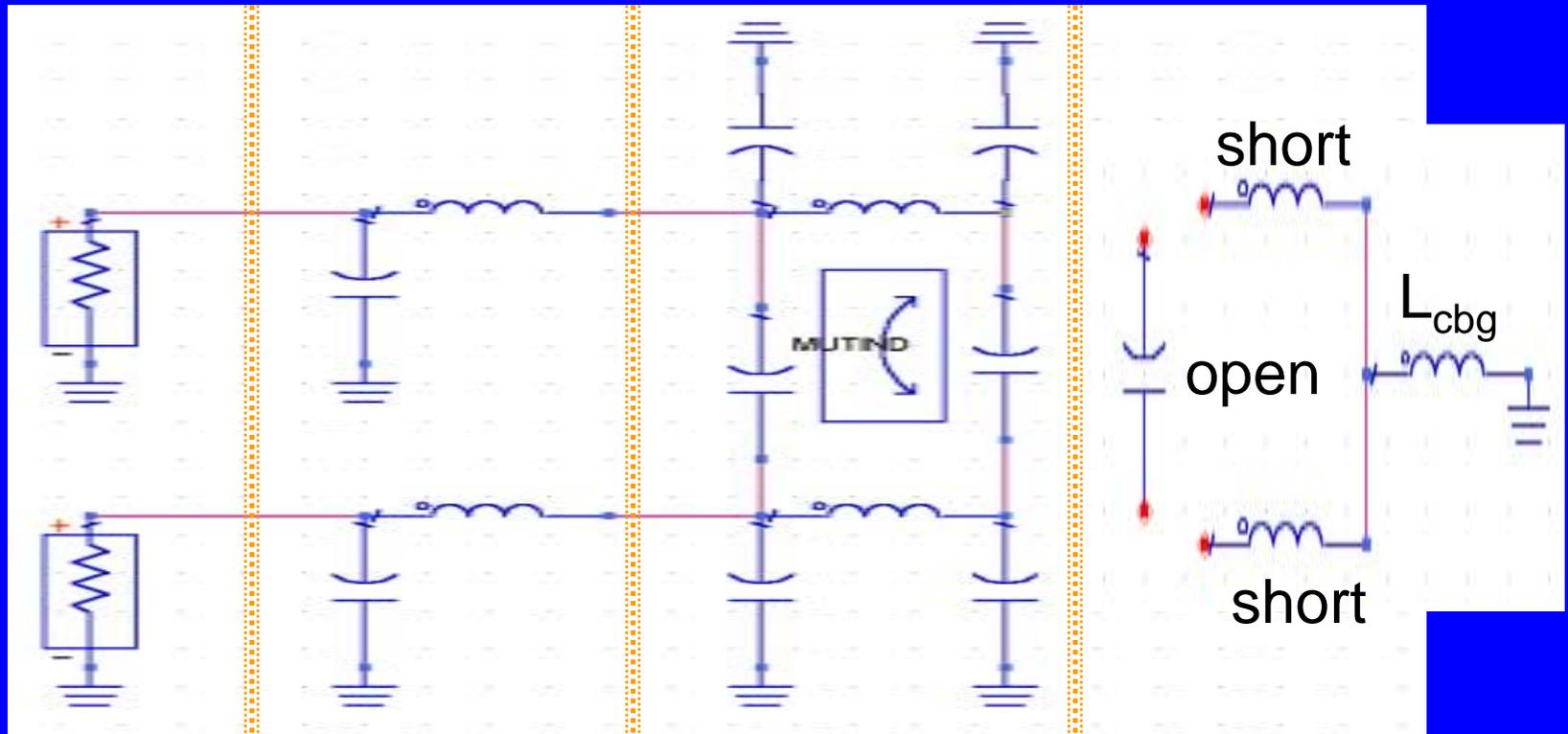


Probing From the Back Side



Probing using microprobes and a
GigaTest Probe Station

Modeling the System with Agilent ADS



VNA

Fixture board

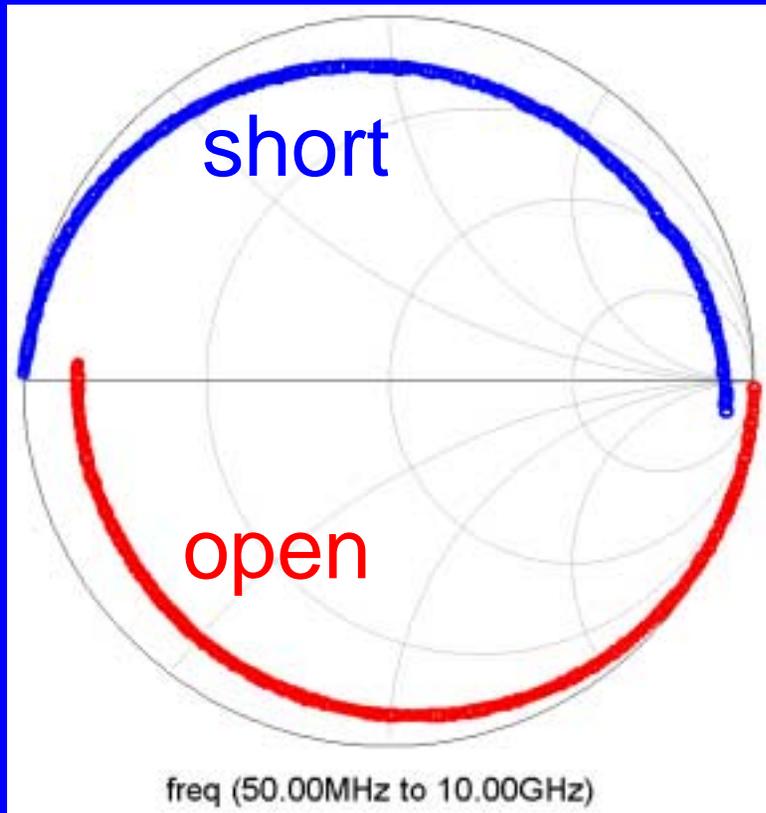
Pads and contactor

Surrogate package

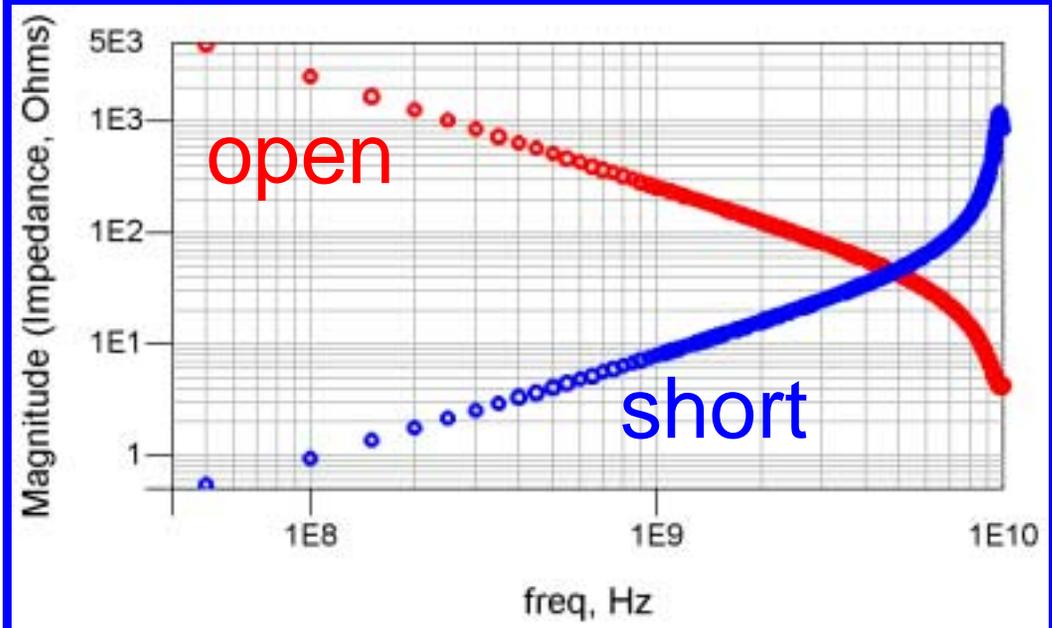
Methodology

- Measure S parameters of calibration vias in bare fixture board
- Extract model for just the fixture
- Select two adjacent corner leads (longest leads)
- Measure open, short, thru for the pair of leads
- Extract model of contactor pins and surrogate package
- Use de-embedded contactor circuit model to simulate performance

Corner Leads (worse case): Open/short Measurements

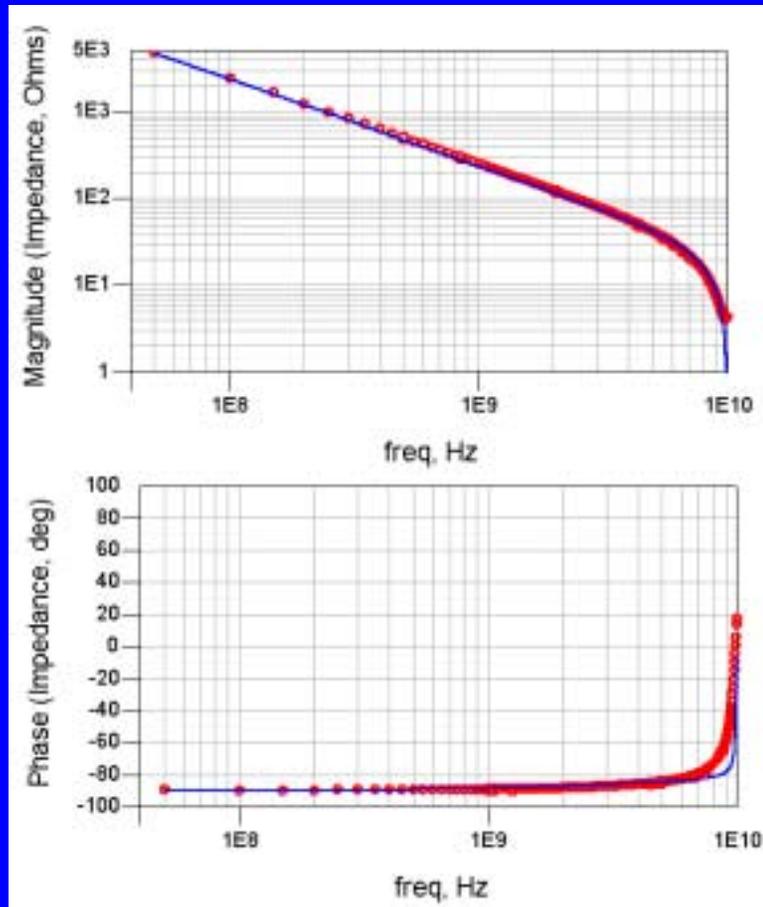


$$Z = 50 \frac{1+S}{1-S}$$

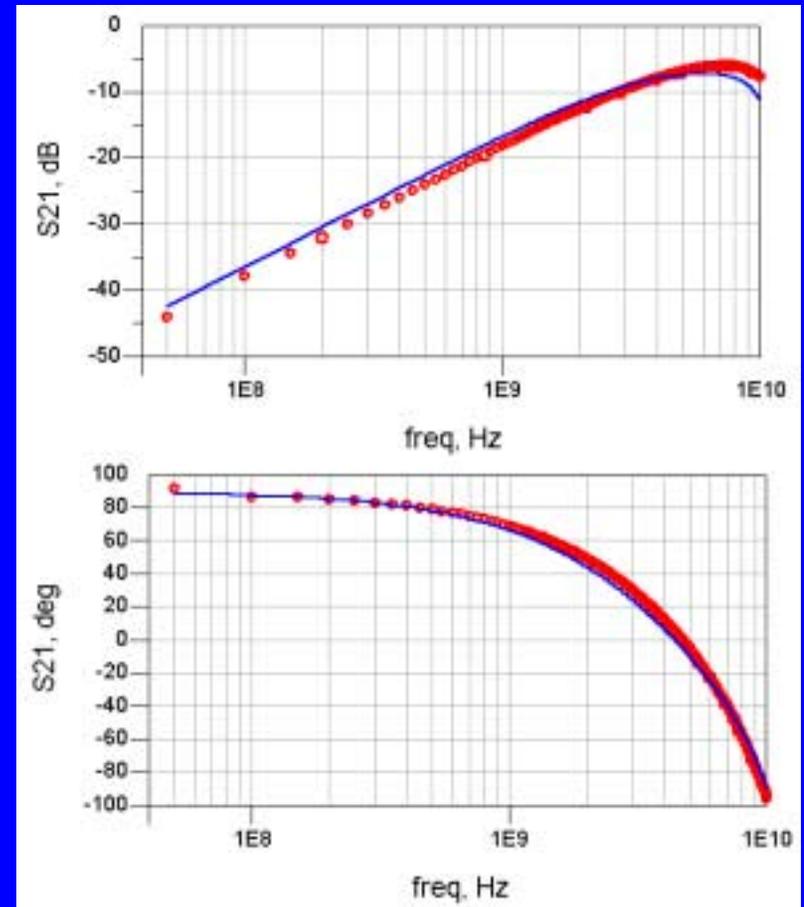


Optimized Model: Open

Impedance of one trace



Coupling between traces

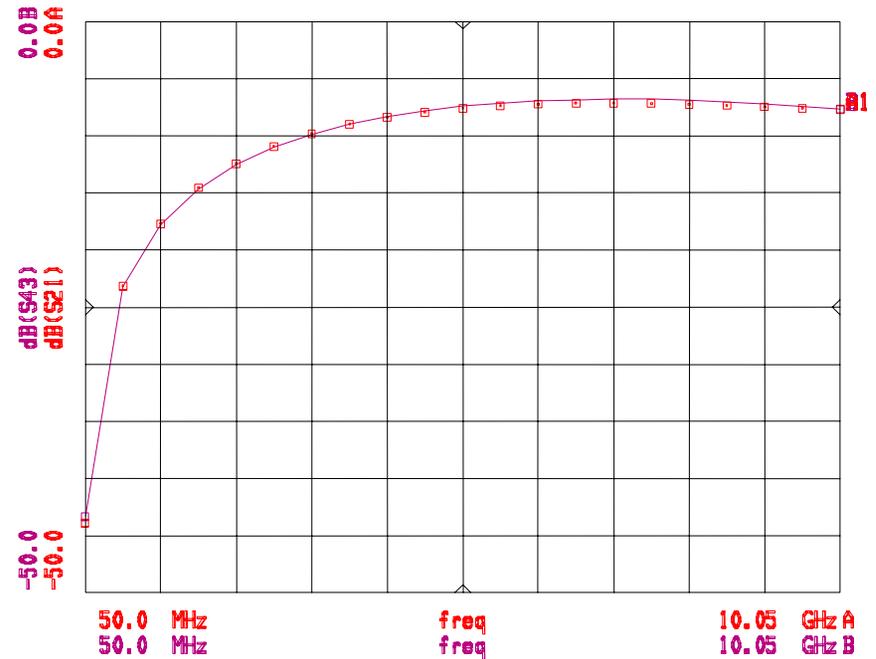
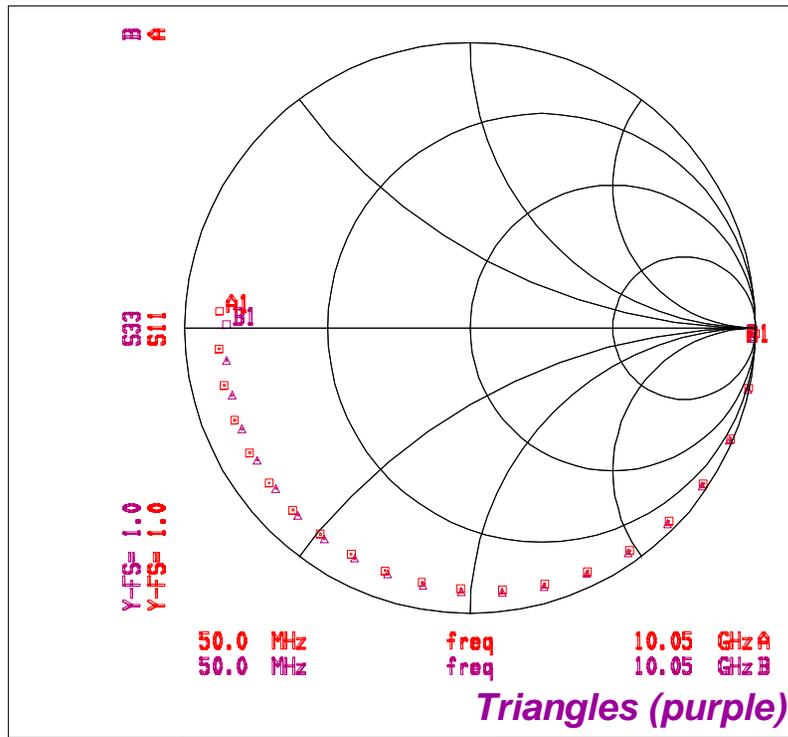


Solid Line is Simulated

Optimized Model: Open

Reflection

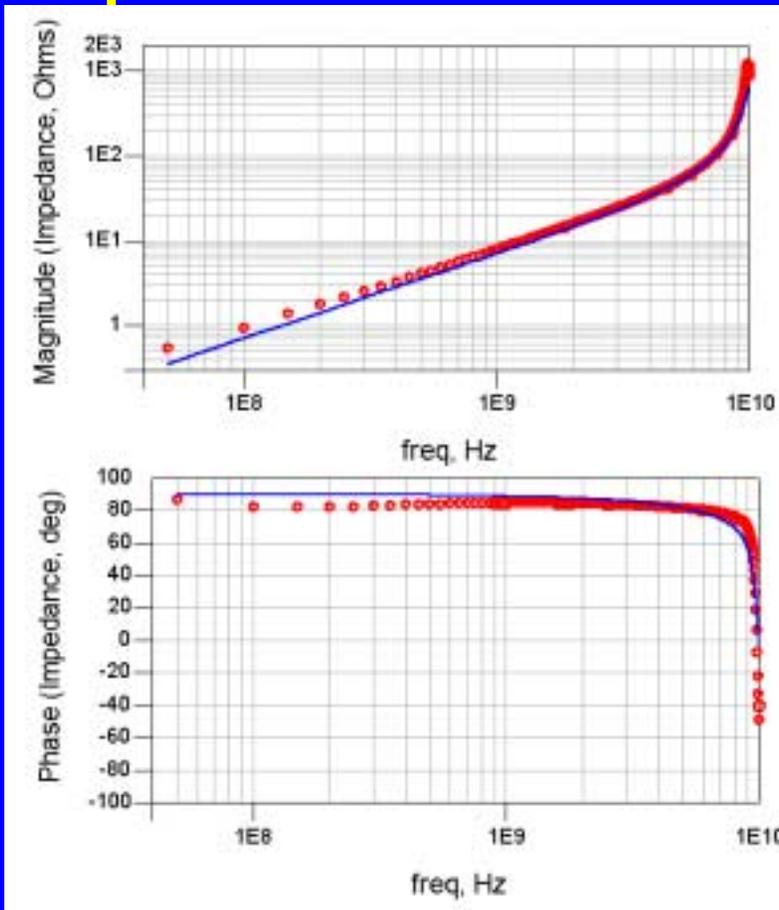
Transmission



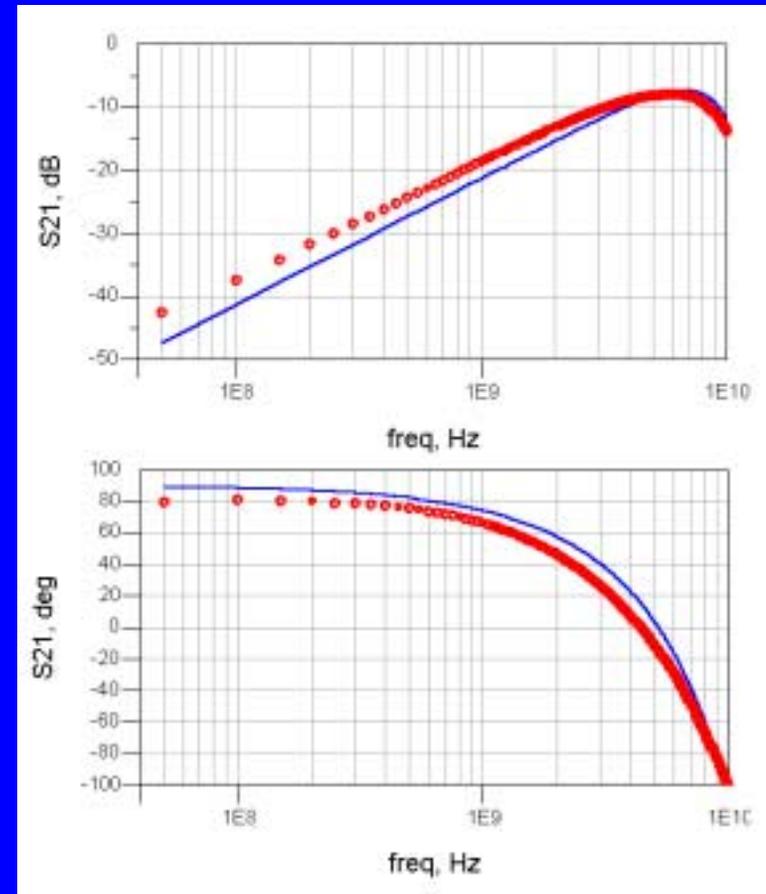
Open provides mutual capacitance info

Optimized Model: Short

Impedance of one trace



Coupling between traces

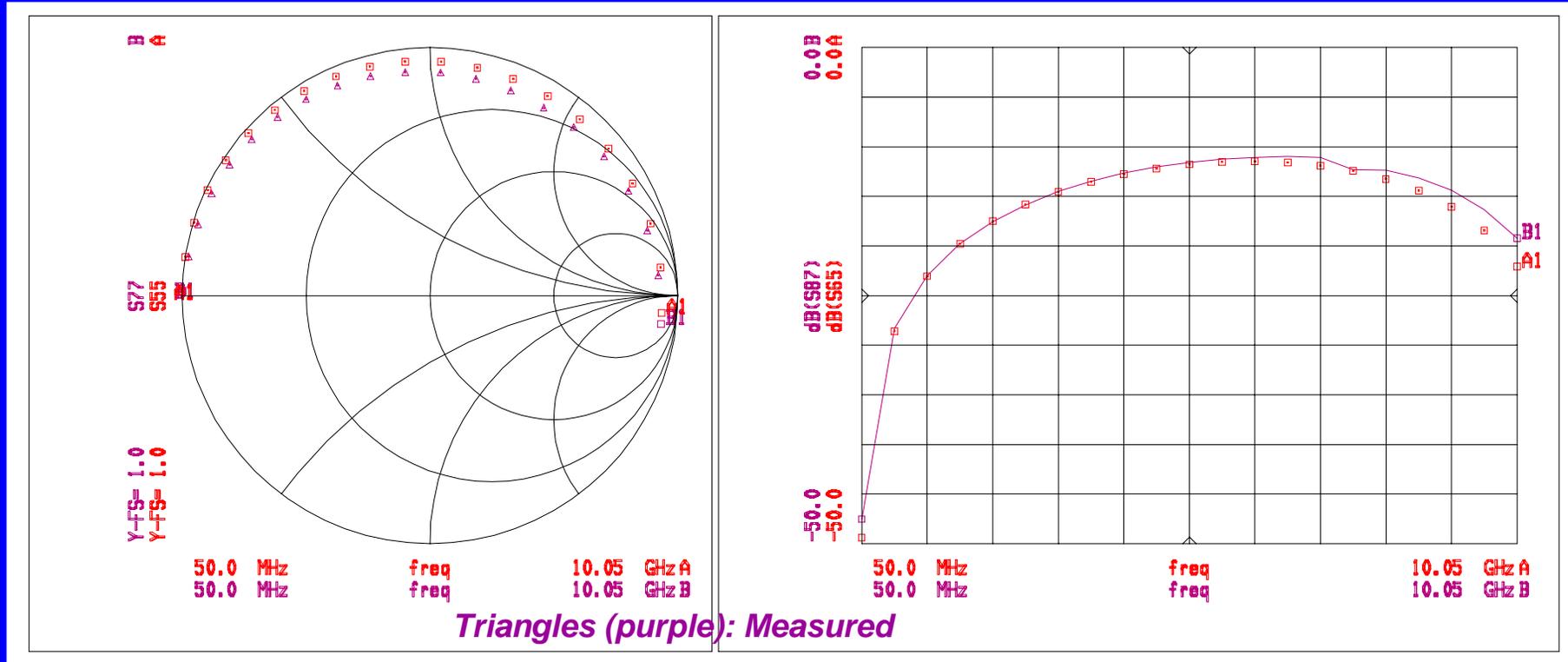


Solid Line is Simulated

Optimized Model: Short

Reflection

Transmission (coupling)

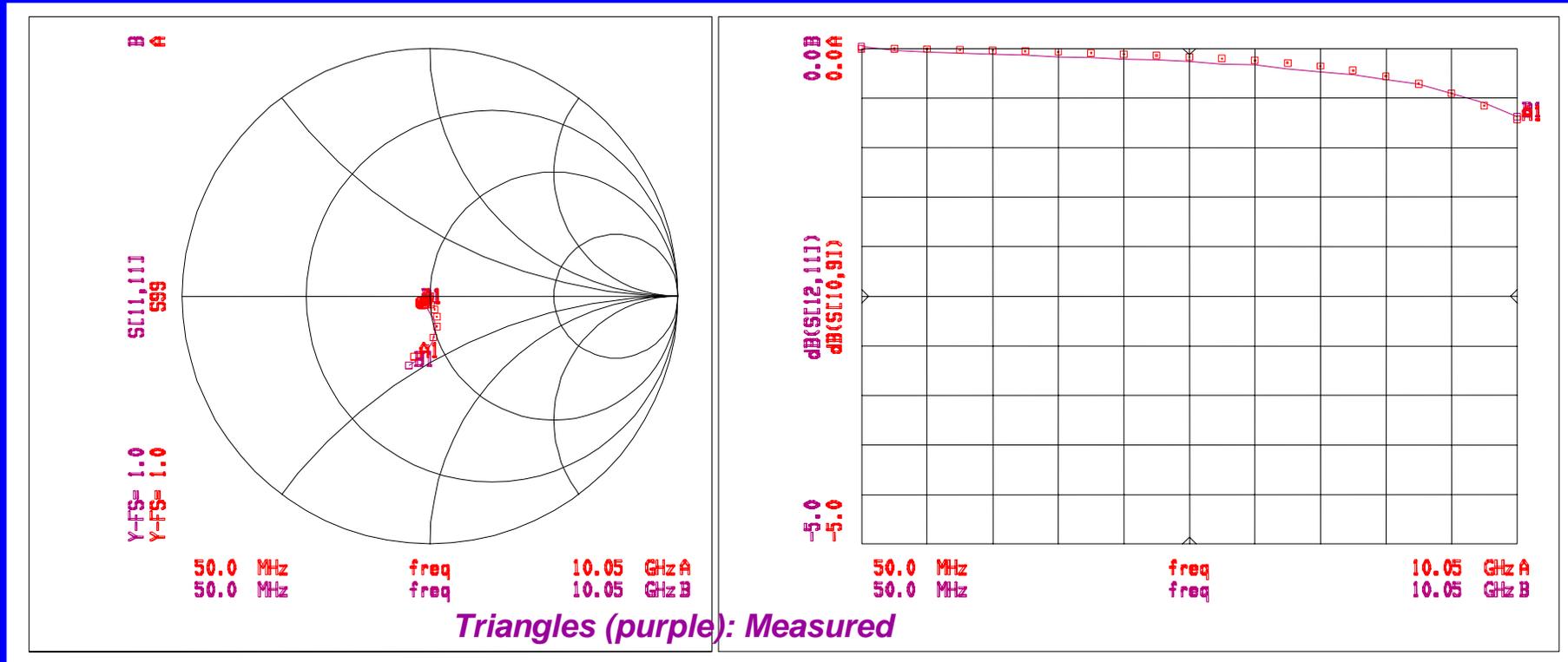


Short provides mutual inductance info

Optimized Model: Loop-Thru

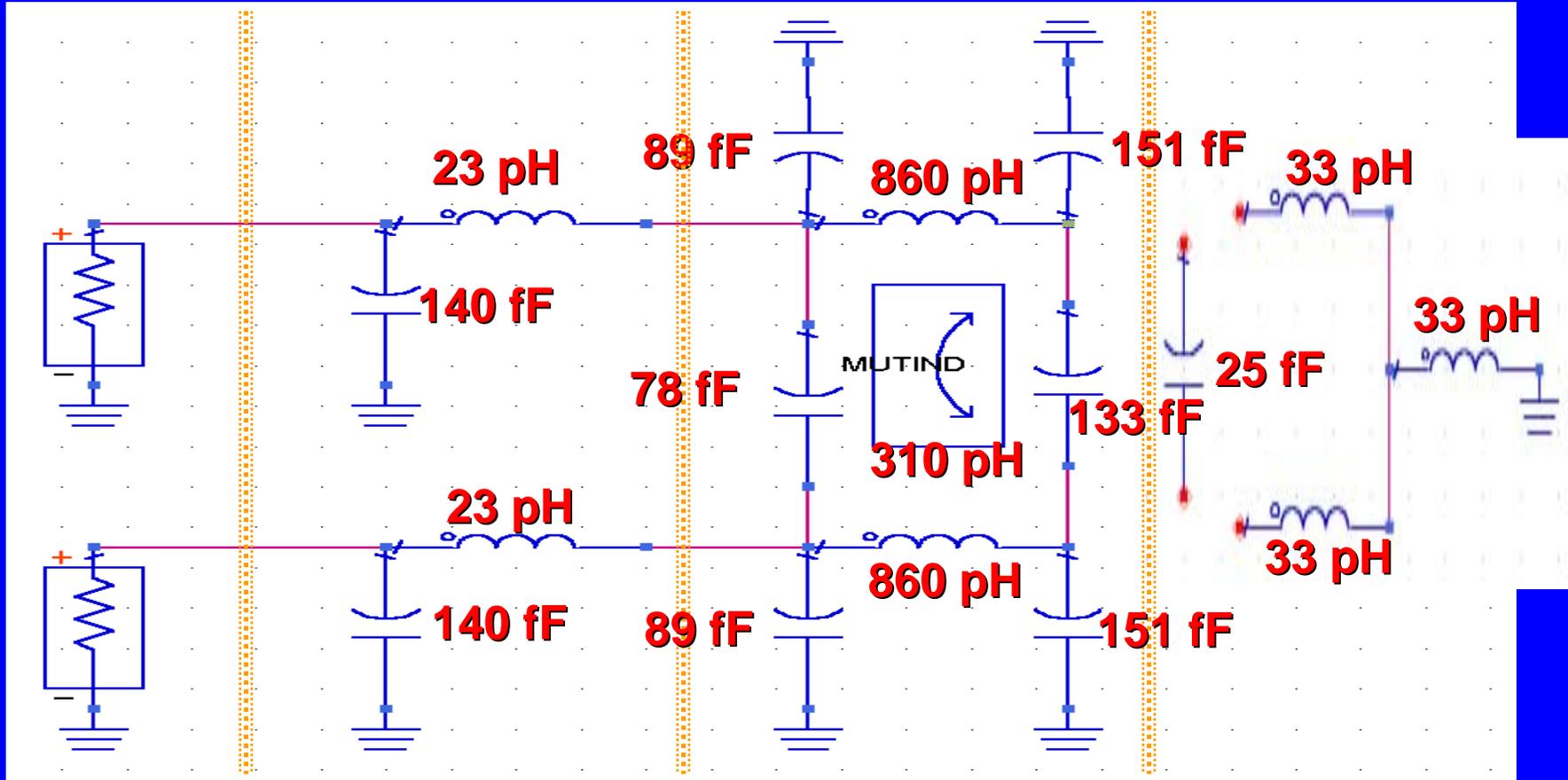
Reflection

Transmission



Bandwidth of the model > 10 GHz

Summary of Extracted Parameters



VNA

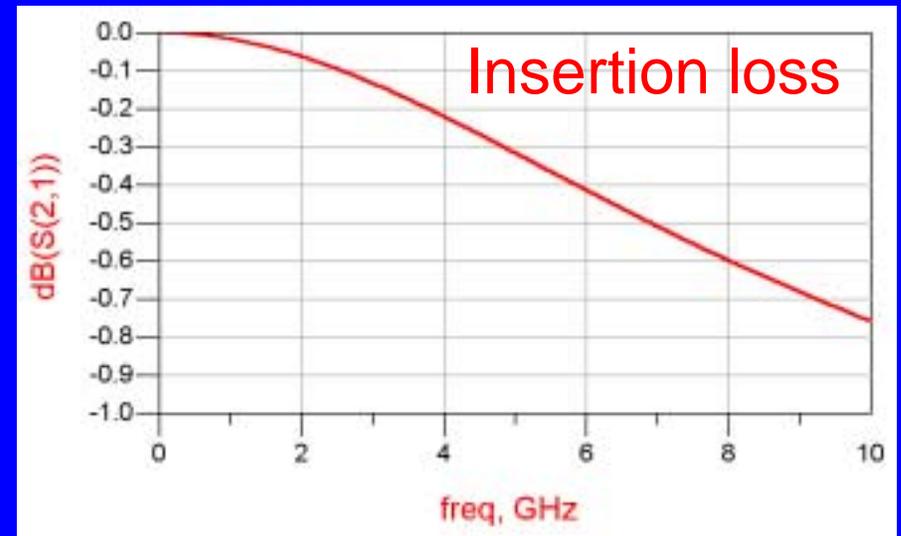
Fixture

Contactor

Surrogate

Note: load board was not optimized for performance

De-Embedded Insertion and Return Loss of Contactor

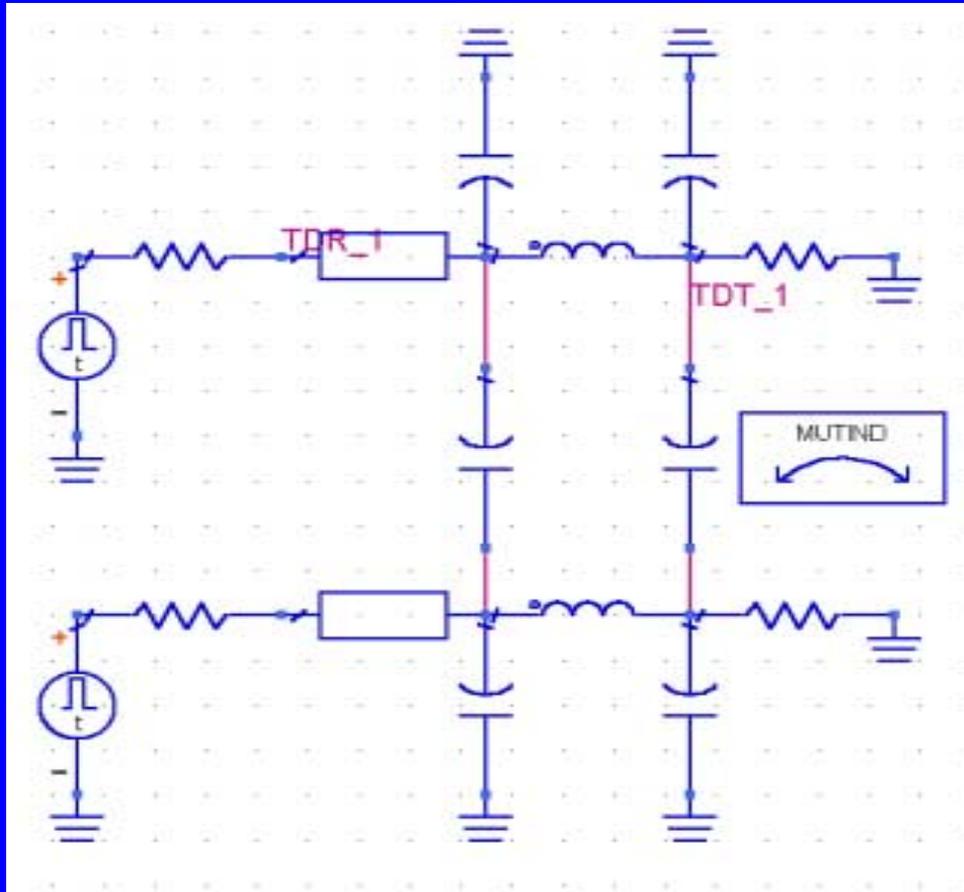


Meets specification:
< -20 dB, below 10 GHz

Meets specification:
> -1 dB, below 10 GHz

Note: load board is not optimized for performance,
standard contactor - not enhanced contactor

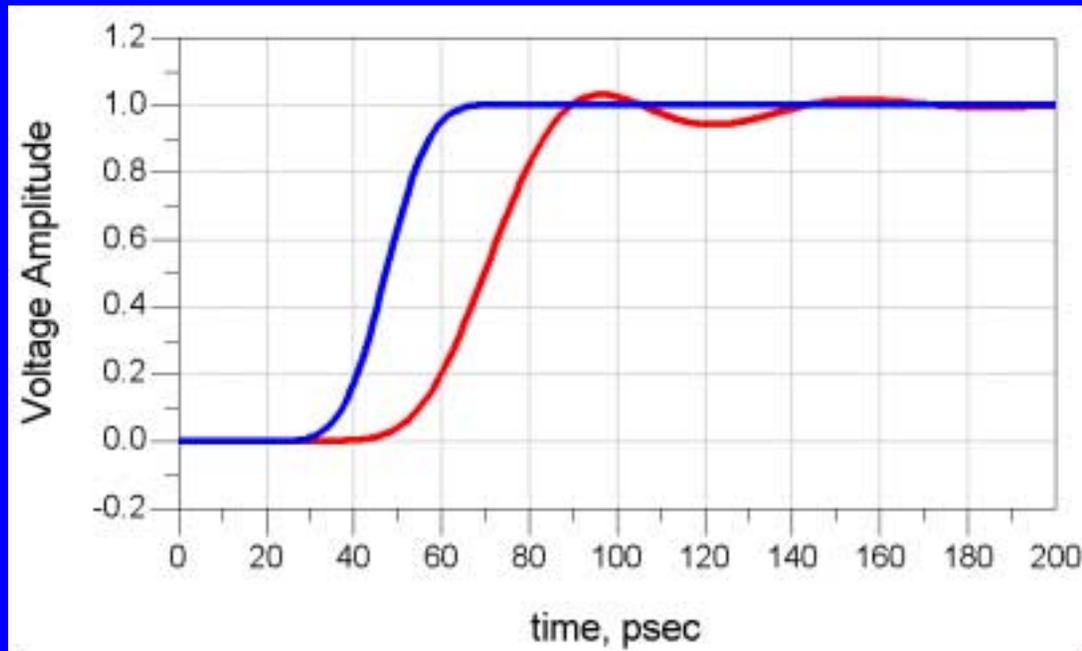
Transient Simulation Using De-embedded Contactor Model



Specs:

- ✓ De-embedded contactor model
- ✓ 20 psec rise time
- ✓ 50 Ω source, termination
- ✓ Differential drive

Transient Simulation with 20 psec Rise Time



- 20 psec input rise time
- 28 psec output rise time
- 20 psec intrinsic interconnect rise time (> 15 GHz bandwidth)
- 21 psec time delay

Note: load board is not optimized for performance,
standard contactor - not enhanced contactor

Conclusions

- A contactor model can be de-embedded from S-parameter measurements
- A simple model matches measured data up to at least 10 GHz. (model could have more bandwidth)
- A model extracted from frequency domain measurements can be used in a transient simulation.

Force Measurement on Sockets and Contactors

2002 Burn-in and Test Socket Workshop
March 3 - 6, 2002

Presenter: **Richard Block**

Rafiq Hussain



Agenda

- **Force Issues in Test and Burn-In Env.**
- **Force Measurement Unit**
- **Experimentation & Test Data**
- **Conclusions**
- **Looking Forward**

Force Issues in Test and Burn-In Env.

- Bent Pins / Deformed Balls
- Overdriving of Pogos
- Crack/Chipped Die or Pkg
- Pkg warping
- Force Distribution

Force Measurement Unit

- Simple Design
 - 1 transducer
 - 2 spacers
 - 1 digital display (giving real-time force readouts to 0.1 lb accuracy)
- Location
 - Replaced support under PCB and Socket

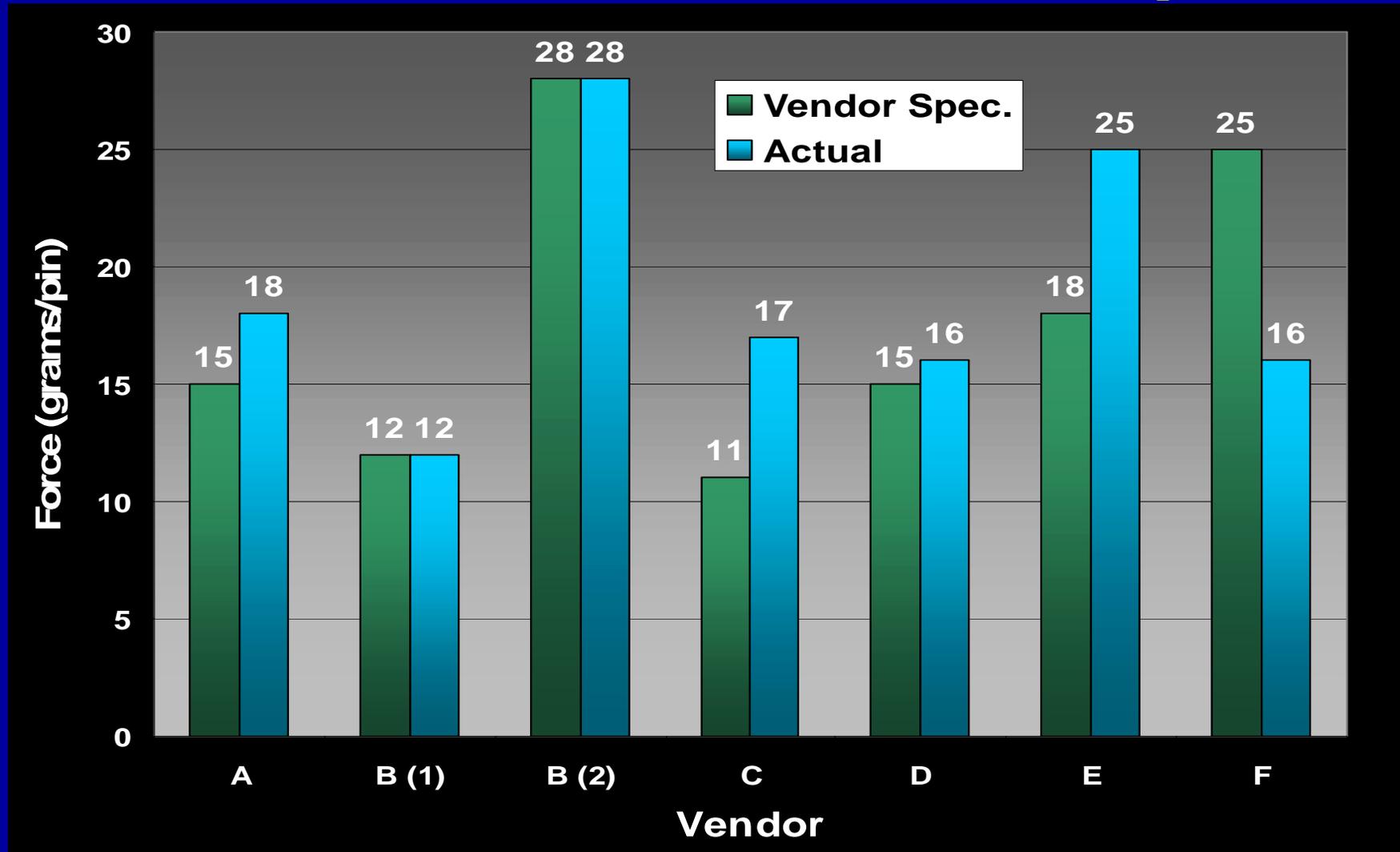
Board Deflection

- Motherboard deflection was necessary for transducer to take measurements
 - Motherboard was 62 mils thick
 - Transducer max deflection was 3 mils for 250lbs
 - Deflection did not create any noticeable error in force readout
 - 2 lb, 5 lb, and 10 lb weights were used for confirmation

Experimentation

- FMU was used for various validations
 - First Experiment
 - Actual force (g/pin) vs. Vendors Spec (g/pin)
 - LLCR measurements were taken at various forces
 - Passing tests consisted of “no opens pins”
 - Both Shorted and Thermal Vehicle pkgs were used

Actual Force vs. Vendor Spec



Experimentation cont.

- FMU was used for various validations
 - Second Experiment
 - Insertion study to find optimal force vs. Pogo life
 - First run:
 - 100,000 insertions were made at ideal force first experiment
 - LLCR measurements were taken periodically to see if resistance values increased
 - Second run:
 - 100,000 insertions at different force
 - LLCR measurements were compared to first run

Insertion Life vs. Force

Vendor	Insertions	ave ohms	Vendor	Insertions	ave ohms
A	Low	22.02	D	Low	23.37
18 g/p	25 k	22.04	16 g/p	25 k	22.75
	50 k	22.10		50 k	22.70
	75 k	22.09		75 k	22.57
B (1)	Low	23.11	E	Low	22.24
12 g/p	25 k	23.27	25 g/p	25k	22.10
	50 k	22.93		50k	22.34
	75 k	22.68		75k	22.30
				96 k	22.14
C	Low	22.82	F	Low	22.25
17 g/p	40 k	22.04	16 g/p	25 k	22.47
	80 k	22.16		50 k	22.30
				75 k	22.38

Insertion Life vs. Force cont.

- Insertions were done at a greater force than first series of insertions.
 - ~3 to 4 g/p depending on initial required force
- Vendor D had pin failures at this higher force

Vendor	Insertions	ave ohms
B (1)		
	Low	23.11
15 g/p	30 k	23.41
	50 k	23.21
	70 k	23.21
D		
	Low	22.57
19 g/p	25 k	22.73
	40 k	22.40
E		
	Low	22.24
28 g/p	25k	26.67
	75k	26.35

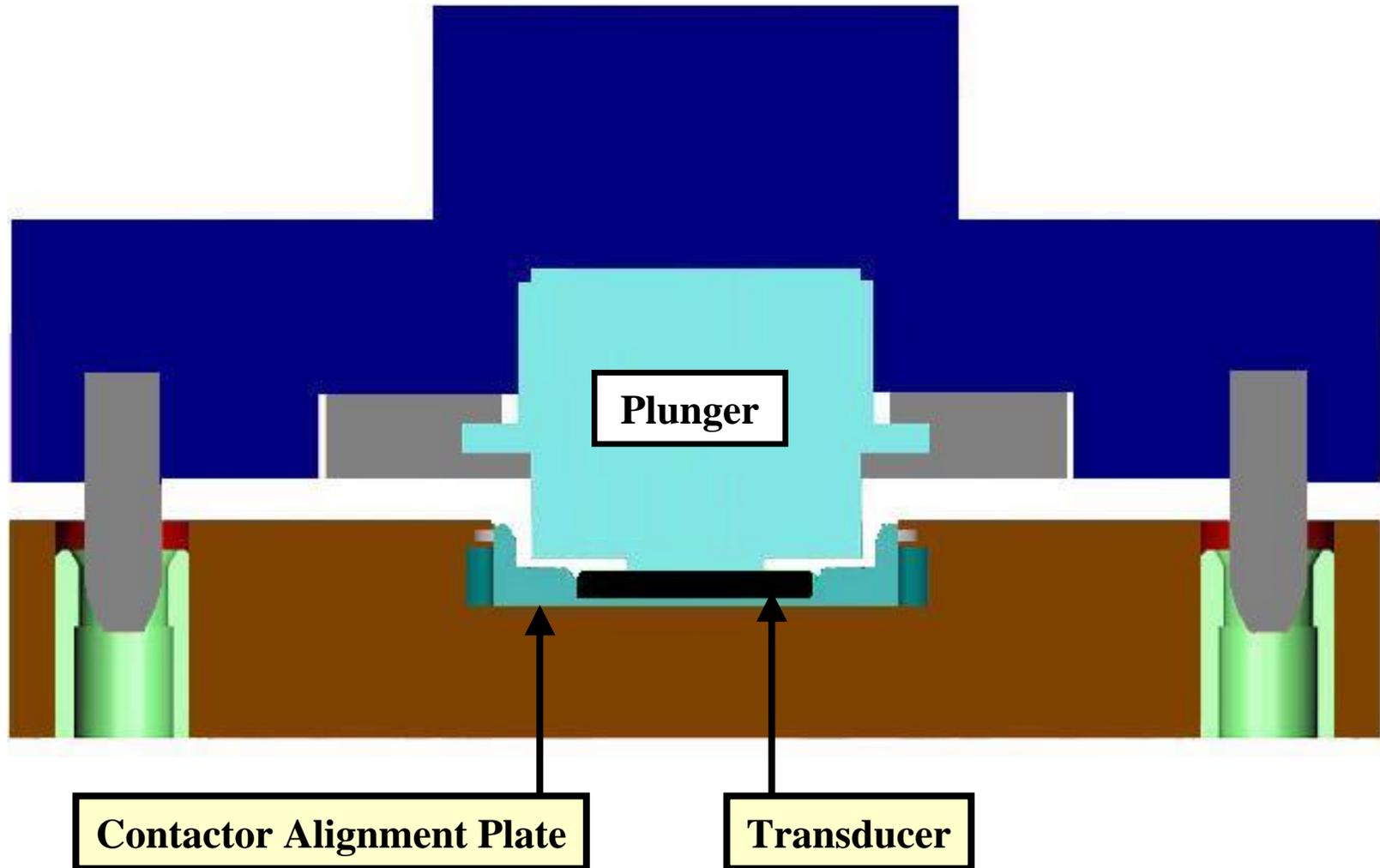
Conclusions

- Insight into vendors tolerance control and machining ability
- Confirmation of test forces on DUT with reaction forces based on complete test setup, not individual pieces tested separately
- More accurate qualification for compression based sockets

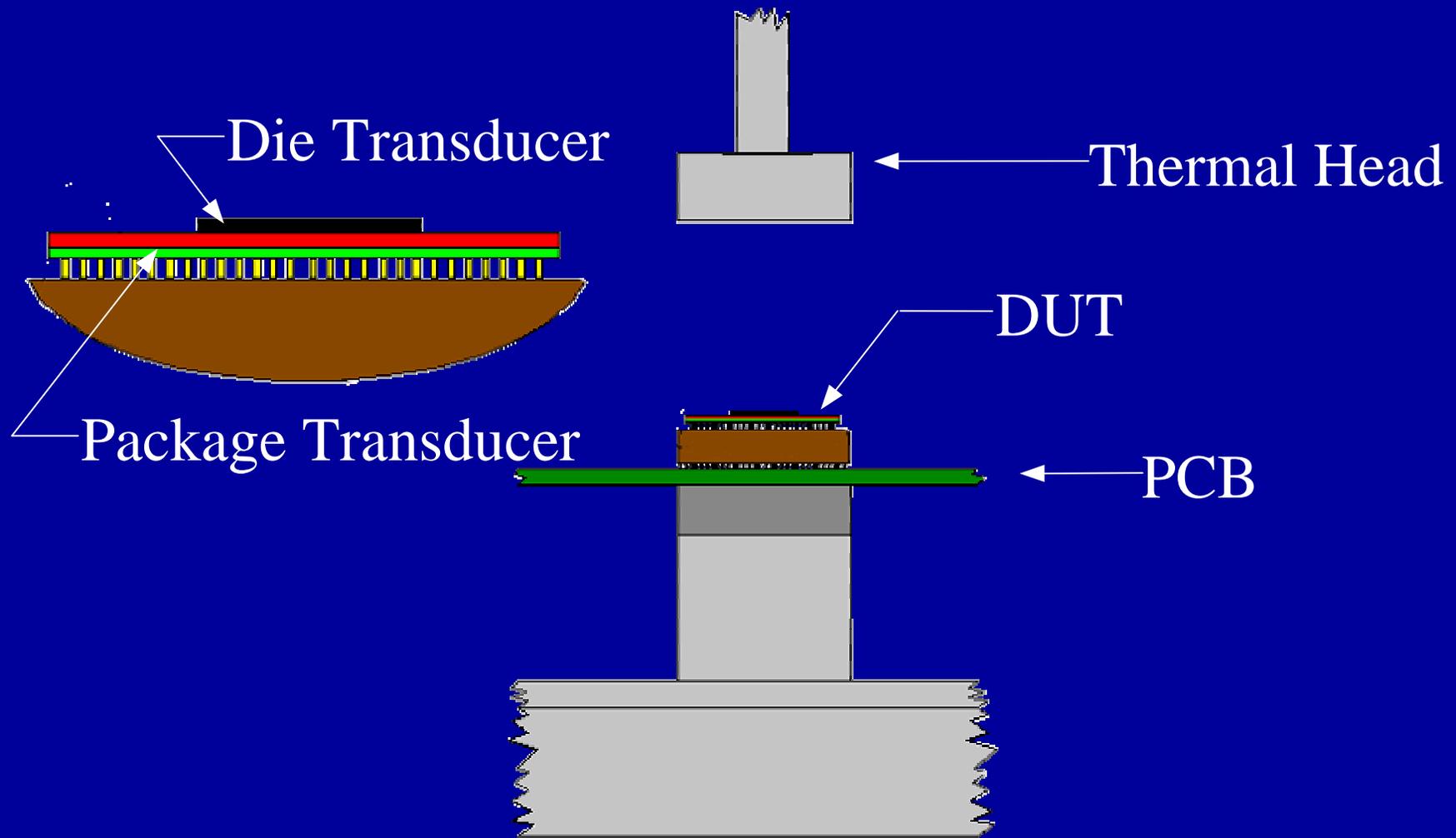
Looking Forward

- Die size Transducers
- Force variation across die/pkg

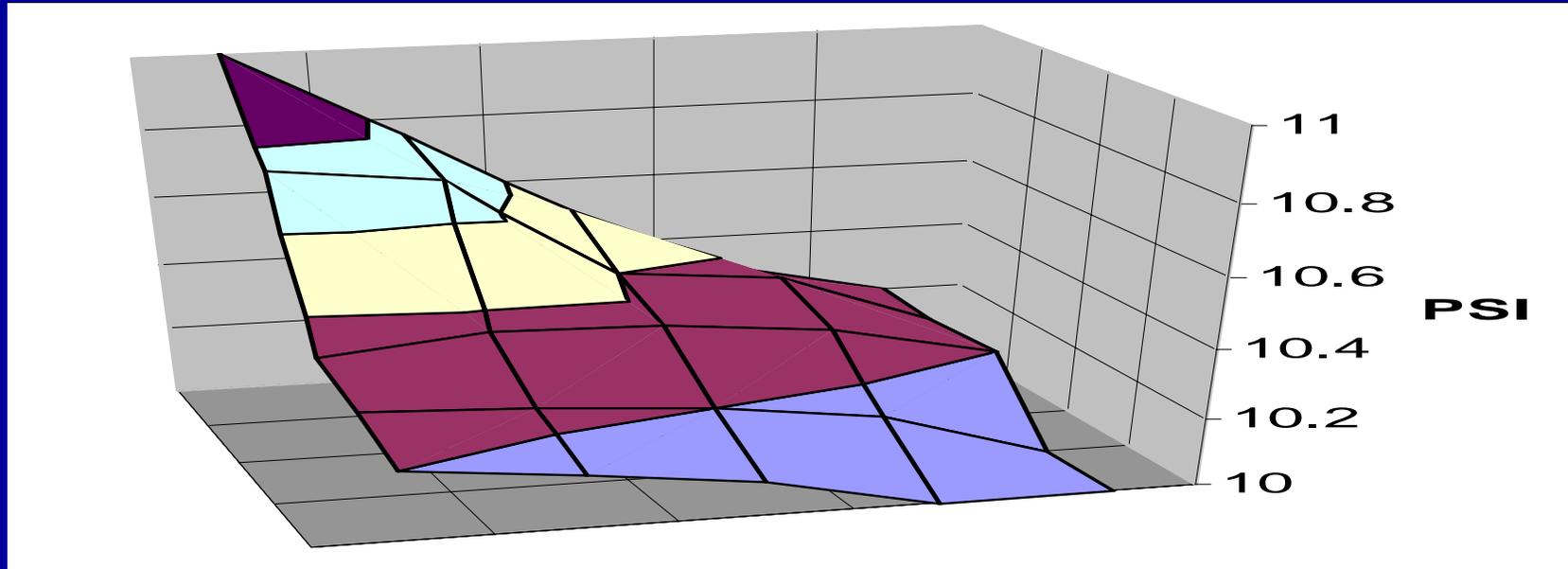
Transducer for Handlers Example



Package/Die Transducer Example



Distribution of Force over Die/Pkg Example



- Check Force across die surface
 - Check flatness of thermal head
 - Check that socket is level